

MX SITING INVESTIGATION GEOTECHNICAL SUMMARY

PRIME CHARACTERIZATION SITES
GREAT BASIN
CANDIDATE SITING PROVINCE

PREPARED FOR SPACE AND MISSILE SYSTEMS ORGANIZATION (SAMSO) NORTON AIR FORCE BASE, CALIFORNIA



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MX SITING INVESTIGATION
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PRIME CHARACTERIZATION SITES
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CANDIDATE SITING PROVINCE

Prepared for:

U. S. Department of the Air Force Space and Missile Systems Organization (SAMSO) Norton Air Force Base, California 92409

Prepared by:

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25 September 1978 15 February 1979 (rev.)

PRIME CHARACTERIZATION SITES GREAT BASIN CSP

ERRATA

Replace the following figures with revised ones which accompany this sheet: Figures 5 (p. 16), 6 (p. 17), 11 (p. 36), 12 (p. 38), 17 (p. 55), and 18 (p. 57).

Replace the following tables with revised ones which accompany this sheet: Tables 5 (p. 19), 14 (p. 39), 23 (p. 58), and 24 (p. 59).

The following corrections are to be made to the original text:

page iii, List of Figures, Figure 2: Change "...Activities Flocations,..." to read "...Activity locations,..."

page iii, List of Figures, Figure 8: Change "...Activities locations,..." to read "...Activity locations,..."

page iii, List of Figures, Figure 14: Change "...Activities locations..." to read "...Activity locations,..."

* page 3, paragraph 3, line 4: Change "...table..." to read "-"able"

page 4, line 9: Change "...Valleys..." to read "...valleys..."

√ page 4, line 13: Change "...sacle..." to read "...scale..."

page 6, Section 2.1, line 5: Change "...Tables 2 and 3..." to read "...Tables 2 and 3."

page 10, Figure 2: Generalized geologic map base revised, see Figure 5.

page 26, Section 3.0, line 4: Change "...bombing..." to read "...Bombing..."

* page 26, Section 3.1, line 3: Change "...is..." to read "...are..."

page 30, Figure 8: Generalized geologic map base revised, see Figure 11.

*/ page 35, last two lines: Remove the two words "...is bed-

page 46, Section 4.0, line 5: Change "...state highway..."
to read "...State Highway..."

* page 46, Section 4.0, line 6: Change word to read "...longi-tude..."

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- page 46, Section 4.0, Line 11: Change "...state highway..."
- ν page 50, Figure 14: Generalized geologic map base revised, see Figure 17.
- *, page 51, paragraph 2, line 2: remove the word "...bouldery..."
- */ page 51, paragraph 2, line 5: Remove the comma.
- page 56, Section 4.4, line 3: Change "...sionnal..." to ν "...sional..."
- * page #1, paragraph 1, line 14: Change sentence to read "...be able to..."
- * Corrections have already been made in some report copies.

FOREWORD

This report was prepared for the Department of the Air Force, Space and Missile Systems Organization (SAMSO) in compliance with conditions of Contract No. F04704-77-C-0010, and is a geotechnical summary of the three prime Characterization sites in the Great Basin Candidate Siting Province (CSP). The three sites are Dry Lake Valley and Ralston Valley, Nevada; and Sacramento Valley, Arizona.

The report presents representative data obtained from geotechnical field investigations performed at the three sites as part of the Characterization program. The information obtained from these studies, in combination with data obtained in the Screening studies, has been used for geotechnical ranking (FN-TR-25).

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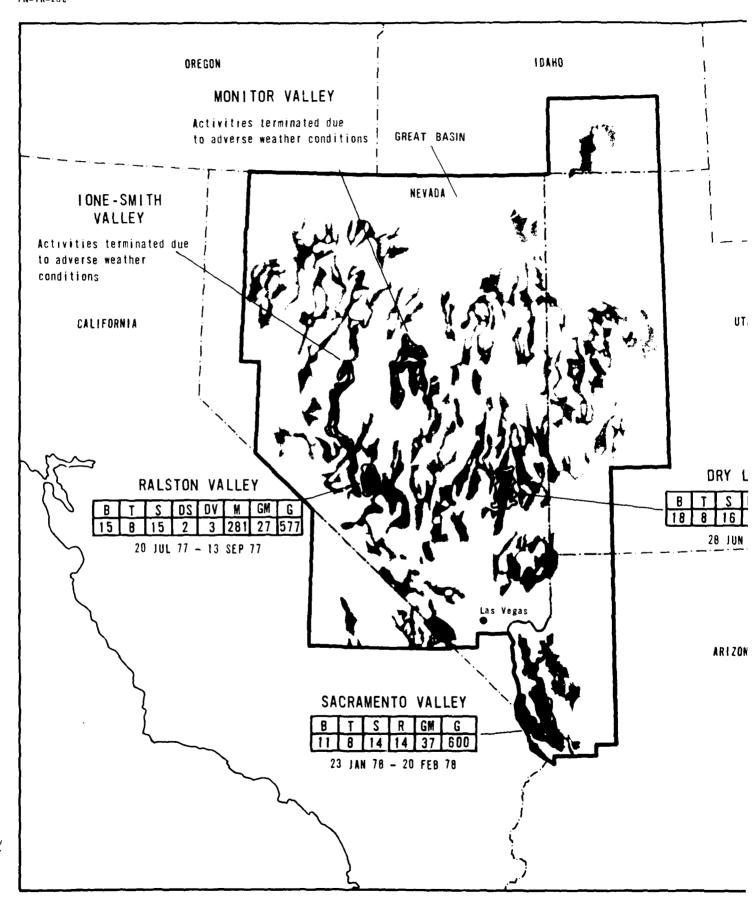
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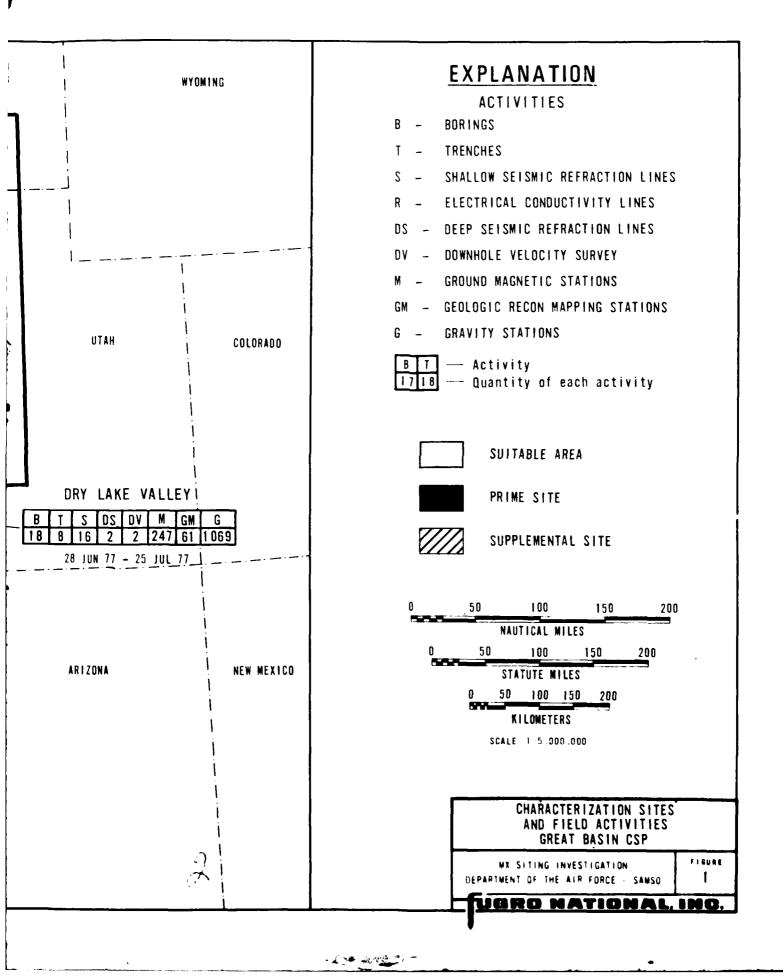
This report presents the results of geotechnical field investigations performed in the Dry Lake and Ralston Valley Characterization Sites in central Nevada and the Sacramento Valley Characterization Site in northwestern Arizona. This report presents representative data collected and analyzed for these sites. Access to the remaining data can be arranged through SAMSO/MNND, Norton Air Force Base, California.

The three sites are located in the Great Basin Candidate Siting Province (CSP), one of six provinces involved in the geotechnical Characterization studies. The location of the sites within the Great Basin CSP is shown in Figure 1. The Great Basin CSP is characterized by northeast to northwest trending elongate mountain ranges with intervening valleys. Most of the CSP lies within the state of Nevada, however, portions do extend into Utah, Arizona, California, and Idaho.

Suitable areas for deployment of MX missile systems remaining after Intermediate Screening were divided into CSPs based on similar geotechnical characteristics. The results of Intermediate Screening (FN-TR-17) indicated that existing data were not adequate in type or level of detail for follow-on geotechnical and geo-environmental evaluations, screening, site selection, and ranking studies. Therefore, the Characterization studies were developed to provide a rapid, relatively inexpensive method of gathering geotechnical data in a small area (maximum 700 nm²; 2400 km²) which is considered to be representative of a larger area within the CSP.

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Emphasis was placed on the collection of information allowing characterization of geological units with respect to the construction aspects of MX missile basing options. Objectives of the Characterization studies were to obtain data that address the following geotechnical aspects:

- o Surficial geology and terrain
- o Subsurface conditions
- o Geophysical properties
- o Engineering properties

Although the program originally emphasized data collection for the trench and horizontal shelter basing modes, the data were utilized for evaluation of the vertical shelter basing mode as well. Characterization was, therefore, a refinement of the screening process whereby the necessary geotechnical information was developed to support the broader MX system design activities that were taking place concurrently and to provide a basis for geotechnical ranking of the CSPs for different basing modes.

Five Characterization sites (three prime and two supplemental) were selected in the Great Basin CSP (Figure 1), representing a total investigated area of less than ten percent of all suitable area within the CSP. Field activities in the two supplemental sites were terminated due to adverse weather conditions. Therefore only the three prime sites are discussed in this report. The Characterization Site selection process began with a delineation of geotechnically similar areas within each CSP having analogous depositional and geologic histories, rock and

water depths, and tectonic settings. Once these areas had been identified, non-geotechnical factors were applied to delineate the actual Characterization site boundaries. These non-geotechnical selection factors included access, proximity to support facilities, environmental sensitivities, and local logistical requirements.

Geologic, geophysical, and soils engineering techniques were used to determine the surface and subsurface geotechnical conditions in Dry Lake, Ralston, and Sacramento Valleys. These include a combination of the following:

- o Analysis of available data
- o Aerial photo interpretation of surficial geologic units utilizing black and white stereographic pairs at a sacle of approximately 1:60,000
- o Geologic field investigation to check aerial photo interpretation and to determine physical properties of the surficial units at selected field stations
- o Shallow and deep seismic refraction, downhole seismic velocity, and electrical conductivity surveys to obtain subsurface profile information
- o Gravity and ground magnetic surveys to aid in interpretation of basin configuration
- O Drilling and trenching to determine subsurface characteristics and obtain soil samples
- o Laboratory testing of soil samples to determine engineering properties

The Battle Mountain, Ely, and Kingman district offices of the U.S. Bureau of Land Management were contacted for access to the sites. Prior to initiating any field work, an archeological and environmental inspection was conducted at each site to ensure minimal impact to the local environment and to avoid damage to archeologic and historic sites. To further minimize potential impacts, all field activities were performed adjacent to existing roads or other previously disturbed areas.

2.0 DRY LAKE VALLEY SITE

The Dry Lake Valley Characterization Site covers an area of 251 nm² (861 km²) in central Lincoln County, Nevada. The site is bounded by mountain ranges on the east, north, and west, and is open to Delamar Valley on the south. U. S. Highway 93 forms the southern boundary of the site and is the only paved road in the vicinity. A network of graded roads and fourwheel drive trails provide access within the site.

2.1 SCOPE OF INVESTIGATION

Scope of geologic, geophysical, and soils engineering field activities performed at the site and laboratory tests performed on soil samples from the site is presented in Table 1. Detailed information about the soils engineering field activities (18 borings and eight trenches) is summarized in Tables 2 and 3 Locations of all the field activities are shown in Figure 2.

2.2 SURFICIAL GEOLOGY AND TERRAIN

Alluvial fan deposits of younger and intermediate age are the predominant surficial geologic units within the Characterization site (Figure 2). The younger fan deposits cover approximately 42 percent of the area while the intermediate fan deposits cover 26 percent. Playa deposits cover approximately six percent of the surface. Although these playa deposits do not represent a large percentage of the surface area, they are generally of great thickness and interfinger with alluvial deposits in the subsurface. Playa deposits are located in the valley center with the alluvial fan deposits present between the playa and mountain fronts.

GEOLOGY AND GEOPHYSICS

TYPE OF ACTIVITY	NUMBER OF ACTIVITIES
Geological mapping stations	61
Shallow refraction	16
Deep refraction	2
Downhole velocity	2
Gravity survey	1069
Ground magnetic stations	247

ENGINEERING

NUMBER OF BORINGS	NOMINAL DEPTH FEET (METERS)
1	25 (8)
3	50 (15)
8	100 (30)
5	300 (91)
1	450 (137)
NUMBER OF TRENCHES	NOMINAL DEPTH FEET (METERS)
1	16 (5)
7	18 (6)

ENGINEERING-LABORATORY TESTS

TYPE OF TEST	NUMBER OF TESTS
Moisture/density	362
Specific gravity	12
Sieve analysis	206
Hydrometer	99
Atterberg limits	121
Consolidation	4

TYPE OF TEST	NUMBER OF TESTS
Unconfined compression	13
Triaxial compression	10
Direct shear	4
Compaction	8
CBR	4
Chemical analysis	11

SCOPE OF FIELD AND LABORATORY ACTIVITIES DRY LAKE VALLEY, NEVADA, GREAT BASIN CSP

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TABLE 1

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BORING NUMBER	TOTAL DEPTH FEET(METERS)	TYPE OF DRILL RIG USED	TYPE OF SAMPLES* OBTAINED
DL-8-1	100.3(30.6)	Rotary Wash	22
DL-B-2	100.9(30.8)	Rotary Wash	SS. B
DL-B-4	44.5(13.6)	Percussion	В
DL-B-5	300.4(91.6)	Sary Air	Р, В
DL-8-6	100.0(30.5)	noissusses	В
DL-B-7	95.0(29.0)	Tercussion	В
DL-B-8	300.5(91.8)	Rotary Air/Wash	P, SS, B
DĽ-5-8	100.0(30.5)	Pércussion	В
OL-8-10	23.0(7.1)	Percussion	В
DL-8-11	54.0(16.5)	Percussion	В
DL-B-12	300.0(91.4)	Rotary Air/Wash	P, SS, B
DL-B-13	302.1(92.1)	Rotary Air/Wash	P, SS, B
DL-B-14	47.0(14.3)	Percussion	В
DL-B-15	300.3(91.5)	Rotary Air/Wash	P.D.SS
DL-B-16	103.0(31.4)	Percussion	B, D
OL-8-17	100.0(30.5)	Percussion	B, D
DL-B-18	100.6(30.7)	Rotary Wash	P, B
DL-B-19	451.9(137.7)	Rotary Air/Wash	P, B

* P = Pitcher sample (undisturbed)

D = Fugro Drive sample (relatively undisturbed)

B = Bulk sample (disturbed, but representative)

\$\$ = Split Spoon sample (disturbed, but representative)

ENGINEERING FIELD ACTIVITIES - BORINGS
DRY LAKE VALLEY, NEVADA
GREAT BASIN CSP

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TABLE

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TRENCH NUMBER	TOTAL DEPTH FEET (METERS)	STABILITY OF VERTICAL EXCAVATION WALLS AND REMARKS
DL-T-1	18.0 (5.5)	O-10° (O-3.0m) stable 10-14° (3.0-4.3m) unstable; heavy sloughing into trench 14-18° (4.3-5.5m) stable; stage II caliche layer
DL-T-2	18.0 (5.5)	0-2° (0-0.6m) unstable 2-16° (0.6-4.9m) stable; stage III caliche layer at 12-14° (3.7-4.3m) 16-18° (4.9-5.5m) unstable; heavy sloughing into trench
DL-T-8	16.0 (4.9)	0-8' (0-2.4m) stable 8-14' (2.4-4.3m) unstable; heavy caving into trench 14-16' (4.3-4.9m) stable
DL-T-9	18.0 (5.5)	0-1' (0-0.3m) unstable 1-11' (0.3-3.4m) stable 11-15' (3.4-4.0m) unstable; sloughing into trench 15-18' (4.6-5.5m) stable
DL-T-11	18.0 (5.5)	0-3' (0-0.9m) unstable 3-18' (0.9-5.5m) stable
DL-T-12	18.0 (5.5)	0-6' (0-1.8m) unstable 6-18' (1.8-5.5m) stable
OL-T-15	18.0 (5.5)	stable
DL-T-17	18.0 (5.5)	unstable; heavy caving and sloughing. Trench was located in an active stream bed.

ENGINEERING FIELD ACTIVITIES - TRENCHES

DRY LAKE VALLEY, NEVADA

GREAT BASIN CSP

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TABLE

<u>ugro national, inc.</u>

. In lique 5 EXPLANATION SURFICIAL GEOLOGIC UNITS A1, A2 and Au - stream channel, terface and undifferentiated deposits A4 - playa deposits A5y - younger alluvial fan deposits A5i — intermediate alluvial fan deposits A50 and A6 - older alluvial fan and pediment deposits ROCK UNITS S - sedimentary 1:250,000 1''≈ 4 MILES 1 - igneous Fault, dashed where approximately located NOTE: For detailed description of geologic units, see Table A-1 SYMBOLS Boring Shallow seismic toitaction line Deep seismic refraction line Tranch Downhole velocity GENERALIZED GEOLOGIC WAP AND FIELD ACTIVITY LOCATIONS DRY LAKE VALLEY, NEVADA, GREAT BASIN CSP WX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAMSO UBRO NATIONAL, INC.

FN-TR-26e 11

The alluvial fan deposits are typically silty sands with gravel, ranging from sandy gravels near the mountain front to sandy silts near the playa. Playa deposits are generally clayey silts. These three units along with the remaining surficial units are described in Table 4.

Surface slopes and depths of drainage incision vary with geologic units, both generally increasing with proximity to the mountain fronts (Table 4). Maximum surface slope is ten percent with typical slopes of four percent. Maximum depths of incision (excluding older alluvial fan deposits) are 15 feet (5 m) with typical depths of five feet (1.5 m).

2.3 SUBSURFACE CONDITIONS

2.3.1 Soil Profiles

The composition of soils with depth is illustrated by the soil profiles shown in Figures 3 and 4. The dominant valley soils are silty sands and gravelly sands, which interbed with sandy gravels near the mountain fronts and clayey silts near the valley center. Cobbles and boulders are occasionally found near the mountain fronts and some plastic clays are encountered in the playas. Cementation of the soils varies with soil type and age, generally increasing with age of soil. Sandy soils with less than five percent fines were generally uncemented to weakly cemented, often caving in unshored trenches.

	GEOLOGIC AGE	THICKNESS		USCS SYMBOL(S)	AREAL EXTENT (SITE)		
SURFICIAL GEOLOGIC UNIT (a)		FEET (METERS)	DESCRIPTIVE NAME(S)		nm ² (km ²)	PERCENT	
Undifferentiated Non-Rock Deposits (Au)	Quaternary- Tertiary	Unknown	Silty Sand with Gravel	SM	16 (55)	6	
Fluvial Deposits (A1)	Holocene	Unknown	Silty Sand with Gravel	SM	24 (82)	10	
Stream Terrace Deposits (A2s)	Holocene	Unknown	Silty Sand with Gravel	SM	16 (55)	6	
Playa Deposits (A4)	Holocene	Unknown	Silty Clay Clayey Silt	CL, ML	11 (37)	4	
Older Playa and or Lacustrine Deposits (A4o)	Quaternary- Tertiary	Unknown	Clayey Sılt	MH	5 (17)	2	
Younger Alluvial Fan Deposits (A5y)	Holocene	Unknown	Silty Sand with Gravel	SM	103 (353)	42	
ntermediate Alluvial Fan Deposits (A5i)	Pleistocene	Unknown	Gravelly Silty Sand	SM	70 (241)	28	
Older Alluvial Fan Deposits (A5o)	Pleistocene	Unknown	Gravelly Silty Sand	SM	6 (21)	2	

NOTES:

- (a) For generic description of geologic units, see Table A-1.
- (b) For description of USCS, see Table A-2.
- (c) For description of stage of caliche, see Figure A-1.
- (d) Mixed Al. A4, and A5 deposits.
- (e) Includes three percent alluvial outwash deposits (Alw) which consists of mixed Al. A5y, and A5i deposits.
- (f) Includes three percent mixed A4 and Au deposits; designated A4 Au on Figures 2 & 5.
- (g) Includes two percent of area underlain by shallow rock, designated A6 on Figures 2 & 5

REAL EXTE	NT (SITE)		PROPERTIE	S OF SURFACE	MATERIALS		SURFACE MORPHOLOGY		1
m ² (km ²)	PERCENT	GRADATION	CEMENTATION	MAXIMUM GRAIN SIZE	PAVEMENT/ PATINA	STAGE OF CALICHE (c)	SLOPE (PERCENT)	DRAINAGE DEPTHS FEET(METERS)	NOTES
6 (55)	6	Poor-Well	Weak- Moderate	Cobble	None-Well/ None-Well	I-IX	×1-10	0-25 (0-8)	(d)
4 (82)	10	Moderately well	None	Cobble	None/None	None-I	«	0-1 (0-0 3)	(e)
8 (55)	6	Moderately well	Weak	Cobbie	Poor/ None-Paor	None-I	«	0-15 (0-5)	
1 (37)	4	Poor	None-Weak	Sand	None/None	None-I	<	0-2 (0-0 6)	(f)
(17)	2	Poor	Weak	Sand	None-Poor/ None-Poor	None-I	<	0-5 (0-1 5)	
3 (353)	42	Poor- Moderately well	None-Weak	Cobble	None-Poor/ None-Poor	None-I	0–5	0-5 (0-1 5)	
(241)	28	Moderately well-Well	Weak- Moderate	Boulder	Poor-Well/ None-Fair	I-II	2-10	315 (1-5)	(g)
(21)	2	Moderately well-Well	Weak- Moderate	Boulder	Poor-Well/ Poor-Well	111-11	5-10	5-25 (0-8)	
									_
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and A5i deposits.

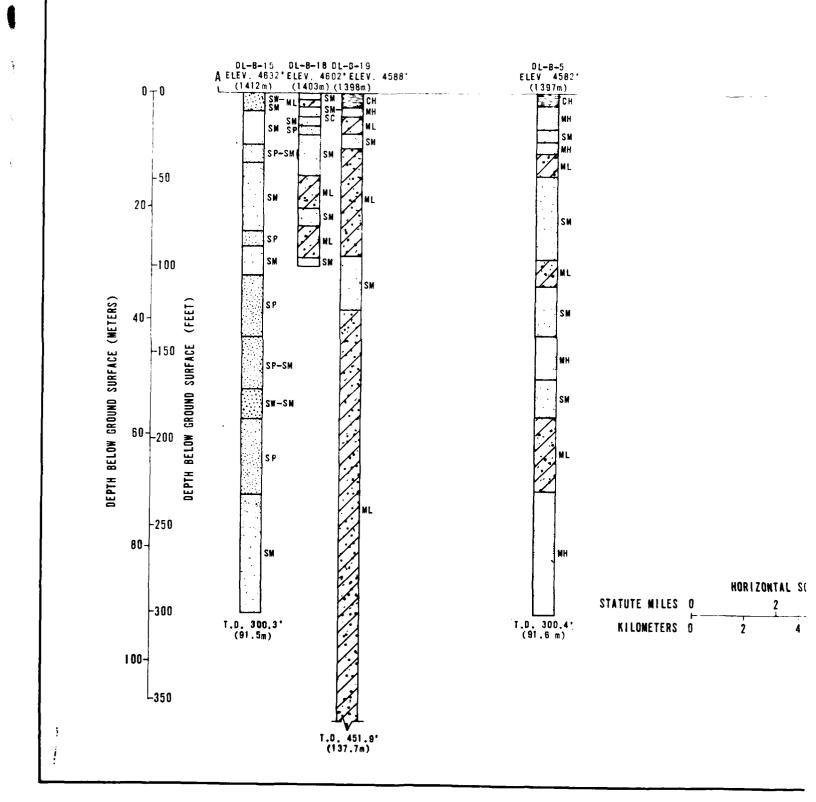
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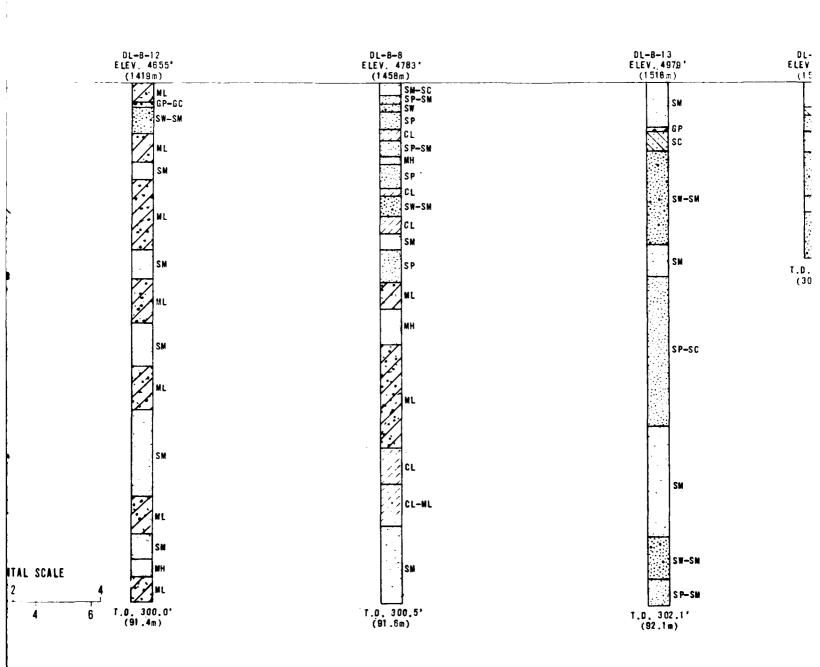
DESCRIPTION OF SURFICIAL
GEOLOGIC UNITS
DRY LAKE VALLEY, NEVADA. GREAT BASIN CSP

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TABLE

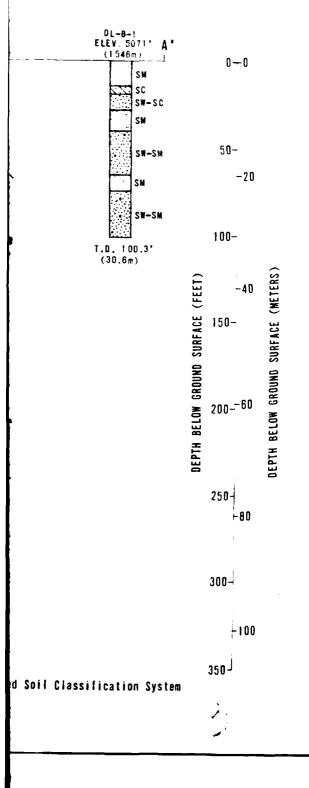
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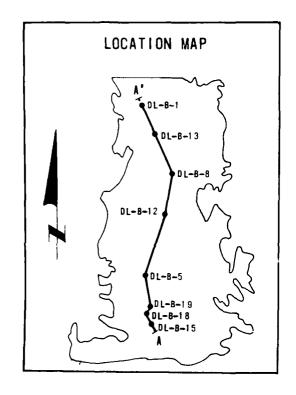




• MOTES: 1. T.D.= Total Depth

2. Soil types shown adjacent to soil column are based on Unified Soil Classific (USCS) and are explained in the appendix



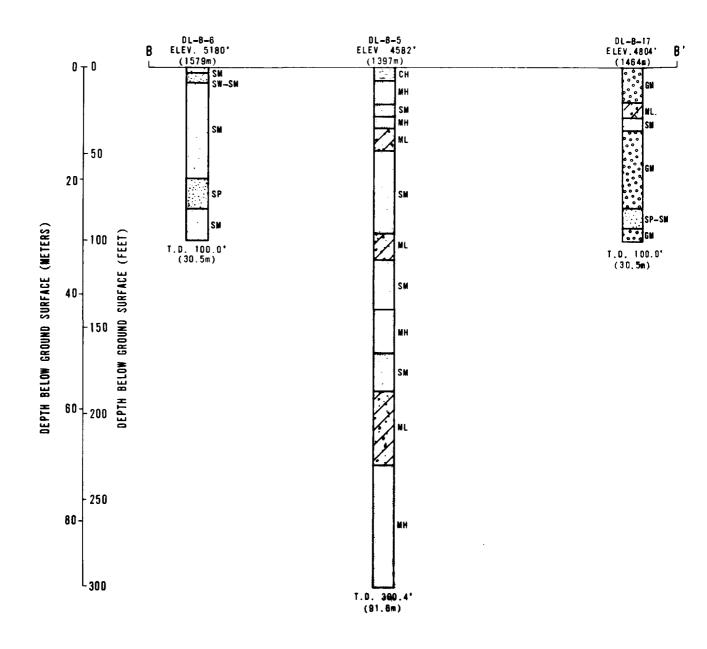


SOIL PROFILE AA'
DRY LAKE VALLEY, NEVADA
GREAT BASIN CSP

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FIGURE 3

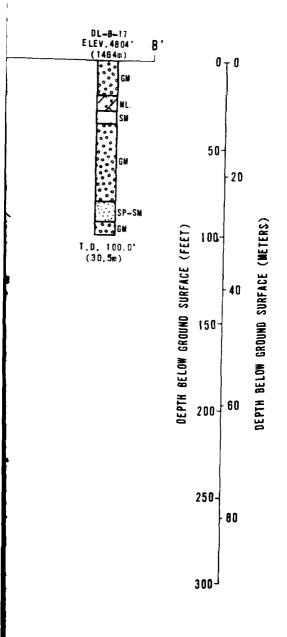
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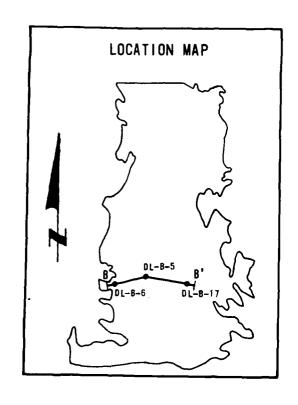


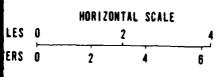
NOTES: 1. T.D. = Total Depth

2. Soil types shown adjacent to soil column are based on Unified Soil Classification System (USCS) and are explained in the appendix.

		HORIZONTAL	SCA
STATUTE MILES	0	2	
KILOMETERS	Ö	2	4







SOIL PROFILE BB'
DRY LAKE VALLEY, NEVADA
GREAT-BASIN CSP

MX SITING INVESTIGATION

FIGURE

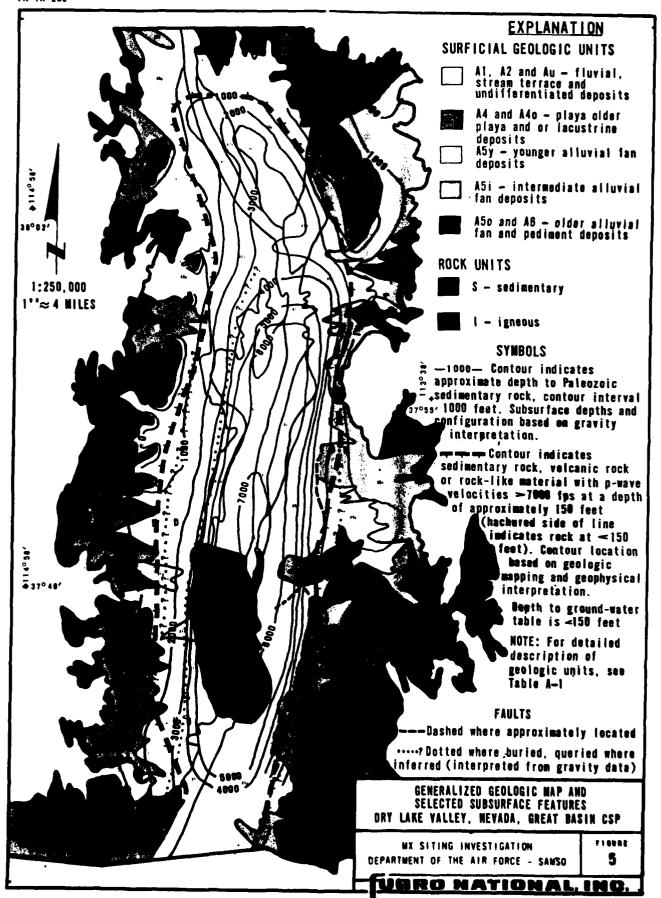
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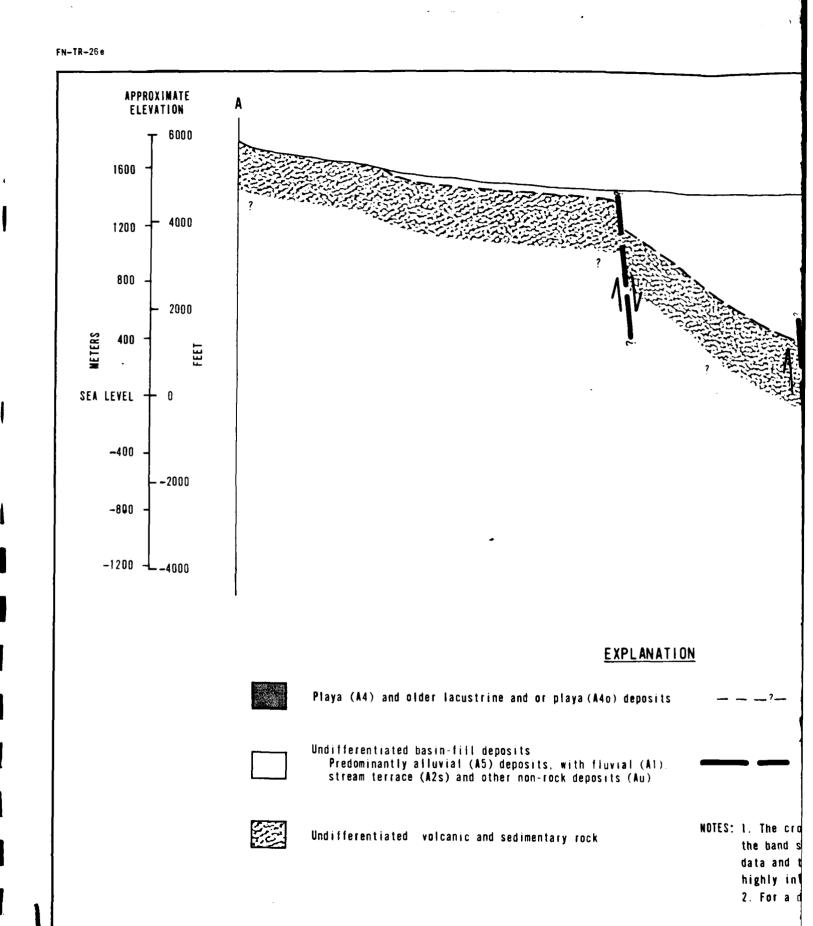
FN-TR-26e 15

2.3.2 Depth to Shallow (<150 ft; <46 m) Rock and Water
Figure 5 shows the portions of the Dry Lake site in which rock
(seismic velocity >7,000 fps; 2134 mps) and water are estimated
to be encountered within a depth of 150 feet (46 m) below the
ground surface. Shallow rock comprises approximately 20 percent
of the site based on data and interpretation from borings, seismic
surveys, gravity surveys, surface outcrops, topography, geologic
maps, and other available data. Ground water is nowhere less
than 150 feet (46 m) below the surface and probably greater than
300 feet (91 m) based on information from five wells and regional
data.

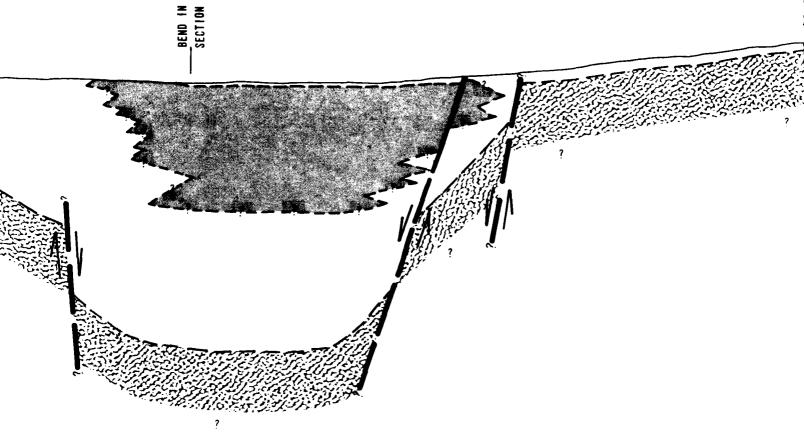
2.3.3 Basin Configuration

Data from deep seismic refraction, gravity, and ground magnetic surveys were used in determining the basin configuration illustrated in Figures 5 and 6. Deep seismic data indicate a layered relationship of basin-fill deposits and/or younger volcanic rocks. Gravity survey data indicate the greatest depth to Paleozoic carbonate and clastic bedrock units to be approximately 6200 feet (1890 m) below the surface in the area of the generalized geologic cross-section (Figures 5 and 6). The basin is bounded on the east, west, and north by steep gradients in basement topography typical of those associated with normal faults. A fault scarp exposed along the east side of the valley coincides with an inferred basement fault, with displacement down on the basinward side. Planated rock shelves, covered by approximately 150 feet (46 m) of basin-fill deposits are inferred along the eastern and western valley margins. The distal limits of these rock





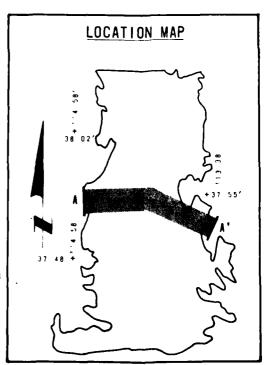
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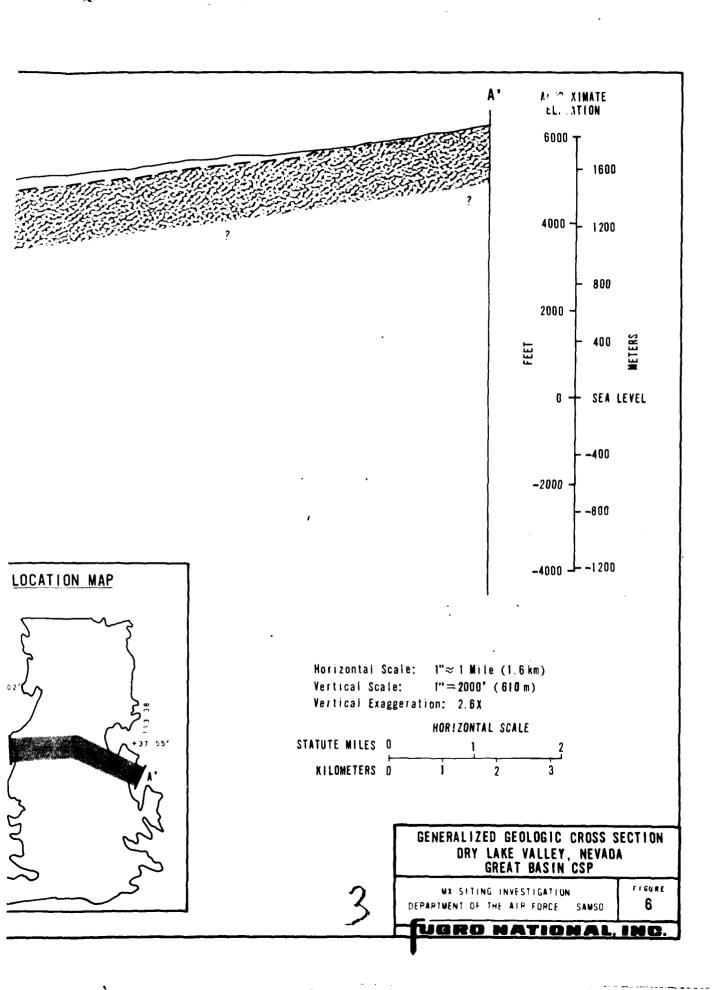
Approximate geologic contact queried where inferred

Fault, dashed where inferred from gravity interpretation

- 1. The cross section is generally representative of subsurface conditions within the band shown on the location map. Due to the limited density of available data and the sparseness of newly acquired data, the subsurface conditions are highly interpretive.
- 2. For a detailed description of geologic units see Table A-1.



7.



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shelves are located near the surface projection of the basement faults. Rock exposures and shallow (<150 ft; 46 m) rock do not occur basinward of these faults.

2.4 GEOPHYSICAL PROPERTIES

Results of shallow and deep seismic refraction surveys and downhole velocity surveys are presented in Tables 5, 6, and 7, respectively. Shallow seismic refraction results (Table 5) indicate dipping and laterally discontinuous velocity horizons.

Deep seismic refraction results (Table 6) indicate discontinuous velocity horizons probably due to an interfingering of basin-fill deposits with younger volcanic rocks or other basin-fill deposits. The compressional wave velocities from downhole velocity surveys (Table 7) do not correspond with those from shallow seismic refraction (Table 5) due to the anisotropy of the ground and method of measurement.

2.5 ENGINEERING PROPERTIES

Engineering properties of the subsoils representing the various geologic units were determined from laboratory tests. The tests included the following; classification, consolidation, shear strength, compaction, CBR, and chemical. The range of engineering properties and compressional wave velocities of the predominant geologic units is presented in Table 8.

Younger and intermediate alluvial fan deposits are combined into one unit since they could not be differentiated at depth. In addition, these two units have similar grain-size and engineering properties. Alluvial fan deposits consist predominantly of

					DEEPER	* ROCK
LINE NO.		VELOCITY	VELOCITY DISTRIBUTION FPS (MPS)		REFRACTORS DEPTH VFI OCLTV	EXCLUSION DEPTH TO 7000 FPS
0L-S-1	2700 (823)		3700 (1128)	8)	2	1
DL-S-2	(457) 4000 (1219)	X	4900 (1494)	A	ı	400 (122)
DL-5-4	2600 (792) 4200 (1280)	V A	6900 (2103)	A	1	42 (13)
DL-S-5	960 (293) 🔦 2100 (640)	*	2700 (823)	A	1	420 (128)
01-S-6	2500 (762) - 3600 (1097)	Y A	4700 (1433)	A	225 (69) 9900 (3018)	-
01-5-7	1800 (549)		4300 (1311)	A	170 (52) 10600 (3231)	
01-5-8	1700 (518)	X	2900 (884)	A	-	275 (84)
01-5-9	1900 (579)		3200 (975)	A	160 (49) 12100 (3688)	1
01-2-10	(1900 5 700 (1737)		12400 (3	(3780)	-	
01-5-11	V	3400 (3400 (1036)	▼ 5500 (1676) ▶	135 (41) 8700 (2652)	300 (91)
DL-S-12	▼ 1200 (366) ▼	¥	2400 (732)	A	-	175 (53)
01-5-13	▲1800 (549)►		3900 (1189)	A	ı	235 (72)
DL-S-14	3000 (914)	¥	3800 (1158)	À	150 (46) 7700 (2347)	1
DL-S-15	1500 (457) ~ 2400 (732)		3000 (914)	4)	i	400 (122)
01-5-16	(549) ~ 2900	0 (884)	12	12700 (3871)	1	
01-5-17	1300 (396) 2700 -		4600 (1402)	◄ 12800 (3901)	_	-
					FT (M) FPS (MPS)	FEET (M)
METERS	5 10	15	20 25 30	35 40 45		
FEET	0 5 10 20 30	40 50	60 70 80 90 100 DEPTH INTERVAL	110 120 130 140 150	ē	

* If no refracting interface or layer with a velocity greater than 7000 fps (rock/rock-like material) was detected, a rock exclusion depth calculation was performed to determine the minimum depth at which rock could occur.

SHALLOW SEISMIC REFRACTION RESULTS
DRY LAKE VALLEY, NEVADA
GREAT BASIN CSP

WX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE

VELOCITY LAYER	COMPRESSIONAL WAVE VELOCITY FPS (MPS)	AVERAGE THICKNESS FT (M)	COMMENTS
1	2600 (792)	90 (27)	PINCHES OUT
2	3300-3900 (1006-1189)	150 (46)	-
3	6000-8200 (1829-2499)	500 (152)	DISCONTINUOUS
4	8200-9000 (2499-2743)	1200 (366)	DISCONTINUOUS
5	14,000-16,000 (4267-4877)	UNKNOWN	BASEMENT

LINE DL-DS-1

VELOCITY LAYER	COMPRESSIONAL WAVE VELOCITY FPS (MPS)	AVERAGE THICKNESS FT (M)	COMMENTS
1	2800 (853)	60 (18)	-
2	3900 (1189)	150 (46)	-
3	6600-7400 (2012-2256)	300 (91)	DISCONTINUOUS
4	9000-9300 (2743-2835)	700 (213)	-
5	14,000-16,000 (4267-4877)	UNKNOWN	BASEMENT

LINE DL-DS-2

DEEP SEISMIC REFRACTION RESULTS
DRY LAKE VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FURCE SAMSO

TABLE

VELOCITY DISTRIBUTION FPS (MPS) WAVE TYPE	■ 3760 (1146) ■ P WAVE		P WAYE	6) 980 (299) S WAVE		20 25 30 35 40 45	OTH INTERVAL	
VELOCITY D	2800 (853)	1980 (604)	2050 (625)	980 (299) 🕶 1200 (366)	,	5 10 15 10 15 20 30 40 50 80		
DOWNHOLE Survey no.	01-07-7	€1400 (427)	01-07-18	540 (165)		METERS 0		

ENGINEERING AND GEOPHYSICAL PROPERTIES	Intermediate and younger alluvial fan deposits (A5i and A5y)	Playa deposits (A4
UNIFIED SOIL CLASSIFICATION SYMBOL(S)	SM, SW, SP, SC, GP, GM, GW	CH, MH, ML, SM
GENERAL PROPERTIES		<u> </u>
DRY DENSITY pcf(kg m ³)	79-120 (1265-1922)	70-94 (1121-1506
MOISTURE CONTENT (%)	0.2-27.7	10-42
DEGREE OF SATURATION (**)	18-75	28-95
SPECIFIC GRAVITY	2.64-2.67	2.61±
DESREE OF CEMENTATION	None to moderate	None to weak
COMPRESSIONAL WAVE VELOCITIES fps(mps)	1240-4870 (378~1484)	1000-4700 (305-143
ELECTRICAL CONDUCTIVITY (mhos m)	DNA	DNA
GRAIN SIZE DISTRIBUTION (%)		
BOULDERS 12 inches(30cm)	0-5	0
COBBLES 3 to 12 inches(8to 30cm)	0-12	0
GRAVEL	0-70	0
SAND	25-98	0-79
SILT AND CLAY	0-48	21-94
PLASTICITY DATA		
LIQUID LIMIT	21-23	27-108
PLASTICITY INDEX	NP-11	NP-60
COMPRESSIBILITY DATA		
COMPRESSION AT 4 ksf(192kn/m²) (%)	1-5	1 0-2 6
SWELL OR COLLAPSE UPON SATURATION (%)	0.5-1.8 (Swell)	0.8-2.8(Swell)
SHEAR STRENGTH DATA		
UNCONFINED COMPRESSION ksf(kn m²)	3.3-4.1 (158-196)	2 9-5 4 (139-259)
CD TRIAXIAL COMPRESSION	$c = 0-6$ ksf (207 kN m ²), $\phi = 33-40$	c=0-4 ksf (192 kN m ²).¢
DIRECT SHEAR ksf(kN m ²)	3.7-8.2 (177-393)	DNA
COMPACTION AND CBR DATA		
MAXIMUM DRY DENSITY pcf(kg m ³)	124.0-128.5 (1986-2058)	110.8±(1775±)
OPTIMUM MOISTURE CONTENT (3)	8.5-10.0	16.5 ±
CBR AT 90% RELATIVE COMPACTION	14-40	3±

DNA=DATA NOT AVAILABLE (INSUFFICIENT DATA OR TESTS NOT PERFORMED)

GEOLO	GIC UNITS			
ya deposits (A4)				
CH, MH, ML, SM				
J-94 (1121-1506)				
10-42				
28-95				
2.61±			 	
None to weak				
D-4700 (305-1433;			 	
DNA				
0		 		
0				
0				
0-79			 	
21-94				
27-108				
NP-60				
0 2 6			 	
8-2.8(Swell)				
1-5 4 (139-259)				
$f(192 \text{ kN m}^2) \neq -20 -32$				
DNA				
1.8±(1775±)				
16.5 ±				
3 ±				

		RANGE GEOPH						
nRV	LAKE	VALLE	Υ.	NEVA	DA.	GREAT	BASIN	CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

TABLE 8

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dense to very dense silty sands and sandy gravels, which are slightly compressible and have moderately high shear strengths. Playa deposits are composed primarily of stiff to very stiff silts and clays, which are moderately compressible and have moderate shear strengths.

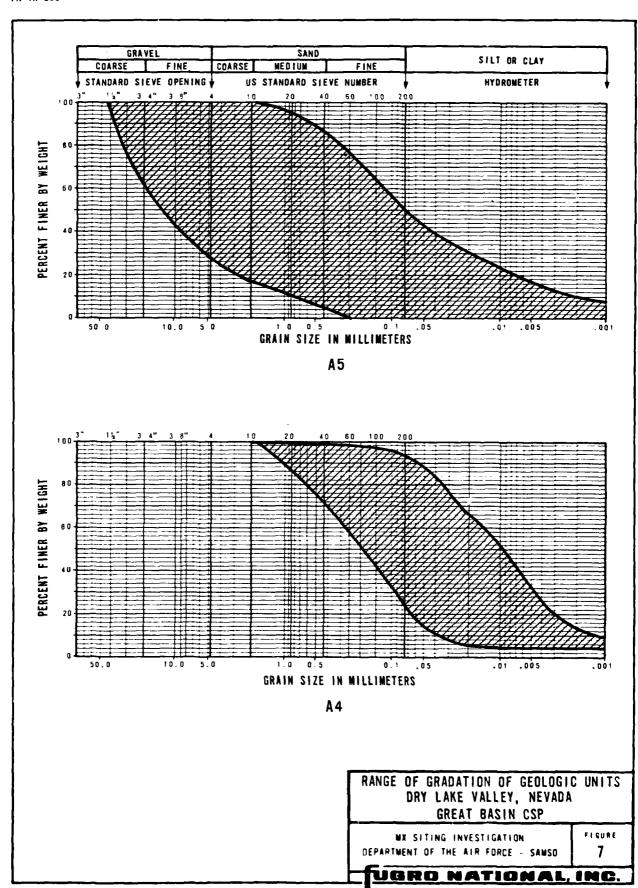
The site soils generally are neither expansive nor collapsible.

Range of gradation of the two geologic units is shown in Figure 7.

Results of chemical tests on soils samples are presented in

Table 9. The test results indicate that sulfate attack of soils on concrete will be "positive" in some areas of the site.

Representative logs of three borings and three trenches from the site are contained in Appendix B. Results of the shear strength and CBR tests performed on soil samples from the site and a summary of all the laboratory tests performed on soil samples obtained from boring DL-B-12 are also included in Appendix B.



TRENCH		SAMPLE	SAMPLE INTERVAL	5			≆	WATER SOLUBLE	'n	CALCIUM
	20.			301L TYPF	吾	800 I UM	CHLORIDE	SULPHATE	CALCIUM	CARBONA TE
2		FEET	METERS			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
01-8-2	SS-4	20.0-21.2	6.10-6.46	WS-MS	6.7	53	9	39	34	85
01-8-4	8-2	14.0-15.0	4.27-4.57	E	7.1	30	33	29	93	233
01-8-5	P-2	10.6-11.3	3.23-3.44	풀			1040	222	37	
	P-3	15.3-15.9	4.66-4.85	橐	7.7	6350	8150	1750	146	365
	P-6	30.0-30.7	9.14-9.36	픛	7.9	3210	4750	936	211	528
	=	80.6-81.3	24.57-24.78	NS.	8.2	1500	1480	675	10	25
01-1-8	8-3	8.0-9.5	2.44-2.90	дS	6.5	155	9/	200	118	295
01-8-12	P-2	10.0-10.7	3.05-3.26	¥	6.9	375	223	620	88	220
	P-30	294.7-295.3	89.82-90.01	Ħ	7.8	521	24	91	41	103
_	B-2	3.0-5.0	0.91-1.52	NS.	7.1	250	219	980	82	205
01-8-19	<u>"</u>	0.0-1.6	0.0-0.49	ĸ	7.9	1000	836	450	36	96

SUMMARY OF CHEMICAL TEST RESULTS DRY LAKE VALLEY. NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION
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TABLE

3.0 RALSTON VALLEY SITE

The Ralston Valley Characterization Site covers an area of 182 nm² (624 km²) in western Nye County, Nevada. The site is bounded by mountain ranges on the east and west, Nellis Bombing and Gunnery Range on the south, and is open to the northern part of Ralston Valley on the north. U. S. Highway 6 and State Highway 8A provide paved highway access through the site while graded roads and four-wheel drive trails provide access within the site.

3.1 SCOPE OF INVESTIGATION

Scope of geologic, geophysical, and soils engineering field activities performed at the site and laboratory tests performed on soil samples from the site are presented in Table 10.

Detailed information about the soils engineering field activities (15 borings and eight trenches) is summarized in Tables 11 and 12.

Locations of all the field activities are shown in Figure 8.

3.2 SURFICIAL GEOLOGY AND TERRAIN

Alluvial fan deposits of younger and intermediate age are the predominant surficial geologic units within the Characterization site (Figure 8). The younger fan deposits cover approximately 23 percent of the area while the intermediate fan deposits cover 18 percent. Undifferentiated non-rock deposits, consisting of fluvial, alluvial, and playa and/or lacustrine deposits cover 24 percent of the area. These non-rock units were not differentiated due to the small scale (1:62,500) of mapping. Playa deposits cover approximately three percent of the surface.

GEOLOGY AND GEOPHYSICS

TYPE OF ACTIVITY	NUMBER OF ACTIVITIES
Geological mapping stations	27
Shallow refraction	15
Deep refraction	2
Downhole velocity	3
Gravity survey	577
Ground magnetic stations	281

ENGINEERING

NUMBER OF BORINGS	NOMINAL DEPTH FEET (METERS)
2	,30 (8)
9	75-100 (23-30)
4	300 (91)
NUMBER OF TRENCHES	NOMINAL DEPTH FEET (METERS)
8	16 (5)

ENGINEERING-LABORATORY TESTS

TYPE OF TEST	NUMBER OF TESTS
Moisture/density	188
Specific gravity	15
Sieve analysis	144
Hydrometer	63
Atterberg limits	32
Consolidation	10

TYPE OF TEST	NUMBER OF TESTS
Unconfined compression	12
Triaxial Compression	2.1
Direct shear	16
Compaction	7
CBR	3
Chemical analysis	8

SCOPE OF FIELD AND LABORATORY
ACTIVITIES

RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
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10

BORING NUMBER	TOTAL DEPTH FEET(METERS)	TYPE OF DRILL RIG USED	TYPE OF SAMPLES* OBTAINED
RY-8-1	300.0(91.4)	Rotary Wash	P. D. SS. B
RV-B-2	27.5(8.4)	Percussion	В
RV-B-3	30.0(9.1)	Percussion	B. SS
RV-B-4	87.0(26.5)	Percussion	В
RV-B-5	101.5(30.9)	Rotary Wash	P, SS, B
RV-B-6	300.5(91.6)	Rotary Wash	P. B
RV-B-7	100.2(30.5)	Rotary Air/Wash	P. D. SS. B
RV-B-8	300.7(91.7)	Rotary Wash	D, P
RV-B-9	100.7(30.7)	Rotary Wash	SS.P
RV-B-10	100.0(30.5)	Percussion	B. \$\$
RV-B-12	101.3(30.9)	Rotary Wash	P.D.B
RV-B-13	301.7(92.0)	Rotary Wash	D. SS. P
RV-B-14	75.0(22.9)	Percussion	В
RV-B-15	82.0(25.0)	Percussion	\$\$.B
RY-B-16	100.0(30.5)	Percussion	B, SS

* P = Pitcher sample (undisturbed)

D = Fugro Drive sample (relatively undisturbed)

B = Bulk sample (disturbed, but representative)

SS = Split Spoon sample (disturbed, but representative)

ENGINEERING FIELD ACTIVITIES - BORINGS RALSTON VALLEY. NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION
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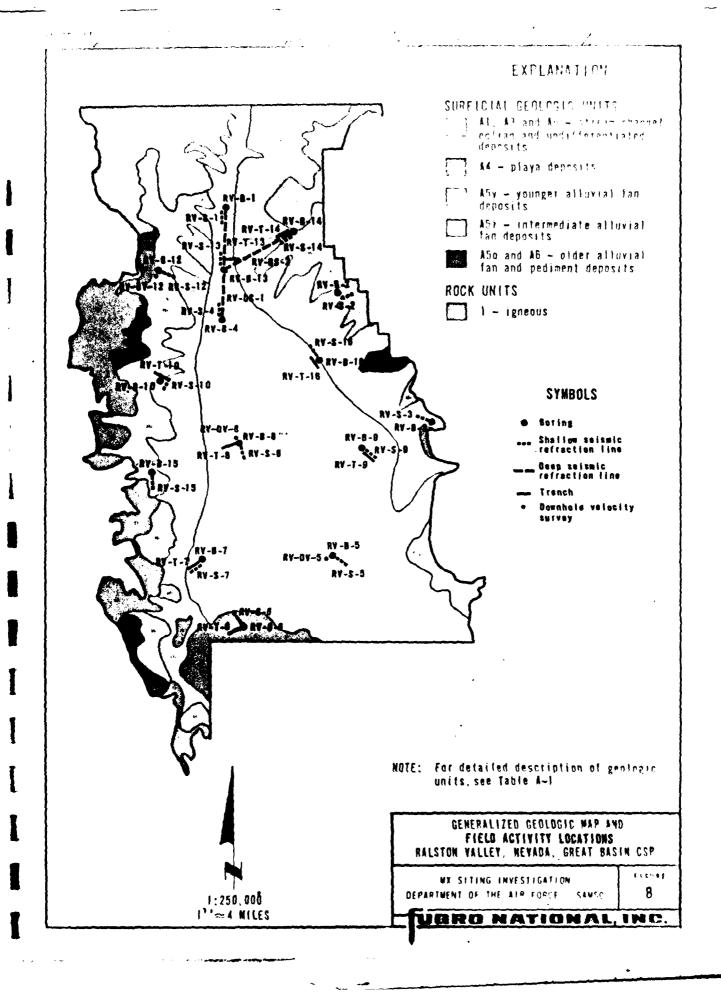
TABLE 11

TRENCH NUMBER	TOTAL DEPTH FEET (METERS)	STABILITY OF VERTICAL EXCAVATION WALLS
RV-T-6	18.0 (5.5)	stable
RV-T-7	18.0 (5.5)	unstable; trench caved in after heavy rain
RV-T-8	18.0 (5.5)	0-9° (0-2.7m) unstable; heavy sloughing into trench
RV-T-9	18.0 (5.5)	D-2° (D-D.6m) unstable; some sloughing 2-18° (D.6-5.5m) stable
RV-T-10	18.0 (5.5)	stable
RV-T-13	18.0 (5.5)	0-6° (0-1.8m) unstable; some sloughing 6-18° (1.8-5.5m) stable
RV-T-14	18.0 (5.5)	O-8° (O-2.4m) unstable; sloughing into trench 8-18° (2.4-5.5m) stable; trench has numerous small caliche layers 3-14° (7.6-35.5cm) thick
RV-T-16	18.0 (5.5)	0-3' (0-0.9m) stable 3-10' (0.9-3.0m) unstable; sloughing into trench 10-18' (3.0-5.5m) stable

ENGINEERING FIELD ACTIVITIES - TRENCHES
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAMSO

1 2



Twenty-one percent of the area consists of mixed playa and undifferentiated non-rock deposits. The large percentage (45%) of the area mapped as undifferentiated non-rock deposits or mixed playa and undifferentiated non-rock deposits is due to the broad, flat topography of the site. Playas located near the valley center and alluvial deposits located between the playa and the mountain front form an interfingering stratigraphic sequence.

Alluvial fan deposits are typically silty sands with gravel, ranging from sandy gravels near the mountain front to sandy silts near the playas. Playa deposits are generally silts. All the surficial geologic units are described in Table 13.

The maximum surface slope is ten percent but typical surface slope is only three percent. Depths of drainage incision (excluding older alluvial fan deposits) range from zero to 15 feet (0-5 m) with typical depths of five feet (1.5 m).

3.3 SUBSURFACE CONDITIONS

3.3.1 Soil Profiles

The soil profiles shown in Figures 9 and 10 illustrate the composition of soils with depth. Silty sands and gravelly sands are the dominant valley soils, and are interbedded with clayey silts near the valley center and sandy gravels near the mountain fronts. Cobbles and boulders are found near the mountain fronts. Cementation of the soils varies with soil type and age, generally increasing with age of soil. Sandy

		THICKNESS		11000	AREAL EXTENT (SITE)		
SURFICIAL GEOLOGIC UNIT (a)	GEOLOGIC AGE	FEET (METERS)	DESCRIPTIVE NAME(S)	SYMBOL(S)	nm ² (km ²)	PERCENT	
Undifferentiated Non-Rock Deposits (Au)	Quaternary- Tertiary	Unknown	Silty Sand with Gravel	SM	45 (154)	24	
Alluvial Outwash Deposits (Alw)	Quaternary	Unknown	Silty Sand. Sand	SM. SP	7 (24)	4	
Lake Terrace Deposits (A21)	Quaternary- Tertiary	Unknown	Silty Sand with Gravel	SM	1 (3)	<1	
Eolian Deposits, Undifferentiated (A3)	Quaternary	0-20 (0-6)	Sand with Gravel	SP	3 (10)	2	
Playa Deposits (A4)	Holocene	Unknown	Silt with Sand and Clay	ML	44 (151)	24	
Younger Alluvial Fan Deposits (A5y)	Holocene	Unknown	Silty Sand with Gravel	SW	41 (141)	23	
Intermediate Alluvial Fan Deposits (A5i)	Pleistocene	Unknown	Gravelly Silty Sand, Sand	SM. SW.	36 (123)	20	
Older Alluvial Fan Deposits (A5o)	Pleistocene	Unknown	Gravelly Silty Sand	SM	5 (17)	3	
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NOTES:

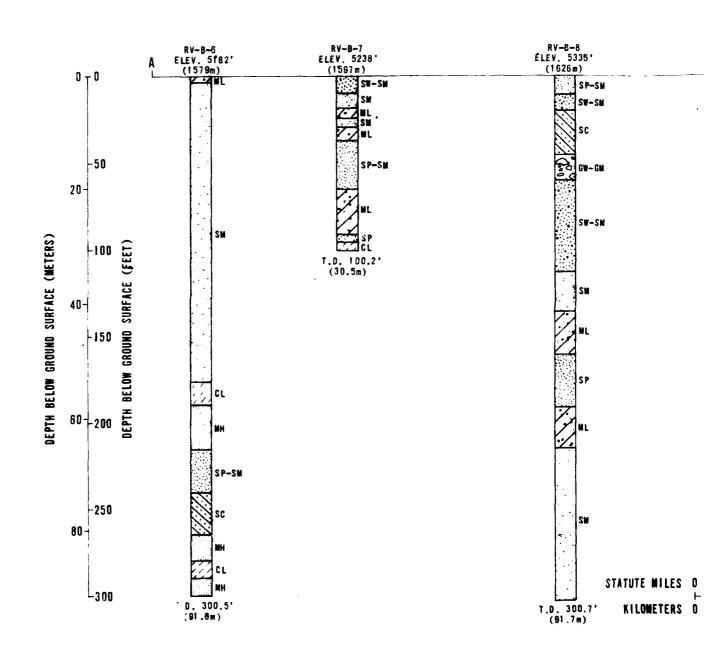
- (a) For generic description of geologic units, see Table A-1.
- (b) For description of USCS, see Table A-2.
- (c) For description of stage of caliche, see Figure A-1.
- (d) Mixed Al, A4, and A5 deposits.
- (a) Consists of mixed A1, A5y and A5i deposits.
- (f) Locally includes gravel, cobbles and boulders derived from upslope rock.
- (g) Includes 21 percent mixed A4 and Au deposits; designated A4 Au on Figures 8 & 11.
- (h) Includes two percent of area underlain by shallow rock, designated A6 on Figures 8 & 11

AREAL EXTE	NT (SITE)		PROPERTIE	S OF SURFACE	MATERIALS		SURFACE I	MORPHOLOGY	\prod
nm ² (km ²)	PERCENT	GRADATION	CEMENTATION	MAXIMUM GRAIN SIZE	PAVEMENT/ PATINA	STAGE OF Caliche (c)	SLOPE (PERCENT)	DRAINAGE DEPTHS FEET(METERS)	NOTES
45 (154)	24	Poor- Well	None- Moderate	Cobbles	None-Well/ None-Well	None - III	< 1-10	0-25 (0-8)	(d)
7 (24)	4	Poor- Moderately well	Weak- Moderate	Boulders	None-Fair/ None-Fair	None-∐	0-5	0-10 (0-3)	(e)
1 (3)	<1	Moderately well	Weak	Gravel	None-Fair/ None-Fair	None-I	1-5	0-2 (0-0 6)	
3 (10)	2	Poor	None-Weak	Cobbles	None/ None	None-I	0-10	0-5 (0-1 5)	(f)
44 (151)	24	Poor	None-Weak	Sand	None/ None	None-I	< 1	0-2 (0-0.6)	(g)
41 (141)	23	Poor-Well	None-Weak	Cobbles	None-Poot/ None-Poor	None-I	0-5	0-3 (0-1)	
36 (123)	20	Poor-Well	Weak- Moderate	Boulders	Poor-Well/ None-Fair	п	1-10	2 -1 5 (0.6-5)	(h)
5 (17)	3	Moderately well-Well	Moderate- Strong	Boulders	Poor-Well/ Poor-Well	ш	5-10	5-25 (1.5-8)	
		,							

DESCRIPTION OF SURFICIAL
GEOLOGIC UNITS
RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

13



NOTES: 1. T.D.= Total Depth

 Soil types shown adjacent to soil column are based on Unified Soil Classification System (USCS) and are explained in the appendix

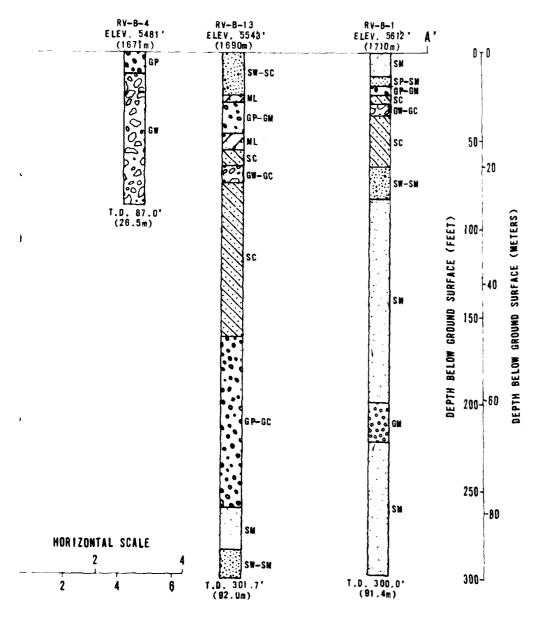
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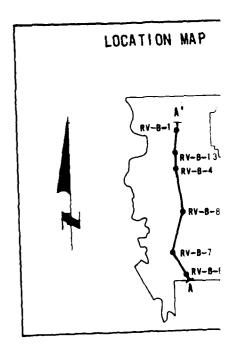
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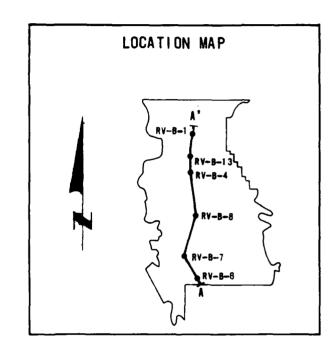




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SOIL PROFILE AA'
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

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150-

DEPTH BELOW GROUND SURFACE (METERS)

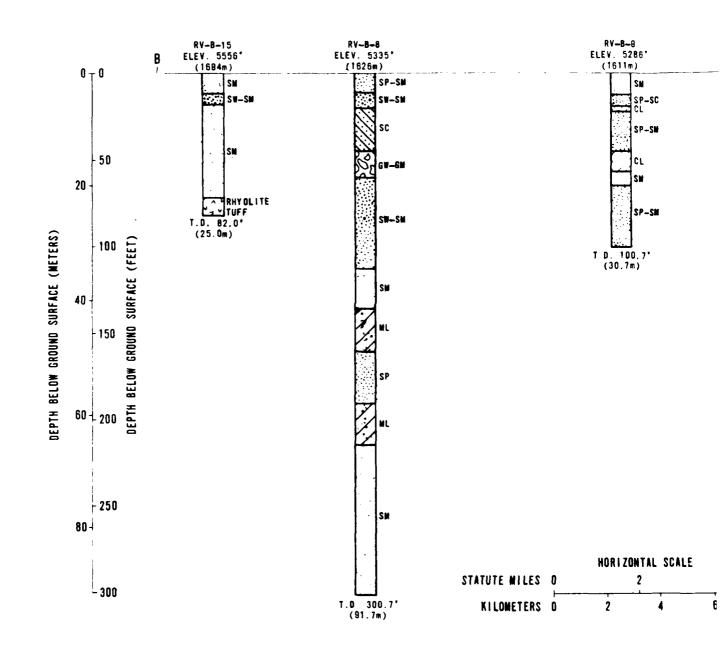
.

200-60

250-

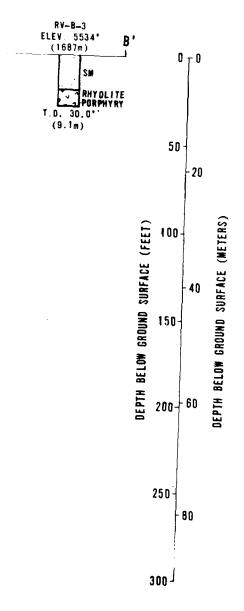
-80

300-

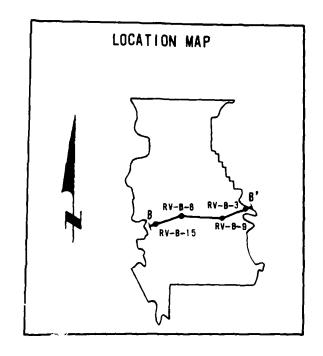


NOTES: 1. T.D. = Total Depth

2. Soil types shown adjacent to soil column are based on Unified Soil Classification System (USCS) and are explained in the appendix.



ALE



SOIL PROFILE BB'
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

FIGURE 10

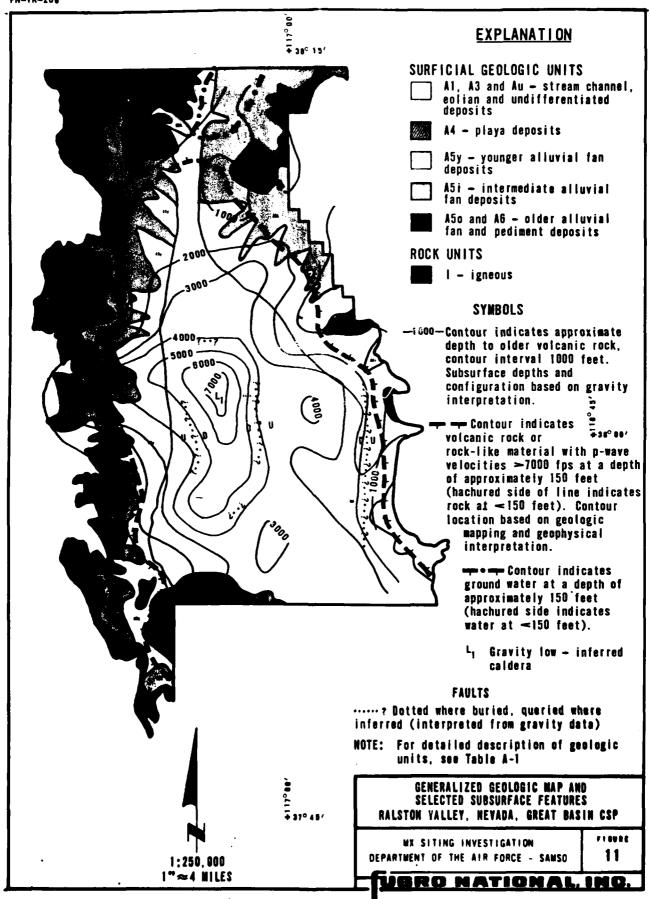
VERO NATIONAL INC

soils with less than five percent fines were generally uncemented to weakly cemented, often caving in unshored trenches.

Depth to Shallow (<150 ft; <46 m) Rock and Water 3.3.2 Figure 11 shows the portion of the Ralston Valley site in which rock (seismic velocity greater than 7000 fps; 2134 mps) and water are estimated to be within a depth 150 feet (46 m) below the ground surface. The portion of shallow rock area is approximately 15 percent of the site area. This analysis is based on data and interpretation from borings, seismic surveys, gravity surveys, surface outcrops, topography, and geologic maps. Depth to ground water is generally greater than 200 feet (61 m) below the surface except for an area near the northern site boundary (location of Tonopah well field used for domestic water supply) where ground-water levels range from 10 to 150 feet (3 to 46 m). The east-west ground-water barrier in this northern area does not show on the gravity contour map, and may represent interfingering of volcanic units and/or basin-fill deposits or an east-west trending intrusive body. Data in the Ralston site south of the Tonopah well field are from four wells and regional information.

3.3.3 Basin Configuration

The basin configuration was interpreted using deep seismic refraction, gravity and ground magnetic survey data. Deep seismic data indicate interbedding of the basin-fill deposits and/or volcanic rock units. The greatest depth to bedrock is approximately 7400 feet (2257 m) below the surface in



4 .

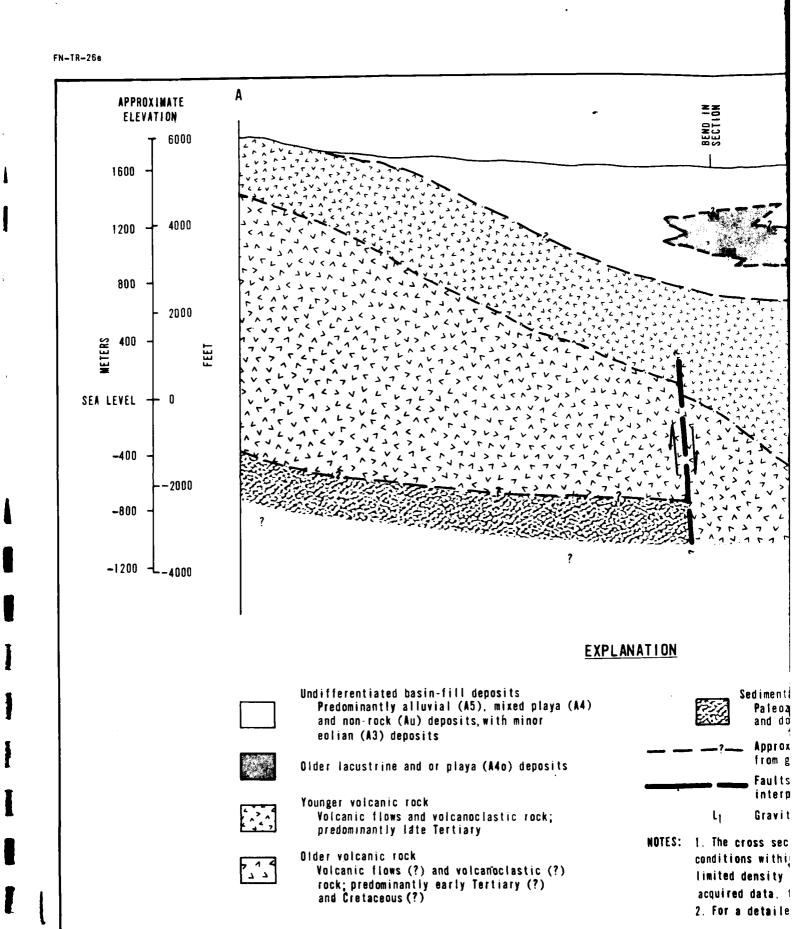
the area of L1 (Figure 11) along the generalized geologic cross-section (Figure 12). Cretaceous and early Tertiary volcanic rocks are the predominant bedrock unit defined in the gravity contour map. The basin is bounded on the east by steep gradients in basement topography typical of those associated with normal faults. No basement rocks are present at the surface west of this fault and a pediment is inferred east of the fault. The basin center is interpreted as a collapsed caldera overlain by younger volcanic rocks and basin-fill deposits (Figure 12). The subsurface basin configuration is illustrated in Figures 11 and 12.

3.4 GEOPHYSICAL PROPERTIES

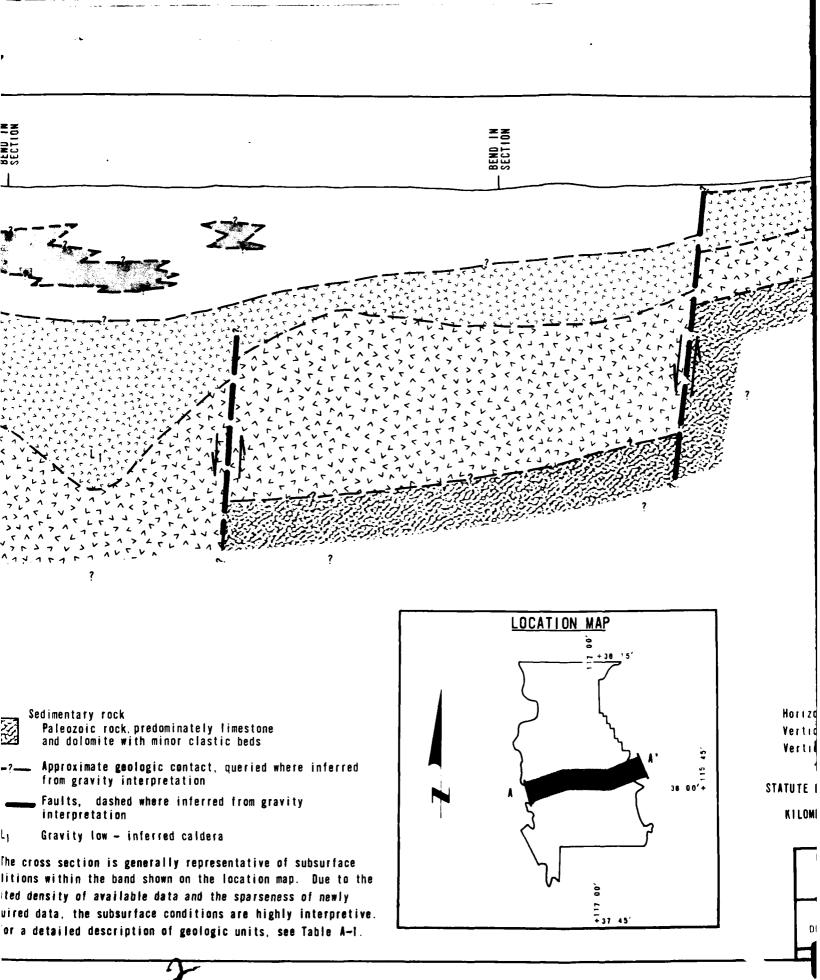
Results of shallow and deep seismic refraction surveys and downhole velocity surveys are presented in Tables 14, 15, and 16. Shallow seismic refraction results (Table 14) indicate a low velocity surficial layer overlying a zone of higher velocity horizons. Borings adjacent to the lines indicate that the change in velocity is probably due to increased consolidation of the soil and not due to a change in lithology. Deep seismic refraction results (Table 15) indicate the bedrock depth within the valley. The compressional wave velocities from downhole velocity surveys (Table 16) do not correspond with those from shallow seismic refraction (Table 14) due to the anisotropy of the ground and method of measurement.

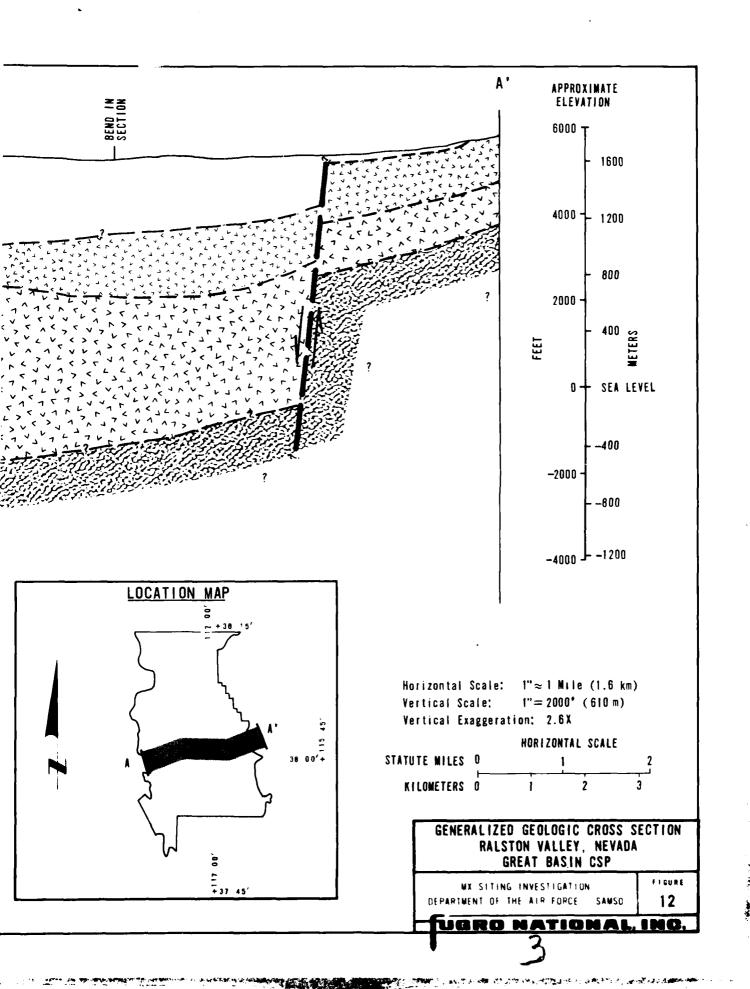
3.5 ENGINEERING PROPERTIES

Laboratory tests were performed to determine the engineering properties of soil samples obtained from the various geologic



[:





SFISMIC										DEEPER REFPACTORS	* ROCK Exclusion:
LINE NO.		ļ		VELOCI	VELOCITY DISTRIBUTION FPS (MPS)	PS (MPS)				DEPTH VELOCITY	DEPTH TO 7000 FPS (2134 MPS)
RV-S-1	1150	2800 (853)	}		4	4100 (1250)			A	ı	550 (168)
RV-S-2	1500 (457)	3300 (1006)	(900	X		6900 (2103)	3)		A	ì	44 (13)
RVS-3	1600 (488)	¥			5000 (1524)	4)	 - - -		A	160 (49) 1300 (3444)	-
RV-S-4	1300 (396)				3200 (975)				A	ı	510 (155)
RV-S-5	1250 (381)				2300 (701)				A	200 (61) 7400 (2556)	_
RV-S-6	V				1500 (457)				A	ı	300 (81)
RV-S-7					2700 (823)				A	1	300 (91)
RV-S-8	1400 (427)				3100 (945)	45)			A	,	250 (76)
RV-S-9	1350 (411)				2500 (762)				A	-	280 (86)
RV-S-10	1100 (335)				2700 (823)	()			A	,	450 (137)
RV-S-12	1400 (427)				4000 (1219)	1219)				ı	500 (152)
RV-S-13	1350 (411)				2200 (671)	(A	ı	435 (133)
RV-S-14	1600 (488)	6	3300 (1006)	(9(X	8100 ((2469)		A	ı	ı
RV-S-15	1300 (396)				2900 (884)	84)			A	ı	240 (73)
RV-S-16	900 (274)				2200 (671))			A	200 (61) 7000 (2134)	
		:		·						FT (M) FPS (MPS)	FEET (M)
METERS 0		- 2 - 2	=	₽-	20 25	30	35	40	45		
. 0	. s.	0 2 0	30 4	40 50	60 70 80 Depth interval	001	110 120	130 140	150		

* If no refracting interface or layer with a velocity greater than 7000 fps (rock/rock-like material) was detected, a rock exclusion depth calculation was performed to determine the minimum depth at which rock could occur. SHALLOW SEISMIC REFRACTION RESULTS
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

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TABLE 14

VELOCITY LAYER	COMPRESSIONAL WAVE VELOCITY FPS (MPS)	AVERAGE THICKNESS FT (M)	COMMENTS
1	2600-3100 (792-945)	100 (30)	-
2	4000-5200 (1219-1585)	300 (91)	-
3	7700-8500 (2347-2591)	400 (122)	_
4	10,500-11,300 (3200-3444)	1200 (366)	-
5	13,600 (4145)	2800 (853)	-
6	18,800 (5730)	UNKNOWN	BASEMENT

LINE RV-DS-1

VELOCITY LAYER	COMPRESSIONAL WAVE VELOCITY FPS (MPS)	AVERAGE THICKNESS FT (M)	COMMENTS
1	2500-3200 (762-975)	50 (15)	-
2	4500-5100 (1372-1554)	300 (91)	PINCHES OUT
3	7300 (2225)	200 (61)	PINCHES OUT
4	10,700 (3261)	500 (152)	_
5	13,600 (4145)	2300 (701)	-
6	18,800 (5730)	UNKNOWN	BASEMENT

LINE RV-DS-2

DEEP SEISMIC REFRACTION RESULTS
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

TABLE 15

WAVE TYPE	P WAVE	SWAVE	P WAVE	S WAVE	P WAVE	S WAVE	ų	4]	0 150			
			Ā	A			9	₹ +	20 130 140			
								-	100 110 120			
I FPS (MPS)	A	A	4000 (1219)	2460 (750)		A		_ _ _	90	VAL.		
VELOCITY DISTRIBUTION FPS (MPS)	2250 (686)	1420 (433)	4	2460	4400 (1341)	3000 (914)		≅	50 60 70	DEPTH INTERVAL		
VE			X A E		A (101) 00	1600 (488)	:	⊒	30 40			
	1730 (527)	1100 (335)	2020 (616)	128	1800 - 2300 (7 (549) - 2300 (7	V		~ } -	5 10 20			
DOWNHOLE SURVEY NO.	y	7	1500	RV-DV-8 940 (287		01 10-11 10-11 10:01 10:			FEET 0			
						D		STO	N V	ITY SUR ALLEY, BASIN	NEVA	JLTS

units. Laboratory analysis consisted of classification tests, consolidation tests, shear strength tests, compaction and CBR tests, and chemical tests. Table 17 presents the range of engineering properties and compressional wave velocities of predominant geologic units.

Younger and intermediate alluvial fan deposits are combined into one unit since they have similar grain-size and engineering properties, and could not be differentiated at depth. These deposits consist predominantly of dense to very dense silty sands and sandy gravels, which are slightly compressible and have moderately high shear strengths. Playa deposits are composed primarily of stiff to very stiff silts and clays, which are moderately compressible and have moderate shear strengths.

In general, the site soils are neither expansive nor collapsible. Figure 10 shows the range of grandflow of the geologic entry. Table 18 shows the results of chemical tests on soil samples, which indicate that sulfate attack of soils on concrete will be "positive" in some areas of the site.

Representative logs of three borings and three trenches from the site are contained in Appendix C. Shear strength and CDR test results, as well as a summary of all the laboratory tests performed on soil samples obtained from boring RV-B-6, are also included in Appendix C.

ENGINEERING AND	Intermediate and vounger alluvial	2 24 744
GEOPHYSICAL PROPERTIES	intermediate and younger alluvial fan deposits (A5) and A5y)	Playa deposits (A4,
UNIFIED SOIL CLASSIFICATION SYMBOL(S)	SW. SP. SH. GP. GM	ML CL. MH. SP SM
GENERAL PROPERTIES		
DRY DENSITY pcf(kg m ³)	86-118 (1378-1890)	75-107 (1201-1714
MOISTURE CONTENT (%)	1-22	6-40
DEGREE OF SATURATION (%)	42-74	21-90
SPECIFIC GRAVITY	2 54-2 60	2.56-2 59
DEGREE OF CEMENTATION	Uncemented to moderate	Uncemented to weak
COMPRESSIONAL WAVE VELOCITIES fps(mps)	1000-6900 (305-2103)	1340-5700 (408-1737)
ELECTRICAL CONDUCTIVITY (mhos m)	DNA	DNA
GRAIN SIZE DISTRIBUTION (%)		
BOULDERS >12 inches(30cm)	0-1	0
COBBLES 3 to 12 inches(8to 30cm)	0-8	0
GRAVEL	0-61	0
SAND	25-86	13-88
SILT AND CLAY	5–33	12-87
PLASTICITY DATA		
LIQUID LIMIT	NP	36-66
PLASTICITY INDEX	NP	MP-30
COMPRESSIBILITY DATA		
COMPRESSION AT 4 ksf (192kn/m²) (%)	DHA	1.4-2.2
SWELL OR COLLAPSE UPON SATURATION (%)	DNA	1.4-2.7 (Swell)
SHEAR STRENGTH DATA		
UNCONFINED COMPRESSION ksf(kn m²)	DNA	2.4-4.3 (155-206)
CD TRIAXIAL COMPRESSION	c=0-8 ksf (383 kN m ²), ϕ =33-39°	$c = 0-4 \text{ ksf (192 kN m}^2), 9$
DIRECT SHEAR ksf(kN m²)	2 7-10.8 (129-517)	1 2-5.2 (57-249)
COMPACTION AND CBR DATA		
MAXIMUM DRY DENSITY pcf(kg m ³)	118-122 (1890-1954)	DNA
OPTIMUM MOISTURE CONTENT (%)	9.8-11.5	DNA
CBR AT 90% RELATIVE COMPACTION	15 -40	DNA

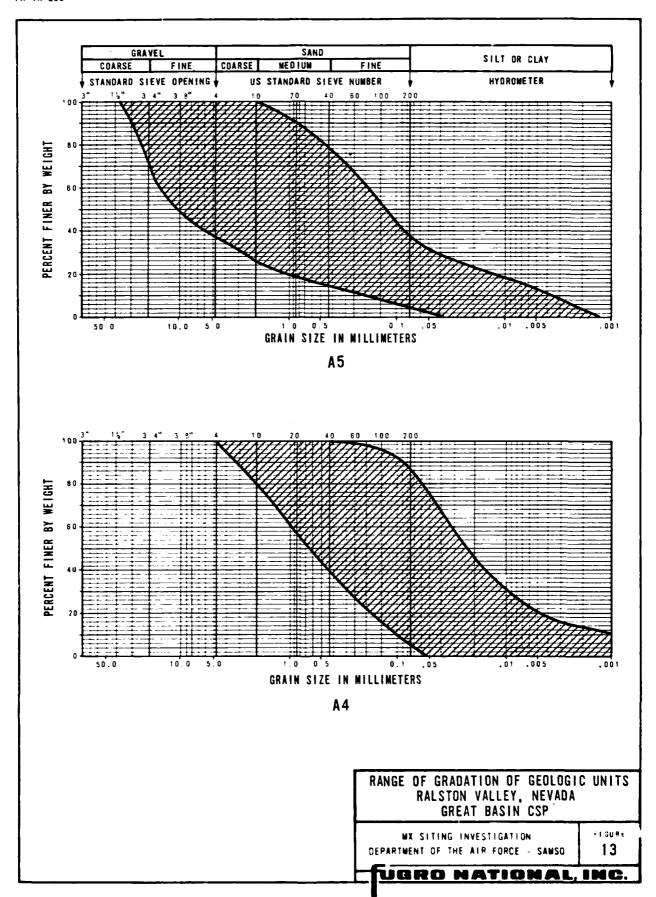
DNA = DATA NOT AVAILABLE (INSUFFICIENT DATA OR TESTS NOT PERFORMED)

GEO	OGIC UNITS
Playa deposits (A4)	
ML. CL MH. SP. SM	
75-107 (1201-1714)	
6-40	
21-90	
2.56-2.59	
Uncemented to weak	
340-5700 (408-1737)	
DNA	
————————————————————————————————————	
0	
0	
0	
13-88	
12-87	
36-66	
!!P-30	
1.4-2.2	
1.4-2.7 (Swell)	
2.4-4.3 (155-206)	
sf (192 kN m ²), $\phi = 20$	4"
1 2-5 2 (57-249)	
Dua	
DNA	
DNA	
DNA	

RANGE OF ENGINEERING AND GEOPHYSICAL PROPERTIES RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
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_		SAUDIE INTERVAL	į			*	WATER SOLUBLE	Ē	CALCIUM
TRENCH SAMPLE	į		TYPE	盂	MOIOOS	CHLORIDE	SULPHATE	CALCIUM	CARBONATE
NO	FEET	METERS			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
RV-8-5 P-3	15.0-15.8	4.57-4.82	NS	B. -	110	6.2	276	=	25
RV-8-6 P-4	20.0-20.7	6.10-6.31	ď	7.7	105	19	84	<u></u>	25
RV-T-6 B-2	5.0-6.5	1.52-1.98	₹	7.4	1100	741	1480	88	220
RV-T-7 B-1	0.0-0.5	0.00-0.15	¥	7.0	650	127	88	144	360
RV-T-8 B-2	2.5-4.5	0.76-1.37	ďS	7.6	125	238	825	12	180
RY-B-9 SS-2	10.0-10.2	3.05-3.11	35	7.6	125	110	166	51	128
RV-T-10 B-2	5.0-6.0	1.52-1.83	SP-SM	7.8	840	437	1380	52	130
RV-B-15 SS-2	14.0-15.0	4.27-4.57	NSMS	7.7	183	133	41	5	12
_									

SUMMARY OF CHEMICAL TEST RESULTS RALSTON VALLEY, NEVADA GREAT BASIN CSP

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DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 18

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4.0 SACRAMENTO VALLEY_SITE

The Sacramento Valley Characterization Site covers an area of 360 nm² (1235 km²) southwest of Kingman in western Mojave County, Arizona. The site consists of two contiguous valleys, the Sacramento Valley to the east and the Mojave Valley to the west. The Sacramento Valley site is bounded by State highway 68 on the north, by the Hualapai Mountains and longitude 114 00' W. on the east, and the Black and Mojave Mountains on the west and south. The Mojave Valley area was found unsuitable after preliminary field investigations and, except for the surficial geology map, the area is not considered in this report. Paved highway access is provided by State highway 68, Interstate 40, and the Kingman-Oatman Road. Graded roads and four-wheel drive trails are also present within the site.

4.1 SCOPE OF INVESTIGATION

Scope of geologic, geophysical, and soils engineering field activities performed at the site and laboratory tests performed on soil samples from the site is presented in Table 19. Detailed information about the soils engineering field activities (11 borings and eight trenches) is summarized in Tables 20 and 21. Locations of all the field activities are shown in Figure 14.

4.2 SURFICIAL GEOLOGY AND TERRAIN

Alluvial fan deposits of intermediate age are the predominant surficial geologic unit at the site, covering approximately
74 percent of the area. Of this amount, 17 percent is covered by a thin (generally less than 20 feet; 6 m) veneer of younger

GEOLOGY AND GEOPHYSICS

TYPE OF ACTIVITY	NUMBER OF ACTIVITIES
Geological mapping stations	37
Shallow refraction	14
Conductivity	14
Gravity survey	600

ENGINEERING

NUMBER OF BORINGS	NOMINAL DEPTH FEET (METERS)
6	50 (15)
4	100 (30)
1	300 (91)
NUMBER OF TRENCHES	NOMINAL DEPTH FEET (METERS)
3	6 (2)
5	11 (3)

ENGINEERING-LABORATORY TESTS

TYPE OF TEST	NUMBER OF TESTS
Moisture/density	117
Specific gravity	4
Sieve analysis	44
Hydrometer	3
Atterberg limits	5

TYPE OF TEST	NUMBER OF TESTS
Triaxial compression	9
Direct shear	15
Compaction	2
CBR	2
Chemical analysis	6

SCOPE OF FIELD AND LABORATORY
ACTIVITIES
SACRAMENTO VALLEY, ARIZONA, GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAMSO

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ugro national, inc.

BORING NUMBER	TOTAL DEPTH FEET (METERS)	TYPE OF DRILL RIG USED	TYPE OF SAMPLES* OBTAINED
SV-B-1	100.0 (30.5)	Rotary Wash	P, D, B
SV-B-3	50.4 (15.4)	Hollow Stem Auger	D, B
SV-B-4	50.5 (15.4)	Rotary Wash	D
SV-B-5	101.3 (30.9)	Rotary Wash	P, D, B
SV-B-6	50.2 (15.3)	Hollow Stem Auger	D , B
SV-8-7	101.0 (30.8)	Rotary Wash	D, B
SV-B-8	50.5 (15.4)	Hollow Stem Auger	D,B
SV-B-10	50.0 (15.2)	Rotary Wash	D
SV-B-11	50.7 (15.5)	Hollow Stem Auger	D, B
SV-B-12	302.5 (92.2)	Rotary Wash	P, D, B
SV-B-14	100.0 (30.5)	Rotary Wash	0,8

*P = Pitcher Sample (undisturbed)

D = Fugro Orive Sample (relatively undisturbed)

B = Bulk Sample (disturbed, but representative)

ENGINEERING FIELD ACTIVITIES - BORINGS SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

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TABLE 20

UGRO NATIONAL, INC.

TRENCH NUMBER	TOTAL DEPTH FEET(METERS)	STABILITY OF VERTICAL EXCAVATION WALLS AND REMARKS
SY-T-2	12.0 (3.7)	0-12° (0-3.7m) stable
S - T- Y S	5.9 (1.8)	0-5.9° (0-1.8m) stable; cemented layer at 5.9° (1.8m); backhoe* could not excavate the cemented layer
SY-T-4	12.0 (3.7)	0-3.4' (0-1.0m) stable; stage I caliche layer at 1.4-3.4' (0.4-1.0m) 3.4-6.0' (1.0-1.8m) unstable 6.0-12.0' (1.8-3.7m) stable
8 - T-¥2	10.5 (3.2)	0-8.0° (0-2.4m) unstable 8.0-10.5° (2.4-3.2m) stable; stage I to stage II caliche layer; cementation at 10.5° (3.2m) exceeded capacity of backhoe*
SV-T-7	11.0 (3.4)	0-11' (0-3.4m) stable; stage I to stage II caliche 2.5-11.0' (0.8-3.4m)
01-T+V2	12.0 (3.7)	0-2.5° (0-0.8m) unstable 2.5-12.0° (0.8-3.7m) stable; stage I caliche layer at 2.5-10.0° (0.8-3.0m); stage II caliche layer at 10.0-12.0° (3.0-3.7m)
SV-T-11	6.4 (2.0)	O-1.0° (O-0.3m) unstable 1.0-6.4° (O.3-2.0m) stable; cementation at 6.4° (2.0m) exceeded capacity of backhoe*
SV-T-12	6.7 (2.0)	O-6.7° (O-2.0m) stable; stage II caliche layer at 6.7° (2.0m) exceeded capacity of backhoe*

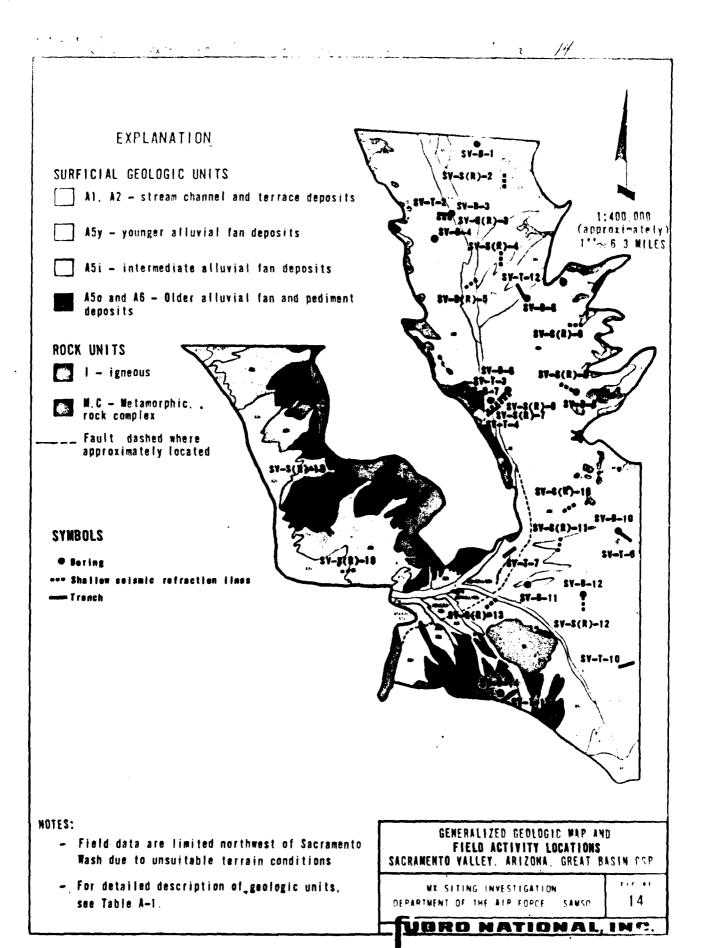
^{*}John Deere 400

ENGINEERING FIELD ACTIVITIES - TRENCHES
SACRAMENTO VALLEY, ARIZONA
GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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alluvial fan deposits. Younger alluvial fan deposits greater than 20 feet (6 m) thick cover another nine percent of the area. The site is characterized by an open drainage system and contains no playa deposits.

The intermediate alluvial fan deposits are typically silty gravelly sands ranging from silty sands to sandy gravels with cobbles and boulders. Younger alluvial fan deposits are generally silty sands with local gravel. The surficial geologic units are described in Table 22.

The maximum surface slope is ten percent with typical slopes of four percent. Depths of drainage incision (excluding older alluvial fan deposits) range from zero to 30 feet (0 to 9 m) with typical depths of ten feet (3 m).

4.3 SUBSURFACE CONDITIONS

4.3.1 Soil Profiles

The composition of soils with depth is illustrated by the soil profiles shown in Figures 15 and 16. The dominant valley soils are silty sands and gravelly sands, which interbed with sandy gravels near the mountain fronts. Cobbles and boulders are occasionally found near the mountain fronts. Cementation of the soils generally increases with age of soil. Sandy soils at shallow depths are generally uncemented to weakly cemented, often caving in unshored vertical trench excavations.

4.3.2 Depth to Shallow (<150 ft; <46 m) Rock and Water

Figure 17 shows portions of the site in which rock (seismic

	THICKNES			4000	AREAL EXTENT (SITE)		
SURFICIAL GEOLOGIC UNIT (a)	GEOLOGIC AGE	FEET (METERS)	DESCRIPTIVE NAME(S)	USCS Symbol(s) (b)	nm ² (km ²)	PERCENT	
Fluvial Deposits (Al)	Holocene	Unknown	Sand	SP	25 (86)	7	
Stream Terrace Deposits (A2s)	Quaternary— Tertiary (?)	Unknown	Gravelly Sand	SP-SM	13 (45)	4	
Younger Alluvial Fan Deposits (A5y)	Holocene	Unknown	Silty Sand	SM	34 (117)	9	
Intermediate Alluviat Fan Deposits (A5i)	Pleistocene	Unknown	Silty Gravelly Sand	SM	264 (905)	74	
Older Alluvial Fan Deposits (A5o)	Pieistocene	Unknown	Sandy Gravel	GW.GP. SM(?)	23 (79)	6	

NOTES:

Area calculations and unit descriptions are from Sacramento Valley proper excluding the area north and west of the designated line shown in Figures 14 and 17

- (a) For generic description of geologic units, see Table A-1.
- (b) For description of USCS symbols, see Table A-2.
- (c) For description of stage of caliche, see Figure A-1.
- (d) Includes four percent Alluvial Outwash deposits (Alw) which consists of mixed Al and A5y or A5i deposits.
- (e) Mapped as A5i(A2s)/A2s on Figures 14 and 17
- (f) Includes seventeen percent A5y/A5i and one percent A6 (areas underlain by shallow rocks) as shown on Figures

EAL EXTE	NT (SITE)		PROPERTIE	S OF SURFACE	MATERIALS		SURFACE	MORPHOLOGY	
1 ² (km ²)	PERCENT	GRADATION	CEMENTATION	MAXIMUM GRAIN SIZE	PAVEMENT/ PATINA	STAGE OF Caliche(c)	SLOPE (PERCENT)	DRAINAGE DEPTHS FEET (METERS)	NOTES
25 (86)	1	Poor	Weak	Boulder	None / None	None-1	< l	0-1 (0-0.3)	(d)
13 (45)	4	Moderate	Strong (Silica)	Cobble	Moderate/ Poor	None	2-6	10-30 (3-9)	(e)
34 (117)	9	Moderately Poor	Weak	Cobble	None-Poor/ None	None-1	1-3	0-5 (0-1.5)	
264 (905)	74	Moderately Poor to Moderately Well	Weak to Moderate	Boulder	Moderate/ None-Well	1-11	2-6	3-30 (1-9)	(f)
23 (79)	6	Moderate to Well	Strong to Very Strong	Boulder	Moderate/ Moderate	11-111	4-10	15-100 (5-30)	
									1

DESCRIPTION OF SURFICIAL
GEOLOGIC UNITS
SACRAMENTO VALLEY, ARIZONA, GREAT BASIN CSP

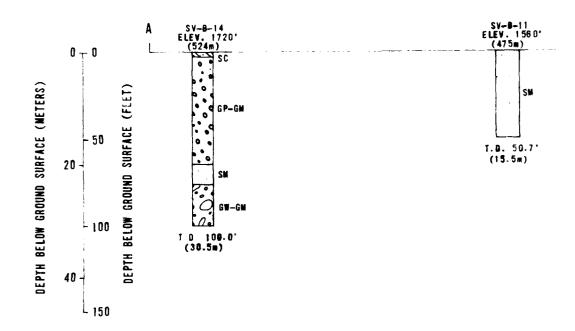
MX SITING INVESTIGATION

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DEPARTMENT OF THE AIR FORCE SAMSO

UGRO NATIONAL, INC.

2



STATUTE MI KILOMETERS

- NOTES: 1. Ground surface elevations shown at locations of borings are approx
 - 2. T.D. = Total Depth
 - 3. Soil types shown adjacent to soil column are based on Unified Soil and are explained in the appendix

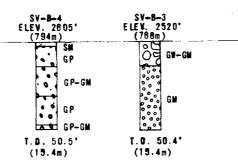
MH-CH T.D. 50.5° (15.4m) SM SW-SW T.B. 101.3'
(30.9m)

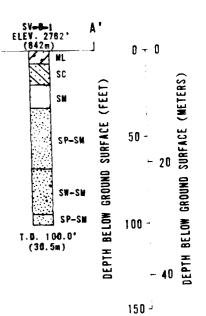
HORIZONTAL SCALE

E MILES TERS

proximate

Soil Classification System (USCS)





LOCATION MAP

SV-B-3

SV-B-4

SV-B-8

SV-B-11

SOIL PROFILE AA° SACRAMENTO VALLEY, ARIZO GREAT BASIN CSP

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SV-B-3
ELEY. 2520'
(768m)
SM (842m)
SC (842m)
SP-SM SP-SM SONOS ONNOS ON

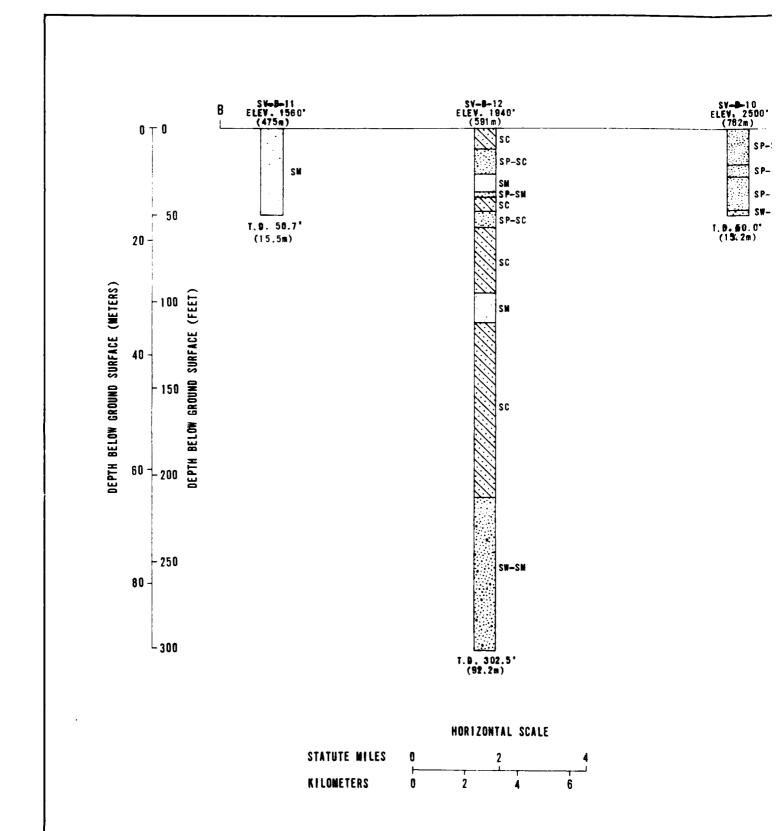
SOIL PROFILE AA° SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

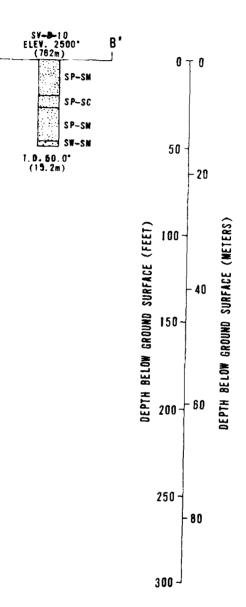
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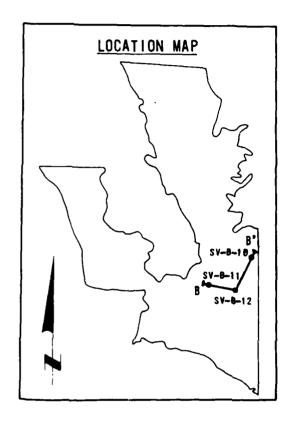
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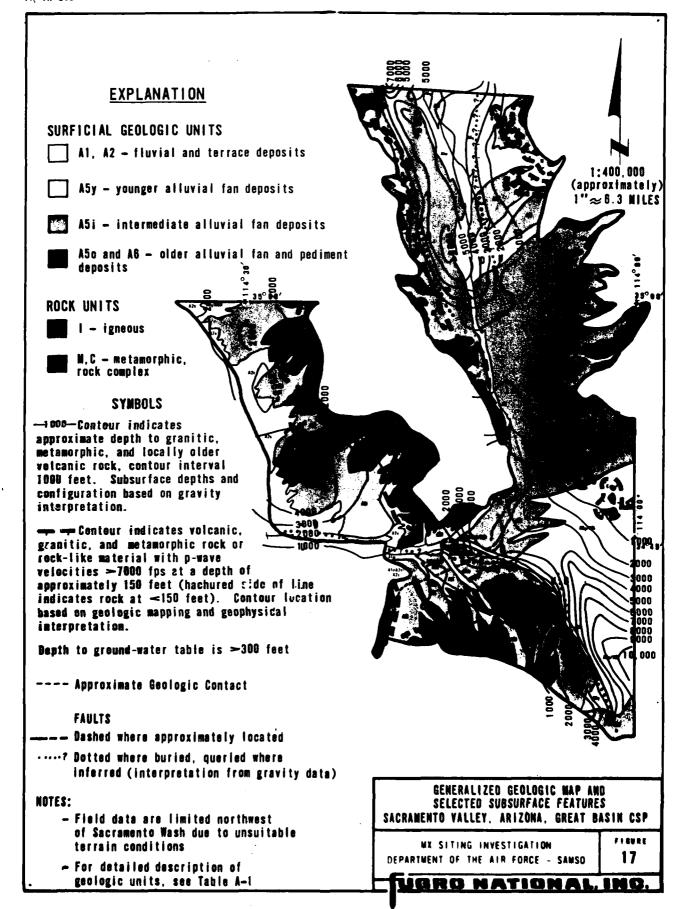
- NOTES: 1. Ground surface elevations shown at locations of borings are approximate
 - 2. T.D. = Yotal Depth
 - Soil types shown adjacent to soil column are based on Unified Soil Classification System (USCS) and are explained in the appendix

SOIL PROFILE BB' SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

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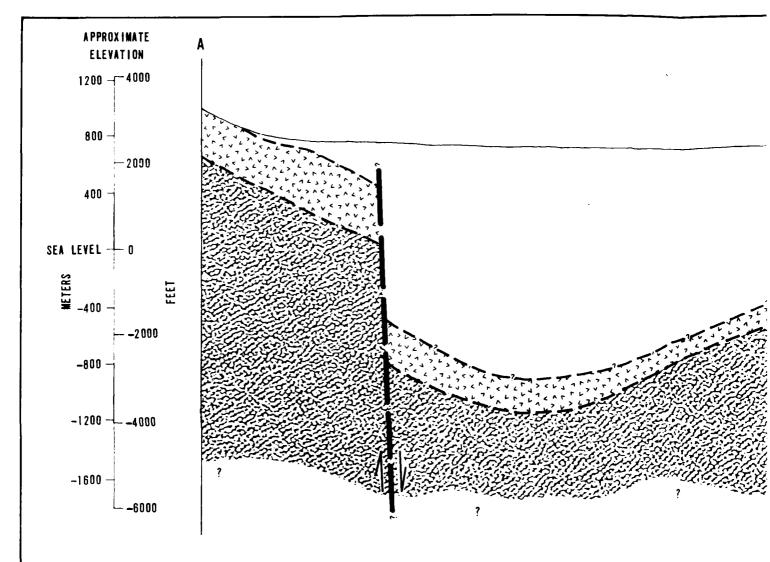
velocities greater than 7000 fps; 2134 mps) is estimated to be encountered within a depth 150 ft (46 m) below the ground surface. This area with shallow rock covers approximately ten to 15 percent of the area. This analysis is based on data and interpretation from borings, seismic surveys, gravity surveys, surface outcrops, topography, and geologic maps. Ground water is nowhere less than 150 feet (46 m) below the surface and generally greater than 300 feet (91 m) based on regional water well data.

4.3.3 Basin Configuration

Data from seismic refraction and gravity surveys were used in interpreting basin configuration. Gravity data indicate greatest depth to basement to be approximately 10,000 feet (3048 m) below the surface near the southeastern boundary of the site (Figure 17). The basement surface on which the gravity is interpreted is probably a Precambrian surface below the basin-fill deposits though locally, this interpretation may be due to a dense volcanic surface. The cross-section (Figure 18) is drawn in the northern part of the site where the depth to basement is only 6000 feet (1829 m). The basin in this area is bounded by gravity gradients similar to those associated with normal faults, with relative movement down on the basinward side. The basin configuration is illustrated in Figures 17 and 18.

4.4 GEOPHYSICAL PROPERTIES

Results of shallow seismic and conductivity measurements are presented in Tables 23 and 24, respectively. Seismic compressionnal wave velocities ranged from 990 to 8540 fps (302 to \$10 r Al



EXPLANATION

1. The cross section is generally representative of subsurface conditions within the band shown on the location map. Due to the limited density of available

NOTES:

data and the sparseness of newly acquired data, the subsurface conditions are highly interpretive.

2. For a detailed description of geologic units see Table A-1.

Undifferentiated basin-fill deposits

Predominantly alluvial (A5) deposits, with fluvial (A1) and stream terrace (A2s) deposits

Volcanic rock

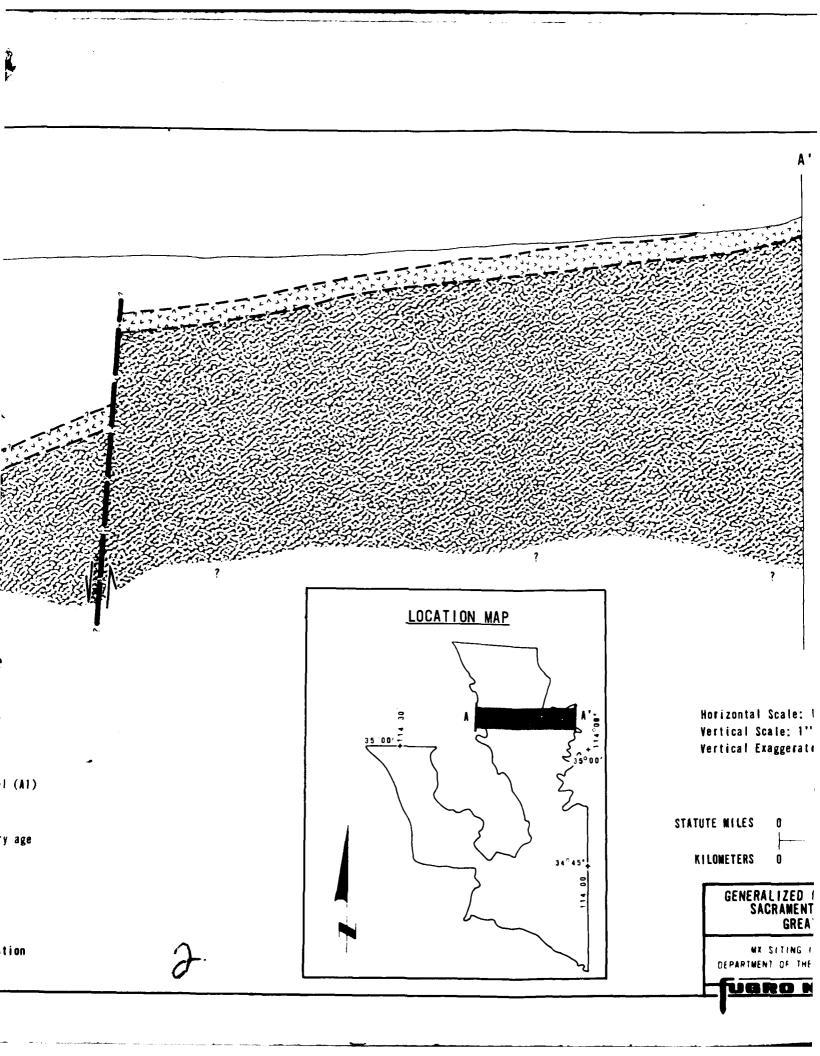
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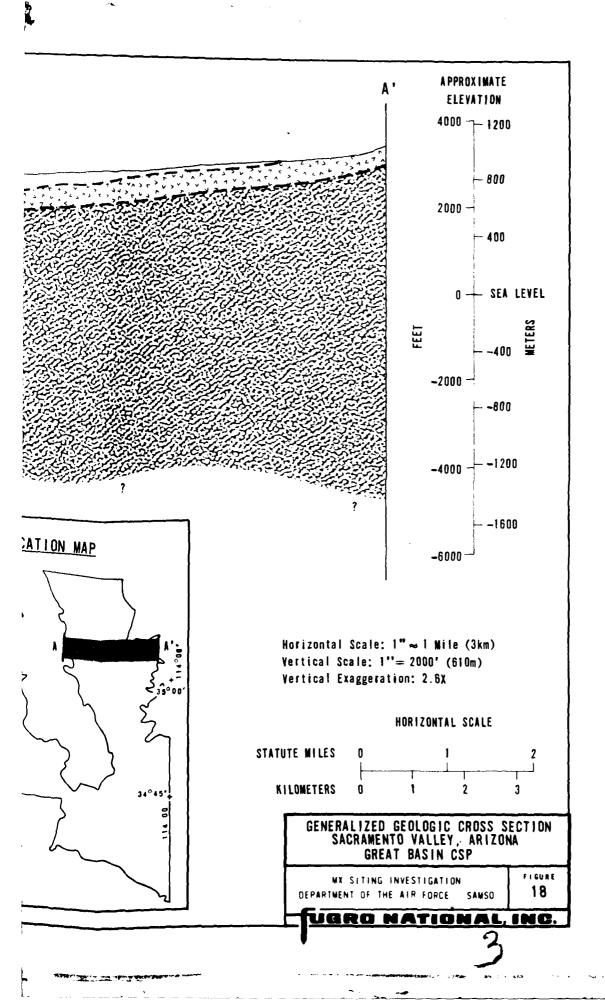
Volcanic flows and volcanoclastic rock of Tertiary age

Precambrian granitic rock

Approximate geologic contact, queried where inferred

Fault, dashed where inferred from gravity interpretation





* ROCK EXCLUSION DEPTH TO 7000 FPS (2134 MPS)	131 (40)	120 (37)	124 (38)	95 (29)	l	ı	116 (35)	122 (37)	131 (40)	144 (44)	142 (43)	121 (37)	149 (45)	132 (40)	FEET (M)			
DEEPER REFRACTORS DEPTH VELOCITY	_	-	1		1	-	-	_	ı	1	1	_	-	ı	FT (M) FPS (MPS)			as detected,
	Å	Å	Å	٨	À	À	Ā	A	A	A	A	Å	A	À		45	0 150	rial) *
					8540 (2603)	01)		4200 (1280)	5980 (1823)				4260 (1298)		e) 1320 (402)	35 40	110 120 130 14	interface or layer with a velocity greater than 7000 fps (rock/rock-like material) was detected, death cornision was neformed to determine the minimum denth at which rock could occur
UTION FPS (MPS)	3490 (1064)	4460 (1359)	(1183)	4750 (1448)	٧	7550 (2301)	(1585)	Ä	X	2820 (860)	2620 (799)	4470 (1362)		4420 (1347)) (d) 1730 (527) (e) 1320 (402)	25 30	80 90 100 Terval	y greater than 7000 of determine the min
VELOCITY DISTRIBUTION FPS (MPS)	34		3880 (1		6670 (2033)	Y	5200 (18	(998)	2880 (878)		2620	i	(963)	٧	(b) 1550 (472) (c) 1650 (503)	15 20	40 50 60 70 80 Depth interval	r layer with a velocit
	2830 (863)	3310 (1009)		1173)	4370 (1332)	3690 (1125)		3170 (26	640)		3120 (951)	475) ~ 3160	3230 (985)	(a) 1440 (439) (b) 1550	5 10	10 20 30	• If no refracting interface or
j	990	<u>e</u>	E	3850 (1173)	∀ ②	(317)	9	\ \ \	1670	2100 (640)	Y	1490 (454)	1560 (475)	2090 (637)	NOTE: (_	. Co	16 10
SEISMIC LINE NO.	SV-S-2	SV-S-3	SV-S-4	SV-S-5	SV-S-6	SV-S-7	SVS-8	SV-S-9	SV-S-10	SV-S-11	SV-S-12	SV-S-13	SV-S-18	SV-S-19	_	METERS 0	FEET 0	*

SHALLOW SEISMIC REFRACTION RESULTS SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

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AVERAGE CONDUCTIVITY (mhos m)**
0.016
0.009
0.007
0.013
0.004
0.015
0.012
0.030
0.005
0.022
0.017
0.008
0.012
0.010

- *Resistivity was determined using a Schlumberger Array at each location where a seismic refraction survey was conducted.
- **Conductivity is the inverse of resistivity. Numbers presented are the average of values determined to a depth of 50 feet, computed as follows:

Average Conductivity = $(c_1t_1+c_2t_2+\ldots+c_nt_n)/50$ feet

Where

 ${\bf C_1} \ \ {\rm through} \ \ {\bf C_n} = {\rm Conductivity} \ \ ({\rm mhos/m}) \ \ {\rm of} \ \ \\ {\rm layers} \ \ 1 \ \ {\rm through} \ \ n$

 t_{1} through $t_{n}\!=\!$ Thickness (feet) of layers $t_{n}\!=\!t_{n}\!+\!t_{n}\!+\!t_{n}\!+\!t_{n}$

CONDUCTIVITY SURVEY RESULTS SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

WE SITING INVESTIGATION TERANTVENT OF THE AIR FORCE SANSO TABLE 24

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2603 mps). The low velocity (2000 fps; 610 mps) surficial layer was less than ten feet (3 m) thick. Velocities greater than 7000 fps or 2134 mps (considered rock) were only observed at depths of 71 and 38 feet (22 and 12 m) at SV-S-6 and SV-S-7, respectively. Average electrical conductivities for the upper 50 feet (15 m) of soil ranged from 0.004 to 0.022 mhos/m. All exceeded the minimum value of 0.004 mhos/m specified in the Fine Screening criteria except at SV-R-6 which was equal to the minimum.

4.5 ENGINEERING PROPERTIES

Engineering properties of the subsoils were determined from laboratory tests. The tests included the following; classification, shear strength, compaction, CBR, and chemical. The range of engineering and geophysical properties of predominant geologic units is presented in Table 25.

Younger and intermediate alluvial fan deposits are combined into one unit since they could not be differentiated at depth. In addition, these two units have similar grain-size and engineering properties. These alluvial fan deposits consist predominantly of dense to very dense silty sands and sandy gravels possessing moderately high shear strengths. Range of gradation of the alluvial fan deposits is shown in Figure 19. Results of chemical tests on soil samples are presented in Table 26. The test results indicate that sulfate attack of soils on concrete will be "positive" in most areas of the site.

Representative logs of three borings and three trenches from the site are contained in Appendix D. Results of the shear strength

ENGINEERING AND GEOPHYSICAL PROPERTIES	Intermediate and younger alluvial fan deposits (A5i and A5y)
UNIFIED SOIL CLASSIFICATION SYMBOL(S)	SM, SC, SP, SW, GP, GM, GW
	3m, 30, 3r, 3m, ur, um, um
GENERAL PROPERTIES	24 100 (4500 0140)
DRY DENSITY pcf(kg m ³)	
MOISTURE CONTENT (')	
DEGREE OF SATURATION (")	15-82
SPECIFIC GRAVITY	2 60-2 73
DEGREE OF CEMENTATION	Uncemented to moderate
COMPRESSIONAL WAVE VELOCITIES fps(mps)	<u> </u>
ELECTRICAL CONDUCTIVITY (mhos m)	0 004-0 022
GRAIN SIZE DISTRIBUTION (%)	
BOULDERS >12 inches (30cm)	0-10
COBBLES 3 to 12 inches (8 to 30cm)	0-26
GRAVEL	2–86
SAND	14-98
SILT AND CLAY	1-39
PLASTICITY DATA	
LIQUID LIMIT	DNA
PLASTICITY INDEX	DNA
COMPRESSIBILITY DATA	
COMPRESSION AT 4 ksf (192 kN m ²) (')	DNA
SWELL OR COLLAPSE UPON SATURATION (%)	DNA
SHEAR STRENGTH DATA	
UNCONFINED COMPRESSION ksf(kn m²)	DNA
CD TRIAXIAL COMPRESSION	$C = 0-2.5 \text{ ksf} (144 \text{ kN/m}^2) \phi = 33 -40$
DIRECT SHEAR ksf(kN m ²)	2 4-10 3 (115-493)
COMPACTION AND CBR DATA	
MAXIMUM DRY DENSITY pcf(kg m3)	119-131
OPTIMUM MOISTURE CONTENT (2)	8 0-11 5
CBR AT 90% RELATIVE COMPACTION	19 ±

DNA = DATA NOT AVAILABLE (INSUFFICIENT DATA OR TESTS NOT PERFORMED)

GEOLOGIC UNIT							
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GEOPHYSICAL PROPERTIES
SACRAMENTO VALLEY, ARIZONA, GREAT BASIN CSP

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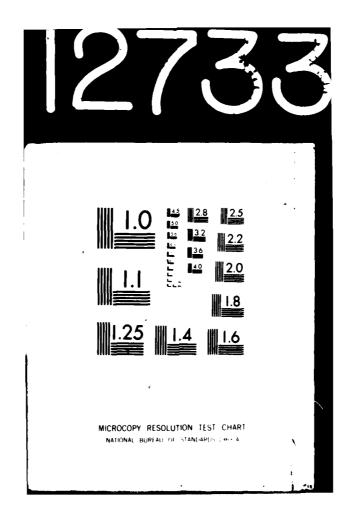
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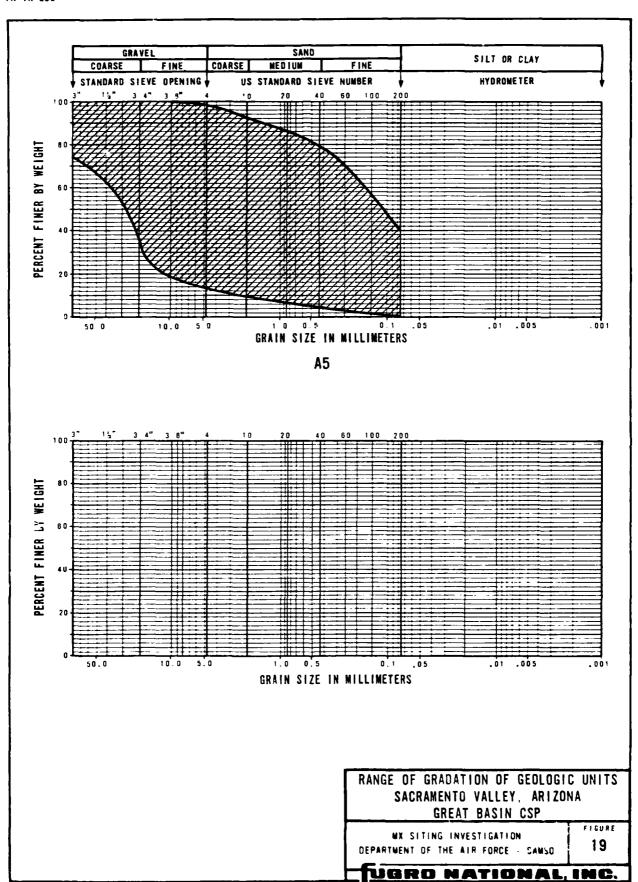
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TABLE

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MX SITING INVESTIGATION. GEOTECHNICAL SUMMARY. PRIME CHARACTERI--ETC(U)
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CALCIUM	CALCIUM CARBONATE mg/kg		504	348	219	508	301	394														
WATER SOLUBLE	CALCIUM	mg/kg	360	340	83	73	1730	130														
	SULPHATE	mg/kg	1520	1880	1220	750	1800	2170														
	CHLORIDE	mg/kg	19	490	260	80	520	360														
	SODIUM	mg/kg	340	1800	520	140	920	600														
	풉		7.5	8.8	7.1	5.9	6.9	6.4														
	SOIL		٦M	HS	MS-MS	SP-SM	SP-SC	M9-d9														
TERVE I	7447	METERS	1.74-1.95	2.96-3.17	3.26-3.47	5.40-5.61	6.31-6.55	4.75-4.88														
SAMPLE INTERVAL		FEET	5.7-6.4	9.7-10.4	10.7-11.4	17.7-18.4	20.7-21.5	15.6-16.0								•						
0	SAMPLE No.		2	4	7-0	0-5	P-6	4-														
BORING /	=	00.	SV-B-1	SV-B-5	SV-8-7	SV-8-10	SV-B-12	SV-B-14														

SUMMARY OF CHEMICAL TEST RESULTS SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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and CBR tests performed on soil samples from the site and a summary of all the laboratory tests performed on soil samples obtained from boring SV-B-12 are also included in Appendix D.

5.0 <u>DISCUSSION</u>

Analysis of the geotechnical data shows similar and dissimilar features between all three sites. In general, Dry Lake and Ralston valleys are similar and may be used to characterize an area between and around the sites in central Nevada. The Sacramento Valley site is significantly different from Dry Lake and Ralston valleys and can be used to characterize scattered areas of the Great Basin CSP in Arizona and Nevada. Similarities between Dry Lake and Ralston valleys are:

- o Younger and intermediate alluvial fan deposits are the predominant surficial geologic units (younger fans being dominant).
- o Playa deposits, though not extensive on the surface, are a significant unit due to their thickness and central valley location.
- o The basins have closed drainage.
- o These valleys are generally down-dropped (relative to mountains) structural blocks bounded by potentially active faults.
- o The engineering characteristics of the geologic units at the two sites are similar, however, there are differences between the areal extent of these units at each site.

Some dissimilar features between Dry Lake and Ralston are:

o Large areas of undifferentiated non-rock and playa deposits exist in the Ralston site (result of very low relief near valley center).

- o Although no eolian sand deposits are present in Dry Lake Valley, they are present in Ralston Valley and may be encountered locally in areas between and adjacent to the sites.
- o The fine grained soils in Dry Lake Valley are slightly more plastic but less extensive than those of Ralston Valley.

Sacramento Valley exhibits properties different from those in Dry Lake and Ralston valleys. The major differences are:

- o Sacramento Valley displays open drainage (the first four differences that follow can be attributed to this basic characteristic).
- o Sacramento has no playa deposits.
- o The ratio of areas of intermediate to younger alluvial fan deposits in Sacramento is greater by an order of magnitude (7.8 for Sacramento compared to 0.7 and 0.9 for Dry Lake and Ralston, respectively).
- o Depth of drainage incision is generally greater in Sacramento.
- o Surface slope is generally greater in Sacramento.
- o Alluvial deposits of Sacramento (due to granitic source) contain more sand.

Some features similar to Sacramento, Dry Lake, and Ralston valleys are:

- o Alluvial fan deposits are the predominant unit.
- o Basins are elongate, generally north-trending structural depressions with bounding normal faults (i.e. grabens).

Geotechnical conditions at the Dry Lake and Ralston sites are representative of approximately 25 percent of the CSP while conditions at the Sacramento site are representative of about eight percent of the area. Approximately two thirds of the CSP is not characterized by these three sites and a variety of conditions exist throughout this remaining portion of the CSP. For example, south and east of Dry Lake the area is typified by open drainages down-cutting into Tertiary lacustrine deposits. Northeast of Dry Lake, the area was inundated by Pleistocene Lake Bonneville and is typified by Pleistocene lacustrine deposits and associated gravel shorelines.

6.0 CONSTRUCTION CONSIDERATIONS

In this section, geotechnical factors and conditions applicable to construction of the MX system are discussed. The three basing mode concepts considered are vertical shelter, in-line hybrid trench, and horizontal shelter.

The important geotechnical factors for a vertical shelter are roads (primary and interconnecting), drainage crossings, and excavation of shelters. For the in-line hybrid trench, important geotechnical factors are excavation and backfill, roads (primary and temporary), drainage crossings, and aggregates for roads and concrete. For the horizontal shelter, roads and drainage crossings are the important geotechnical factors. A brief summary of the applicable geotechnical factors is presented in the following paragraphs.

- o Terrain Surficial slopes are typically less than four percent, requiring little preconstruction grading for roads and trenches. Depths of drainage incision are generally five to ten feet (1.5 to 3 m) minimizing the need for major drainage structures for roads and trenches.
- o Roads Few roads exist at the sites and therefore, a network of roads will have to be constructed. Approximately
 90 percent of the surficial deposits are coarse-grained
 soils consisting of gravelly sands, silty sands, and
 sandy gravels. These soils have good to excellent subgrade characteristics when compacted, resulting in costeffective road sections.

Excavation - Most of the subsurface soils are dense, weakly to moderately cemented, and possess moderately high shear strength. Except in areas close to mountain fronts, compressional wave velocities range from 1000 to 5000 fps (305 to 1524 mps) up to depths of 150 feet (46 m) below the ground surface, indicating good excavatability. The soils are suitable for excavation of: vertical shelters by augers, continuous trenches (cast-in-place trench construction) by an MX trencher, and horizontal shelters using conventional equipment. In approximately 20 percent of the area, the excavation walls of a vertical shelter may be unstable, requiring slurry or other techniques to support them. Approximately five percent of the area has zones of concentrated cobbles and boulders where an MX trencher will not be able to excavate a trench suitable for cast-in-place construction.

Depth to rock is greater than 150 feet (46 m) over approximately 80 to 85 percent of the sites, therefore, additional expense for excavation of vertical shelters is minimal.

Depth to ground water is greater than 300 feet (92 m) in Dry Lake and Sacramento valleys and greater than 200 feet (61 m) in 90 percent of Ralston Valley, thus, ground-water problems during excavation are expected to be minimal.

o Backfill - Subsurface soils are generally suitable for backfill and compaction in trench excavations; minimum compactive
effort will be required. Backfill will have to be imported
from within the sites for areas of concentrated cobbles and
boulders.

o Aggregates and Water - Sufficient quantities of aggregates and water required for roads and concrete are available within and/or adjacent to the sites, thus minimizing haul costs.

7.0 <u>CONCLUSIONS</u>

In summary, Dry Lake, Ralston, and Sacramento sites present favorable geotechnical conditions for deployment of any of the three present MX basing mode concepts. Geotechnical conditions from these three sites can be extrapolated to approximately 33 percent of the Great Basin CSP.

APPENDIX A

GENERAL GEOTECHNICAL INFORMATION

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GLOSSARY OF TERMS

- ACTIVITY NUMBER A designation composed of the valley abbreviation followed by the activity type and a unique number; may also be used to designate a particular location in a valley.
- AEROMAGNETIC DATA Magnetometer observations made from an airplane.
- ALLUVIAL BASIN A lowland area, generally between uplifted mountain blocks, filled with alluvial deposits.
- ALLUVIAL FAN A low, outspread, relatively flat to gently sloping mass of alluvium, shaped like an open fan or a segment of a cone, deposited by a stream (especially in a semiarid region) at the place where it issues from a narrow mountain valley upon a plain or broad valley. It is steepest near the mouth of the valley where its apex points upstream, and it slopes gently and convexly outward with gradually decreasing gradient.
- ALLUVIAL FAN DEPOSITS Alluvium deposited by a stream or other body of running water as a sorted or semisorted sediment in the form of a cone or fan at the base of a mountain slope.
- ALLUVIAL PLAIN A level or gently sloping tract or a slightly undulating land surface produced by extensive deposition of alluvium, usually adjacent to a river that periodically overflows its banks; it may be situated on a flood plain, a delta, or an alluvial fan.
- ALLUVIUM A general term for unconsolidated clay, silt, sand, gravel, and boulders deposited during relatively recent geologic time by a stream or other body of running water as a sorted or semisorted sediment in the bed of a stream or on its flood plain or delta, or as a cone or fan at the base of a mountain slope.
- ANOMALY 1) A deviation from uniformity in physical properties; especially a deviation from uniformity in physical properties of exploration interest. 2) A portion of a geophysical survey which is different in appearance from the survey in general.
- AQUIFER A permeable saturated zone below the earth's surface capable of conducting and yielding water as to a well.

- ARKOSIC SANDSTONE A sandstone with considerable feldspar, such as one containing minerals from coarse-grained quartzo-feldspathic rocks (granites, granodiorites, medium or high-grade schists) or from older, highly feldspathic sedimentary rocks; specifically a sandstone containing more than 25% feldspar and less than 20% matrix material of clay, sericite, and chlorite.
- ARRIVAL An event; the appearance of seismic energy on a seismic record; a line-up of coherent energy signifying the arrival of a new wave train.
- ATTERBERG LIMITS A general term applied to the various tests used to determine the various states of consistency of fine grained soils. The four states of consistency are solid, semisolid, plastic, and liquid.

Liquid limit (LL) - The water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D423-66).

Plastic limit (PL) - The water content corresponding to an arbitrary limit between the plastic and the semisolid states of consistency of a soil (ASTM D424-59).

Plasticity index (PI) - Numerical difference between the liquid limit and the plastic limit.

- BASIN-FILL MATERIAL/BASIN-FILL DEPOSITS Heterogenous detrital material deposited in a sedimentary basin.
- BEDROCK Rock with a seismic p-wave velocity of 7000 ft (2333 m) per second or more.
- BOUGUER ANOMALY The residual value obtained after latitude, elevation and terrain corrections have been applied to gravity data.
- BOULDER FIELD Five or more rocks, each with diameters of 6 ft or more occurring within an acre.
- BULK SAMPLE A disturbed soil sample (bag sample) obtained from cuttings brought to the ground surface by a drill rig auger or obtained from the walls of a trench excavation.
- c Cohesion (Shear strength of a soil not related to interparticle friction).
- CALICHE Gravel, sand or other material cemented principally by calcium carbonate.

- CALIFORNIA BEARING RATIO (CBR) A test performed on a specifically prepared soil sample which is useful in the design of road pavement to be supported by the soil tested (ASTM D1833-73). The load is applied on the penetration piston which is penetrated into the soil sample at a constant penetration rate. The bearing ratio reported for the soil is normally the one at 0.1 inches (2.5 mm) penetration.
- CANDIDATE One of some group of regions, areas or sites being considered for MX deployment. Removal of candidate from a specifically named region, area or site term indicates selection by SAMSO/MNND.
- CANDIDATE DEPLOYMENT AREA (CDA) An area encompassing between 500 and 1000 square nautical miles of potentially suitable land with either naturally or artificially defined boundaries designated for convenience of study, discussion and data depiction. The candidate deployment area could be composed of two to four parcels and should have a specific place name description.
- CANDIDATE DEPLOYMENT PARCEL (CDP) An area of 150 to 500 square nautical miles potentially suitable for MX siting which, when aggregated with others, forms a Candidate Deployment Area. Each parcel should have a specific geographic description. (In the Basin and Range Physiographic province a parcel may correspond to a geographic valley and in Texas to some agri-economic unit.)
- CANDIDATE DEPLOYMENT SITE (CDS) A non-specific (i.e. not finally approved) site proposed for some element of the MX system within a chosen deployment area (i.e. trench or shelter site).
- CANDIDATE SITING PROVINCE (CSP) An area potentially suitable for deployment of the MX system generally encompassing more than 6000 square nautical miles which, in a broad sense, is homogeneous with respect to most of the important characteristics governing siting of a total MX system.
- CANDIDATE SITING REGION (CSR) Potentially suitable area between 4000 and 6000 square nautical miles within one, or encompassing portions of more than one, candidate siting province which allows for full MX deployment.

- CAPABLE (fault) Movement at or near the surface at least once in the past 35,000 years, and/or more than once in the past 500,000 years, (Nuclear Regulatory Commission).
- CAPROCK A resistant, moderately to strongly cemented caliche layer forming a "cap" over less resistant layers.
- CD TRIAXIAL SHEAR-A type of test to measure the shear strength of an undisturbed soil sample
- CLOSED BASIN A catchment area draining to some depression or lake within its area, from which water escapes only by evaporation.
- COARSE-GRAINED A term which applies to a soil of which more than one-half of the soil particles, by weight, are larger than 0.075 mm in diameter (passing the No. 200 U.S. size).
- COARSER-GRAINED A term applied to alluvial fan deposits which are predominantly composed of material larger than 3 inches (76 mm) in diameter.
- COLLUVIAL DEPOSITS A general term applied to any loose, heterogenous, and incoherent mass of soil material or rock fragments deposited chiefly by dislodgement and downslope transport of the material under the direct application of gravitational body stresses. Material is usually found at the base of a steep slope or cliff.
- COMPACTION TEST A type of test to determine the relationship between the moisture content and density of a soil sample which is prepared in compacted layers at various water contents (ASTM D1557-70).
- COMPRESSIBILITY-Property of a soil pertaining to its susceptibility to decrease in volume when subjected to load.
- COMPRESSIONAL WAVE -An elastic body wave in which particle motion is in the direction of propagation; the type of seismic wave assumed in conventional seismic exploration. Also called P-wave, dilatational wave, and longitudinal wave.
- CONSOLIDATION TEST A type of test to determine the compressibility of a soil sample. The sample is enclosed in the consolidometer which is then placed in the loading device. The load is applied in increments at certain time intervals and the change in thickness is recorded.

- CONTERMINOUS UNITED STATES The contiguous 48 states.
- CORE SAMPLE A cylindrical sample obtained with a rotating core barrel with a cutting bit at its lower end. Core samples are obtained from indurated deposits and in rock.
- DEBRIS FLOW A high-density flow of mud containing abundant coarse-grained materials (boulders, cobbles, gravel, sand) that frequently result from an unusually heavy rain.
- DEGREE OF SATURATION Ratio of volume of water in soil to total volume of voids.
- DETECTOR See GEOPHONE.
- DIRECT SHEAR TEST A type of test to measure the shear strength of a soil sample where the sample is forced to fail on a predetermined plane.
- DISSECTION/DISSECTED (alluvial fans) The cutting of stream channels into the surface of an alluvial fan by the movement (or flow) of water.
- DISTAL That portion of an alluvial deposit farthest from its point of origin.
- DRY UNIT WEIGHT/DRY DENSITY Weight per unit volume of the solid particles in a soil mass.
- ELECTRICAL CONDUCTIVITY Ability of a material to conduct electrical current
- ELECTRICAL RESISTIVITY Property of a material which resists flow of electrical current
- ENTRENCH The process whereby a stream erodes downward to form a trench.
- ${\tt EOLIAN}$ A term applied to materials which are deposited by wind.
- EPHEMERAL(stream) A stream in which water flow is discontinuous and of short duration.
- EXTERNAL DRAINAGE Stream drainage system whose downgradient flow is unrestricted by any topographic impediments.
- EXTRUSIVE (rock) Igneous rock that has been ejected onto the earth's surface (e.g., lava, basalt, rhyolite, andesite; detrital material, volcanic tuff, pumice).

- FAULT A plane or zone of rock fracture along which there has been displacement.
- FAULT BLOCK MOUNTAINS Mountains that are formed by normal faulting in which the surface crust is divided into structural, partially to antirely fault-bounded blocks of different elevations.
- FINE-GRAINED A term which applies to a soil of which more than one-half of the soil particles, by weight, are smaller than 0.075 mm in diameter (passing the No. 200 U.S. size sieve).
- FINER-GRAINED A term applied to alluvial fan deposits, which are composed predominantly of material less than 3 inches (76 mm).
- FLOODING/LOW ENERGY FLOW Flood waters flowing on a slope of low gradient.
- FLUVIAL DEPOSITS Material produced by river action; generally loose, moderately well-graded sands and gravel.
- FORMATION A mappable assemblage of rocks characterized by some degree of homogeneity or distinctiveness
- FREE AIR ANOMALY Gravity data which have been corrected for latitude and elevation (free air correction) but not for the density of rock between the datum and the plane of measurement (Bouguer correction).
- FUGRO DRIVE SAMPLE A 2.50 inch (6.4 cm) diameter soil sample obtained from a drill hole with a Fugro Drive Sampler. The Fugro drive sampler is a ring-lined barrel sampler containing 12 one-inch (2.54 cm) long brass sample rings. The sampler is advanced into the soil using a drop-hammer.
- GAMMA A unit of magnetic-field intensity. A gamma is 10^{-5} oersteds; sometimes expressed (incorrectly) as 10^{-5} gauss with which it is numerically equal.
- GECMORPHOLOGY The study, classification, description, nature, origin, and development of present landforms and their relationships to underlying structures, and of the history of geologic changes as recorded by these surface features.
- GEOPHONE The instrument used to transform seismic energy into electrical voltage; a seismometer, jug, or pick-up.

- GRAIN-SIZE ANALYSIS (GRADATION) A type of test to determine the distribution of soil particle sizes in a given soil sample. The distribution of particle sizes larger than 0.075mm (retained on the No. 200 sieve) is determined by sieving, while the distribution of the particle sizes smaller than 0.075 mm is determined by a sedimentation process, using a hydrometer.
- GRAVEL Particles of rock that pass a 3-in. (76.2 mm) sieve and retained on a No. 4(4.75 mm0 sieve
- GRAVITY The force of attraction between bodies because of their mass. Usually measured as the acceleration of gravity.
- GRAVITY GRADIENT The partial derivative of the acceleration of gravity with respect to distance in a particular direction, for which purpose the acceleration of gravity is considered as a scalar.
- INTERIOR DRAINAGE Stream drainage system that flows into a closed topographic low (basin).
- INTRUSIVE (rock) A rock formed by the process of emplacement of magma (liquid rock) in pre-existing rock.
 (e.g. granite, granodiorite, quartz monzonite).
- LACUSTRINE DEPOSITS Materials deposited in lake environment.
- LINE A linear array of observation points, such as a seismic line.
- LIQUID LIMIT See ATTERBERG LIMITS.
- LOESS A wind blown deposit predominantly silt or silty clay or clayey silt.
- LOW ENERGY FLOW See FLOODING.
- MAGNETIC INTENSITY A vector quantity measuring magnetic field strength. The unit of magnetic intensity commonly used in geophysical exploration is the gamma (see GAMMA).
- MANTLED PLAYA A playa surface or a portion of the surface that is covered with younger geologic material such as windblown sand, or alluvium.
- MILLIGAL A unit of acceleration used with gravity measurements; l milligal = 10^{-5} m/sec.². Abbreviated mgal.

- MOISTURE CONTENT The ratio, expressed as a percentage, of the weight of water contained in a soil sample to the oven-dry weight of the sample.
- N VALUE Penetration resistance, number of blows required to drive the standard split spoon sampler for the second and third six inches (0.15 m) with a 140 pound (63.5 kg) hammer falling 30 inches (0.76 m) (ASTM D1586-67).
- OPTIMUM MOISTURE CONTENT Moisture content at which a soil can be compacted to a maximum dry unit weight by a given compactive effort
- OVERBANK FLOODING A large flow of water that overflows the sides of A stream channel.
- O Angle of internal friction
- PATINA A dark coating or thin outer layer produced on the surface of a rock or other material by weathering after long exposure (e.g., desert varnish).
- PAVEMENT/DESERT PAVEMENT When loose material containing pebble-sized or larger rocks is exposed to rainfall and wind action the finer dust and sand are blown or washed away and the pebbles gradually accumulate on the surface, forming a mosaic which protects the underlying finer material from wind attack. Pavement can also develop in finer-grained materials. In this case the armored surface is formed by dissolution and cementation of the grains involved.
- PEGAMATITE DIKE A coarse grained igneous rock of granitic composition that forms as a tabular intrusion that cuts across the planar structures of the surrounding rock.
- P-WAVE See COMPRESSIONAL WAVE.
- PERIMETER SEISMIC REFRACTION SURVEY Shallow seismic refraction measurements made around the perimeter of a valley.
- PERMEABLE The ability of liquid to pass through soil and/or rock material.
- PICK-UP See GEOPHONE.

PITCHER TUBE SAMPLE - An undisturbed, 2.87 inch (73 mm) diameter soil sample obtained from a drill hole with a Pitcher tube sampler. The primary components of this sampler are an outer rotating core barrel with a bit and an inner stationary, spring-loaded, thin-wall sampling tube which leads or trails the outer barrel drilling bit, depending upon the hardness of the material being penetrated.

PLASTIC LIMIT - See ATTERBERG LIMITS.

PLASTICITY INDEX - See ATTERBERG LIMY (4).

- PLAYA/PLAYA DEPOSITS A term used in the southwest U.S. for a dried-up, flat-floored area consisted of thin, evenly stratified sheets of fine class wilt, or sand, and representing the lowest part of a shallow, completely closed or undrained, desert lake basin in which water accumulates and is quickly evaporated, usually leaving deposits of soluble salts.
- PONDING (of water) The accumulating of water in a topographic depression.
- PRIME Modifier used to indicate the highest ranking province, region, area, or site. If not an interdisciplinary ranking, then a qualifier should be used such as "prime" geotechnical candidate siting area".
- PROXIMAL That portion of an alluvial deposit nearest to its point of origin.
- REGIONAL The general attitude or configuration disregarding features smaller than a given size. The regional gravity is the gravity field produced by large-scale variations ignoring anomalies of smaller size. See residualize.
- RELATIVE AGE The relationship in age (oldest to youngest) between geologic units without specific regard to number of years.
- RESIDUAL What is left after a regional field has been removed, as in gravity or magnetic analysis. See RESIDUALIZE.

- RESIDUALIZE The process of separating a graphically depicted curve or a surface into its low-frequency parts (called the regional) and its high-frequency parts (called the residual).

 Residualizing is an attempt to sort out of the total field those anomalies which result from local structure; that is, to fine local anomalies by subtracting gross (regional) effects.
- ROCK UNITS Distinct rock masses with different characteristics (e.g., igneous, metamorphic, sedimentary).
- S-WAVE See SHEAR WAVE.
- SAND Soil passing through No. 4(4.75 mm) sieve and retained on No. 200 (0.075 mm) sieve
- SAND DUNE A low ridge or hill consisting of loose sand deposited by the wind, found in various desert and coastal regions and generally where there is abundant surface sand.
- SEISMIC Having to do with elastic waves. Energy may be transmitted through the body of an elastic solid as P-waves (compressional waves) or S-waves(shear waves).
- SEISMIC REFRACTION DATA: deep/shallow Data derived from a type of seismic shooting based on the measurement of seismic energy as a function of time after the shot and of distance from the shot, by determining the arrival times of seismic waves which have travelled nearly parallel to the bedding in high-velocity layers, in order to map the depth to such layers.
- SEISMOGRAM A seismic record.
- SEISMOMETER See GEOPHONE.
- SHEAR WAVE A body wave in which the particle motion is perpendicular to the direction of propagation. Also called S-Wave or transverse wave.
- SHEET FLOW A process in which storm-borne water spreads as a thin, continuous veneer (sheet) over a large area.
- SHEET SAND A blanket deposit of sand which accumulates in shallow depressions or against rock outcrops, but does not have characteristic dune form.
- SHOT Any source of seismic energy; e.g., the detonation of an explosive.

- SHOT POINT The location of any source of seismic energy; e.g., the location where an explosive charge is detonated in one hole or in a pattern of holes to generate seismic energy. Abbreviated SP.
- SILT AND CLAY Fine-grained soil passing through No. 200 (0.075 mm) sieve.
- SITE Location of some specific activity or reference point.

 The term should always be modified to a precise meaning or be clearly understood from the context of the discussion.
- SPECIFIC GRAVITY The ratio of the weight in air of a given volume of soil solids at a stated temperature to the weight in air of an equal volume of distilled water at a stated temperature.
- SPLIT SPOON SAMPLE A disturbed sample obtained with a split spoon sampler with an outside diameter of 2.0 inches (5.1 cm). The sample consists of a split barrel which is driven into the soil using a drop-hammer.
- SPREAD The layout of geophone groups from which data from a single shot are recorded simultaneously. Spreads containing twenty-four geophones have been used in Fugro's seismic refraction surveys.
- STREAM CHANNEL DEPOSITS Materials (clay, silt, sand, gravel, cobbles, boulders) which have been deposited in a stream channel.
- STREAM TERRACE DEPOSITS Stream channel deposits no longer part of an active stream system, generally loose, moderately well graded sand and gravel.
- SURFICIAL DEPOSIT Unconsolidated residual and alluvial deposits occurring on or near the earth's surface.
- TRANSITORY A poorly defined, shallow ephemeral stream across an alluvial fan surface, the position of which is temporary and tends to shift frequently.
- UNCONFINED COMPRESSION A type of test to measure the compressive strength of an undisturbed soil sample.
- UNIFIED SOIL CLASSIFICATION SYSTEM (USCS) A system which determines soil classification on the basis of grain-size distribution and Atterberg Limits. (See page A-17).

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- VALLEY SEISMIC REFRACTION SURVEY Deep seismic refraction measurements made near the middle of a valley to determine seismic wave propagation velocities and thickness of basin fill.
- VELOCITY Refers to the propagation rate of a seismic wave without implying any direction. Velocity is a property of the medium and not a vector quantity when used in this sense.
- VELOCITY LAYER A layer of rock or soil with a homogenous seismic velocity.
- VELOCITY PROFILE A cross-section showing the distribution of material seismic velocities as a function of depth and its configuration.
- WASH SAMPLE A sample obtained by screening the returned drilling fluid during rotary wash drilling to obtain lithologic information between samples.

Definitions were derived in part from Webster's New Collegiate Dictionary (1972 edition), Glossary of Geology (American Geological Institute, 1972), Encyclopedic Dictionary of Exploration Geophysics (Sheriff, 1973), and 1976 Annual Book Book of ASTM Standards.

DIAGNOSTIC CARBONATE MORPHOLOGY

STAGE	GRAVELL	A 20172		NON	GRAVELLY SOILS						
1	Thin, disconti	nuous pebble	coatings	Few filame	nts or faint coatings						
п	Continuous peb interpebble fi		some	Few to abundant nodules, flak filaments							
ш	Many interpebt	ole fillings		Many nodules and internodular fillings							
II.	Laminar horizo horizon	on overlying p	lugged	Laminar ho horizon	rizon overlying plugged						
	STAGE	I Weak Ca	II Strong Ca		IY Indurated K						
	GRAVELLY SOILS				K21m K22m K3						
	NONGRAVELLY SOILS	A A A A A A A A A A A A A A A A A A A		12000	K2Im K22m K3						

Stages of development of a caliche profile with time. Stage I represents incipient carbonate accumulation, followed by continuous build-up of carbonate until, in Stage IV, the soil is completely plugged.

SUMMARY OF CALICHE DEVELOPMENT

Reference: Gite, L.H. Peterson, F.F., and Grossman, R.B., 1965.
The K. horizon, A. master horizon of carbonate

accumulation: Soil Science, v. 99, p. 74-82

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(1) Arei Mbols	MX () GEOLOGIC UNITS	NON-ROCK UNITS	(1) A Arei Geol Symbols un
Au. Ast	Au	Non-rock Deposits (undifferentiated); fine- to coarse-grained materials deposited by alluvial, fluvial, eolian, lacustrine, gravity or glacial processes.	
Aal	AI	Fluvial Deposits; predominantly composed of poorly- to well-graded sand and gravel with lesser amounts of silt- and boulder-sized material. The unit pre-dominantly consists of recent water-laid deposits occupying present drainages and flood plains.	gr
		- Older Fluvial Deposits (Alo) are generally thicker, more extensive units deposited in ancestral fluvial systems.	٧u
		 Alluvial Outwash Deposits (Alw) consist of mixed, geomorphically nondescript alluvial and fluvial deposits covering large, relatively flat, river and playa basins. 	۷b
A t	A 2	Terrace Deposits; predominantly composed of moderately to well graded, clay- to gravel-sized material. Principally elevated terraces bordering modern streams (A2s) and lakes playas (A21).	Su
	A 3	Eolian Deposits; predominantly composed of poorly graded sand-sized material deposited by wind action. Deposits may consist of mixed sand, silt, and clay (A3u), or be differentiated on the basis of predominant grain size and landform.	Qtz
		A3s d - Predominantly fine sand-sized material deposited in sheets (A3s) or dunes (A3d).	Psa, Pm, Ph, Cau, Ls, Py,
		 A31 - Loess composed predominantly of silt-sized material with lesser amounts of clay and fine sand. 	Par
		A3f - Predominantly clay-sized material with lesser amounts of silt and fine sand.	
	A 4	Lacustrine, Estuarine, and Playa Deposits; predominantly composed of poorly graded clay, silt, and fine sand deposited in bodies of standing water. Older lacustrine, estuarine, and playa deposits (A4o) are thicker, more extensive units occupying ancestral lake basins	ûtz. gn
Aaf	A 5	Alluvial Fan Delosits; predominantly composed of well graded sand and gravel with varying amounts of silt—, cobble—, and boulder—sized malerial. Deposited principally by distributary channels adjacent to mountain fronts. Relative ages are indicated by o — older, i — intermediate, or y — younger	
	A 6	Pediment. Pediment Deposits, and Areas of Shallow Rock; planated bedrock shelf or near surface rock generally overlain by a thin mantle of sand- to boulder- sized residual or alluvial material.	
	A7	Colluvial Deposits; predominantly composed of moderately- to well-graded sand and gravel with varying amounts of silt-, cobble-, and boulder-sized material. Deposited locally by gravity and water adjacent to steep gradients.	

NOTES. (1) ARE1 symbols were developed for use in the Aggregate Resources Evaluation Investigation (See Section 5.1 and Drawings 5.1A through 5.1C)

(2) MX Geologic units were used for Methodology, Screening, and Characterization studies.

(1) MX (2)
AREL GEOLOGIC
SYMBOLS UNITS

ROCK UNITS

Shown in regions where rock is exposed; the areally predominant (greater.than 70 percent) rock type is indicated. In those areas where two rock types occur the predominant rock type is shown followed by the subordinate rock type (e.g. S2MP 14T).

I IGNEOUS (UNDIFFERENTIATED). Rocks formed by solidification of a molten or partially molten mass.

18

V11

Vb.

- Il Intrusive Typically crystalline, formed by the solidification of molten material below the surface (e.g., granite, syenite, diorite).
- 12 Extrusive (undifferentiated). Formed by solidification of molten material at or near the surface.
- Extrusive (flows). Extrusive rocks formed by solidification of lava (e.g. basalt, dacite) T3b denotes young basaltic flows which may be interbedded with basin-fill materials.
- Extrusive (volcaniclastic). Formed by accumulation, welding and or cementation of deposits of volcanic ejecta (e.g. tuff, agglomerate, lapilli).

SU SEDIMENTARY (UNDIFFERENTIATED). Coarse— to fine—grained materials that exhibit some degree of cementation and were deposited by water, wind, gravity, or evaporation.

Psa. Pm. Ph. Cau. Ls. Py. Par

- Sandstone. Composed predominantly of sand-sized particles.
- \$2 Limestone and Dolomite. Composed predominantly of carbonate material.
- Shale. Composed predominantly of clay- and silt-sized particles (e.g. shale, siltstone, mudstone).
- Evaporites. Sediments deposited from solution as a result of evaporation (e.g. gypsum, anhydrite, halite).
- Clastics. Undifferentiated deposits composed of silt- to boulder-size?

 material May be angular to rounded.
- Otz. M METAMORPHIC (UNDIFFERENTIATED). Rocks formed through alteration of igneous or sedimentary rock material by pressure, heat, or chemical changes below the weathered zone (e.g. gneiss, schist, slate, marble, quartzite).
 - ROCK COMPLEXES. Indicated where no areally predominant (greater than 70 percent) rock type is present.

USEAGE

Modifying letter (r) indicates concentrations of resistant secondary carbonate (caliche), silicious, ferruginous and or gypsiferous material, e.g. A51r.

A3s A5y - Mixed non-rock units; most aleally extensive unit is listed first.

Aby(ACI) - Parenthetic unit underlies thin veneer of overlying mapped unit.

- Established formations may have a supplemental letter added to distinguish formal designation (e.g. Tertiary Ugallala Fm.)

EXPLANATION OF GEOLOGIC UNITS

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Information Required for Describing Soils	9	For undisturbed soils add information	on stratification, degree of compact- ness, cementation, moisture conditions and drainage characteristics.		Give typical name; indicate approximate procentages of sand and gravel, max. size; angularity, surface condition, and hardness of the coarse	grains; local or geologic name and other pertinent descriptive informa- tion; and symbol in parentheses.	Example: Sity and gravelly: about 20% hard	angular gravel particles 15-in. maximum size; rounded and sub- angular sand grains coarse to fine.	about 13% nothersterntes with low dry strength; well compacted and moist in place; alluvial sand; (SM).			Give typical name, indicate degree and character of plasticity, amount and maximum size of coarse grains, color	in wet condition, odor if any, local or geologic name, and other petiment descriptive information; and symbol in parenthese	:	For undisturbed soils and informa- tion on structure, stratification, consistency in undisturbed and re- molded states, moisture and drain	age conditions.	Example: Clayey silt, brown, slightly plastic.	small percentage of fine sand, numerous vertical root holes, firm and dry in place, loess, (ML).
cedures han 3 inches ated weights)		nd substantial particle sizes.	range of sizes missing.	ow plasticity.	procedures see	nd substantial particle sizes.	range of sizes missing.	w plasticity. see ML below)	procedures see	ures 40 Sieve Size	Toughness (Consistency near PL)	None	Medium	Slight	Slight to medium	High	Slight to medium	r, spongy feel ture.
Field Identification Procedures (Excluding particles larger than 3 inches and basing fractions on estimated weights)	\$	fide range in grain sizes and substantial amounts of all intermediate particle sizes.	redominantly one size or a range of with some intermediate sizes missing.	Nonplastic fines or fines with low (for identification procedures see	Plastic fines (for identification procedures see CL below).	ide range in grain sizes and substantial amounts of all intermediate particle sizes.	edominantly one size or a range of with some intermediate sizes missing.	Nouplastic fines or fines with low plasticity. (for identification procedures see M.), below)	Plastic fines (for identification procedures see CL below).	Identification Procedures on Fraction Smaller than No. 40 Sieve Size	Dilatancy (Reaction to shaking)	Quick to slow	None to very slow	Slow	Slow to none	None	None to very	Readily identified by color, odor, spongy feel and frequently by fibrous texture.
Field I (Excluding		Wide range ir amounts of	Predominantly one size with some intermediat	Nonplastic fines	Plastic fines (f CL helow).	Wide range in	Predominantly with some in	Nouplastic fines	Plastic fines (f CL below).	Iden on Fraction S	Dry Strength (Crushing characteristics)	None to slight	Medium to high	Slight to medium	Slight to medium	High to very	Medium to high	Readily identificand frequently
Typical Names	Þ	Well-graded gravels, gravel-sand mix- tures, little or no fines.	Poorly-graded gravels, gravel-sand mix- tures, little or no fines.	Silty gravels, gravel-sand-silt mixtures.	Clayey gravels, gravel-sand-clay mix- tures.	Well:graded sands, gravelly sands, little or no fines.	Poorly-graded sands, gravelly sands, little or no fines.	Silty sands, vand-silt mixtures.	Clayey sands, sand-clay mixtures,			Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.	Inorganic clays of low to medium plas- ticity, gravelly clays, sandy clays, silty clays, lean clays.	Organic sitts and organic sitty clays of low plasticity.	Inorganic silts, micaceous or diatoma- ceous fine sandy or silty soils, clastic silts.	Inorganic clays of high plasticity, fat clays.	Organic clays of medium to high plas- ticity, organic silts.	Peat and other highly organic soils.
Group	3	СW	GP	СМ	ည	SW	SP	SM	SC			ML	CL	OL	MP	CH	но	ų
Major Divisions	2	es ba	vels alf of c larger (seve size y be use) (clean (Littl on fi	than his on is on is on is on is on is on is one is	sert I i .ni-¾	inan ion, the to the	sbn. of of states size	at than 1 at notice 4 a b. oM consistent consistent and consistent	ant) ji	O bas mit biu	piJ		yalO br simil b ocnanis	iupiJ		Highly Organic Soils
Z	-	io. 200 More than half of maternal is larger than No. 200 aseve size. — sieve size. — ut the smallest particle visible to the naked eye.									1971 - 1971	.3518	SISVE!	a to tla	ų u e ų;	910M	High	

UNIFIED SOIL CLASSIFICATION SYSTEM

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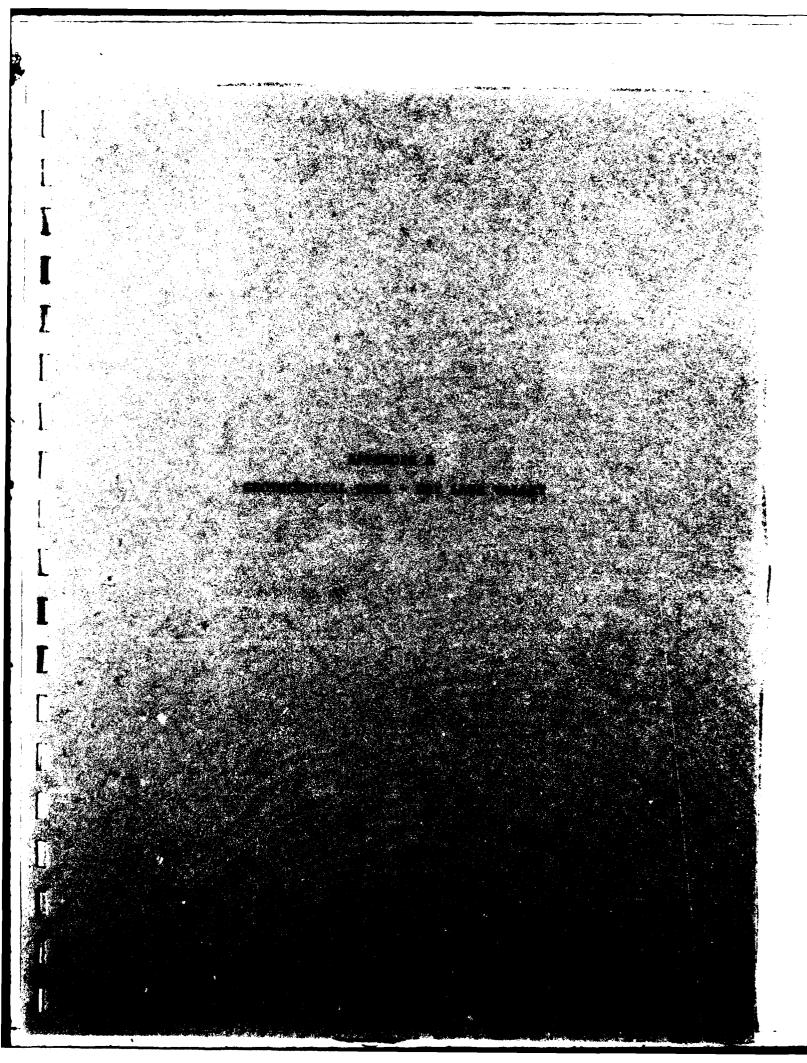


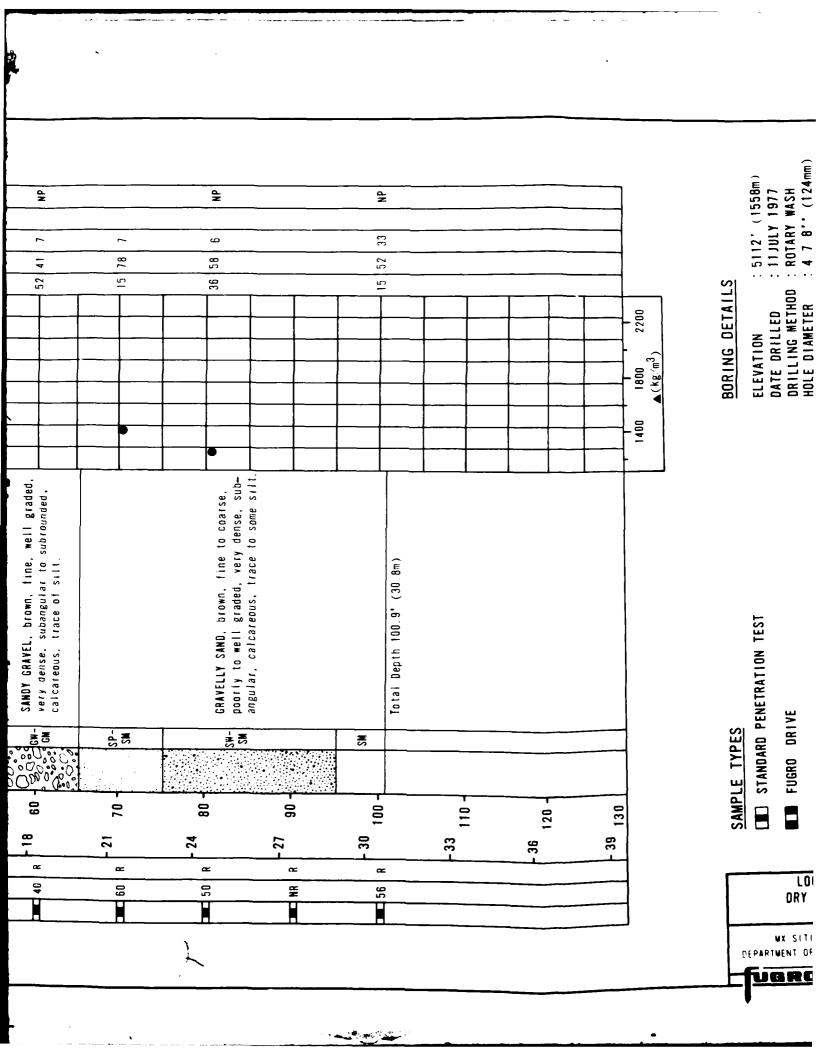
TABLE OF CONTENTS APPENDIX B

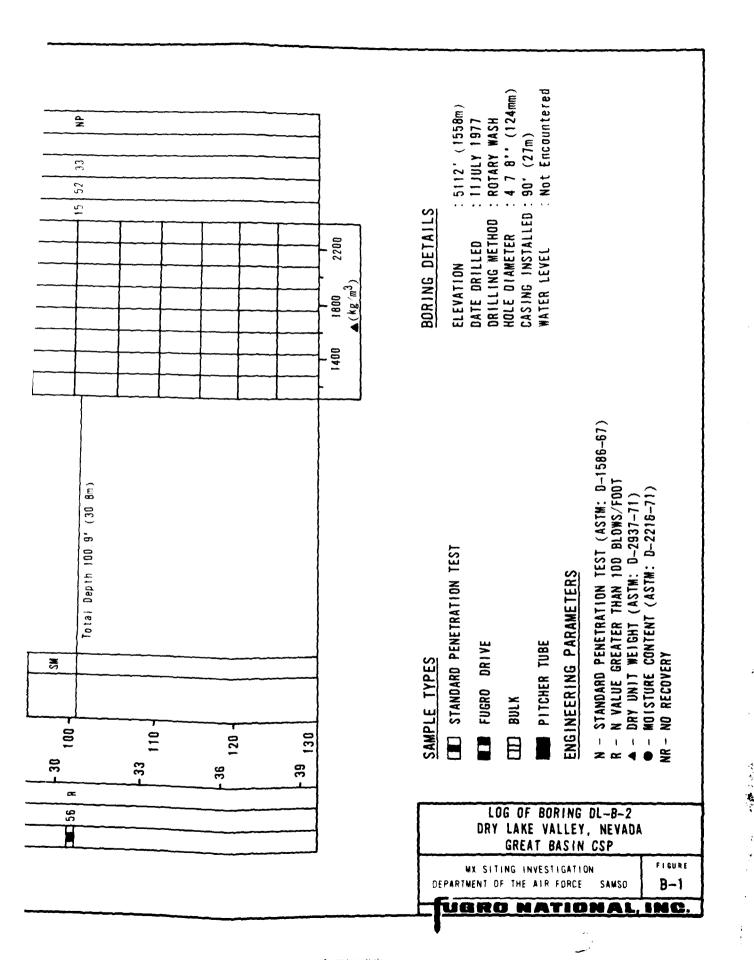
BORING AND TRENCH LOGS	
LOG OF BORING DL-B-2	Figure B-1
LOG OF BORING DL-B-5	Figure B-2
LOG OF BORING DL-B-12	Figure B-3
LOG OF TRENCH DL-T-2	Figure B-4
LOG OF TRENCH DL-T-8	Figure B-5
LOG OF TRENCH DL-T-9	Figure B-6
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UNCONFINED COMPRESSION TEST RESULTS	Table B-2
TRIAXIAL SHEAR TEST RESULTS	Table B-3
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CALIFORNIA BEARING RATIO (CBR) CURVES	Figure B-7
GRAIN SIZE CURVES, CBR TESTS	Figure B-8

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	SOIL DESCRIPTION			`			GRAVELLY SAND, brown, fine to coarse, poorly to well graded, medium dense to very dense, angular, calcareous, trace	to some silt.					SANDY GRAVEL	very dense, subangular to subrounded, calcareous, trace of silt.
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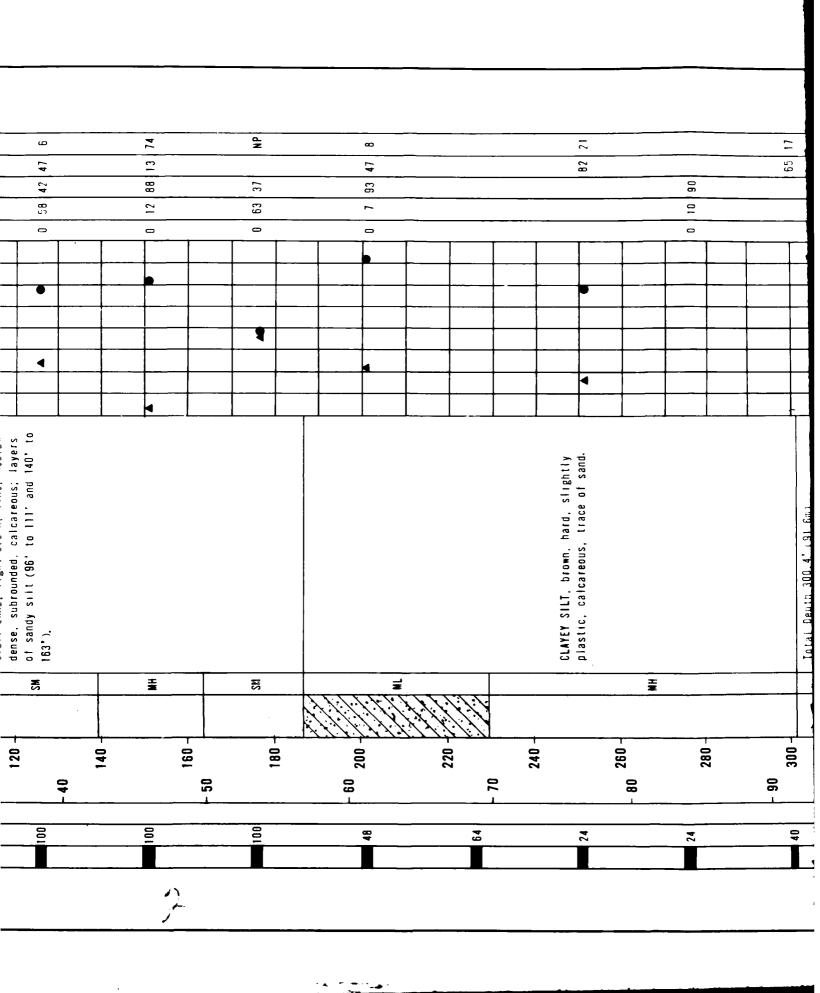
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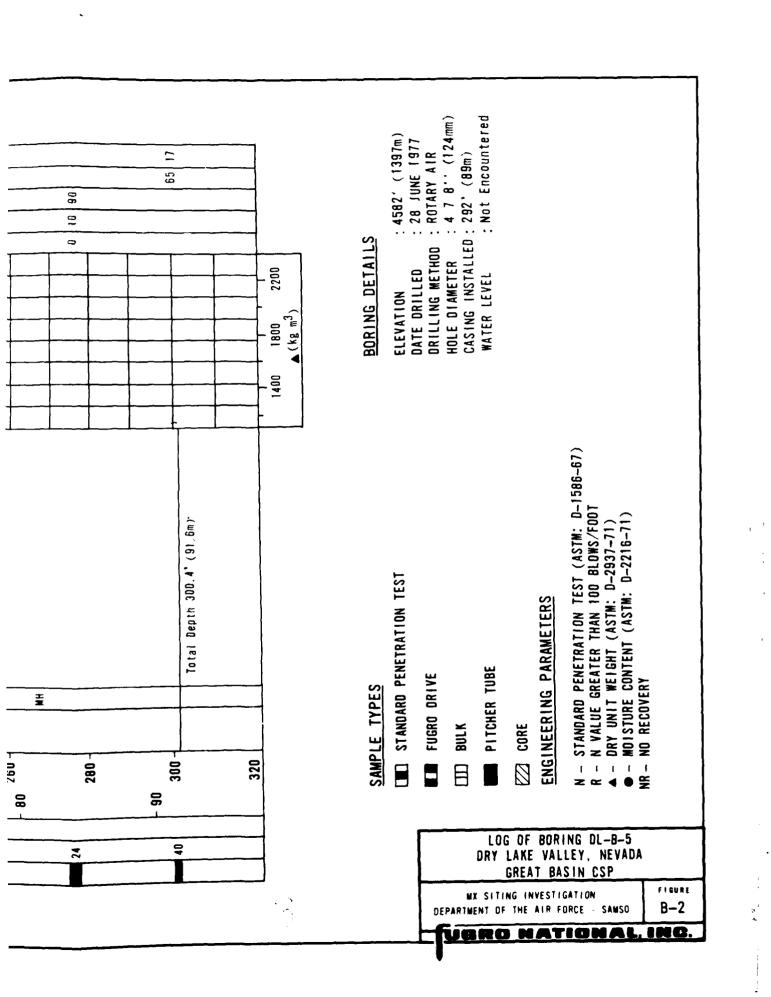
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	SOIL DESCRIPTION	CLAY, light gray, ha d, high plasticity, calcareous, trace of sand.				sand; layer of silty sand (22' to 29').							SILTY SAND, light brown, fine, medium dense subfounded calcareous; layers	y silt (96° to 111° and	
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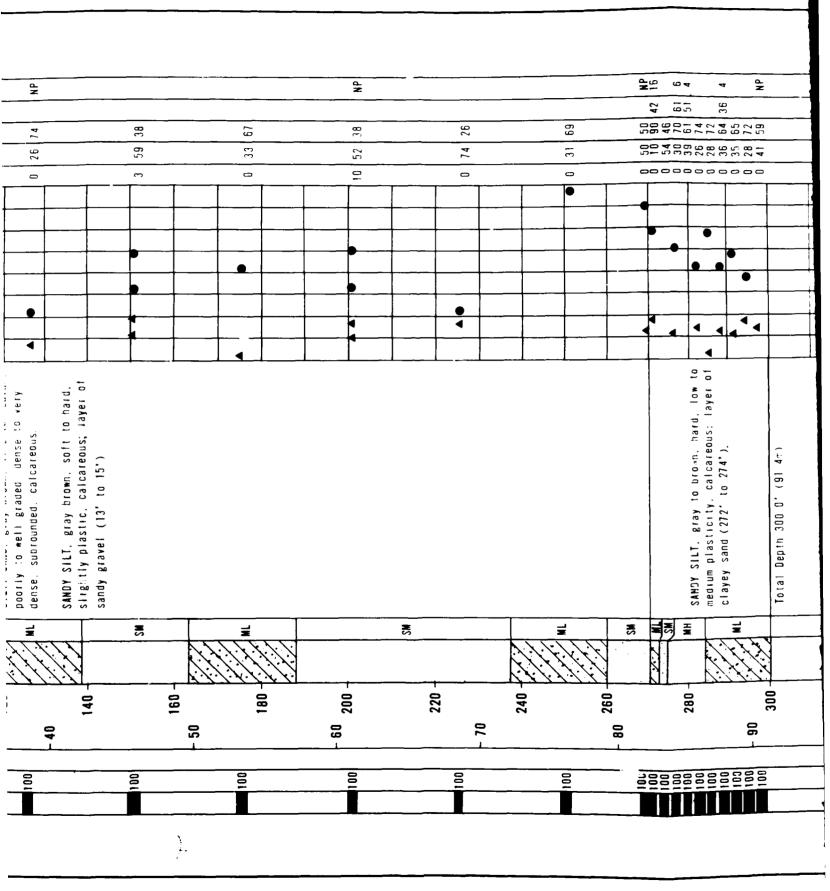


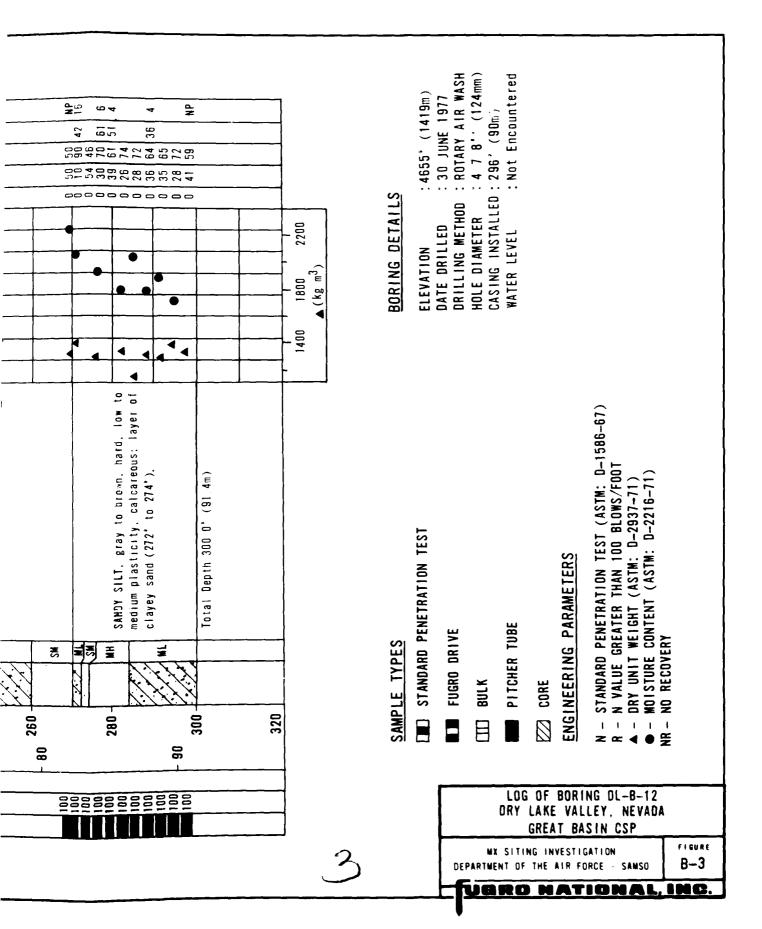
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COVERY		53 4	82			901		100	100	001	100		100			100	
ALUE -	METI	45 0		25					- 20	·			- 30				40
F	 FEE	0		20		6	4		. 09		08		100		120		
ногоел	. –												- -				
505	SN	=	- E	ا ود	5 5		<u>=</u>	S			<u> </u>			¥.		=	
	SOIL DESCRIPTION													A CONTRACTOR OF THE CONTRACTOR	SILITY SAND and SANDY SILI IN EL EUGEG:	to well graded, dense to subrounded, calcareous.	
▲(pcf) 80 90 100 110 120 130 140	5 10 15 20 25 30 35 • (*z)	•		••	•	•		•	•			3				•	
SI	85			54	=		7								——————————————————————————————————————		
SIEVE	SAF		34 6	35 10 87 10	500		40 6	76 2	29 7	33_E	14	28 7	70 2			26 74	
[v	11		99	20	ر .	69	09	24	711	67	29	72	29	···			
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BULK SAMPLE	FEET	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	ĺ	ALY:	SIS		
		5		CON		GR	SA	FI	LL	P
Щ°	0			Loose		a	63	27		
1	2 -		SM	Medium dense		10	74	16		
	4			Very dense	GRAVELLY SAND, brown, fine to coarse, poorly graded, slightly moist, angular to subrounded, calcareous, moderately cemented; trace to some sit; trace of boulders at 4' (lm), boulder size to 3.5' (1.1m); trace of cobbles at 5' (2m).	27	59	14		
- 3	8 -		SP	Dense		33	57	סו		
-4	14-		SP and GP	Deπse	GRAVELLY SAND to SANDY GRAVEL, light brown, fine to coarse sand, fine gravel, poorly graded, slightly moist, subangular to subrounded, cal-careous, weakly to strongly cemented.	49	49	2		
	18 ~		SP-	Medium dense	GRAVELLY SAND, gray, fine to coarse, poorly graded. dry, subangular to subrounded, calcareous, weakly cemented, trace of sit.	27	62	11		:
- 6	20 -				Total Depth 18' (5.5m) Stability of vertical walls: Instable 0 to 2' (0 to 0.7m) Stable 2 to 16' (0.7 to 4.9m) Unstable 16 to 18' (4.9 to 5.5m)					

SURFACE ELEVATION : 5112" (1558m)

DATE EXCAVATED : 24 August 1977

SURFACE GEOLOGIC UNIT : A5y

SURFACE GEOLOGIC UNIT : A5y
TRENCH LENGTH : 57' (17m)
TRENCH ORIENTATION : N60E

LOG OF TRENCH DL-T-2 DRY LAKE VALLEY, NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION CEPARTMENT OF THE AIR FORCE SAMSO

B-4

UGRO NATIONAL, INC.

BULK SAMPLE	METERS FET	9070	nscs	CONSISTENCY	SOIL DESCRIPTION		SIEV ALY	'E S 1 S		
Į.			↓_	CON		GR	SA	FI	11	Ρ
	0 0			Soft					30	,
	-1		ML	Firm	SANDY SILT, light brown, slightly moist, slightly plastic, calcareous.	0	23	77	33	1
	- 2									
	3 10	1-		Loose	GRAVELLY SAND, light brown, fine to coarse,	24	73	3		
	12		SP		poorly graded, dry, subangular to subrounded, calcareous, trace of silt, trace of caliche nodules.					
	14			Medium dense						
}	-5				Total Depth 16" (4.9m)					
	18 -6 20				Stability of vertical walls: Stable 0 to 8° (0 to 2.4m) Unstable 8 to 14° (2.4 to 4.3m) Stable 14 to 16° (4.3 to 4.9)					
	22									

TRENCH DETAILS

SURFACE ELEVATION : 4783' (1458m)
DATE EXCAVATED : 24 August 1977

SURFACE GEOLOGIC UNIT: AT

TRENCH LENGTH : 60° (18m)
TRENCH ORIENTATION : N8CW

LOG OF TRENCH DL-T-8 DRY LAKE VALLEY, NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

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ugro national, inc.

BULK SAMPLE METERS ST	0010	nscs	CONSISTENCY	SOIL DESCRIPTION	1	SIEV	/E \$1\$	
ME	1 1 1		NOO	SOIL BESONTFIELD	CR	SA	F1	LLP
0			Loose					
1	4	sc	Medium dense	CLAYEY SAND, brown, fine to coarse, poorly graded, slightly moist, subangular to subrounded, cal- careous, moderately cemented.		71	27	26
-2	8							
1:	2	SP-	Loose		35	58	7	
	4 - 6 -	SM	Medium dense	GRAVELLY SAND, light brown, fine to coarse, poorly graded, slightly moist, round to angular, calcareous, trace to a little silt, trace of cobbles; maximum particle size to 5 (127mm).	17	67	16	
1	8	-		Total Depth 18° (5.5m)				1 1
-6 2	0 -			Stability of vertical walls: Unstable 0 to 1° (0 to 0.3m) Stable 1 to 11° (0.3 to 3.4m) Unstable 17 to 15° (3.4 to 4.6m) Stable 15 to 18° (4.6 to 5.5m)				
2	2	<u> </u>	L			<u>L</u> _		
SUF Da Sui	ENCH DETAILS RFACE ELEVATION TE EXCAVATED RFACE GEOLOGIC ENCH LENGTH		: 24 A:	(1487m) Igust 1977 DRY LAKE VALLEY GREAT BASIN	. 1	NEV		

TUGRO NATIONAL, INC.

				Υ					PERCE	NT FIN	ER BY	WEIGHT		
ی دو	R (a)	SAMPLE I	NTERVAL		S.	TANDARD	SIEV	E OPEN	ING		U S	STAN	DARD S	IEVE
BORING	SAMPLE NUMBER			BLDRS.	COBE	LES		GRA	VEL			SA	ND	
88 2	S. ∃	FEET	METERS	24"	12"	6"	3"	11."	3 4"	3 8"	4	10	40	100
DL-B-12	SS-1	5.0- 5.8	1.52- 1.77	1										
	P-2	10.1- 10.7	3.08- 3.26	İ							1	† '	1	Ì
	T	10.7- 10.9	3.26- 3.32	1				†			1	100	92	7!
	T	10.9- 11.6	3.32- 3.54	1					1	j	Ī	1		Í
	B-3	13.5- 14.5	4.11- 4.42	1 1				100	8-	59	46	31	14	1.
	SS-4	I 15.0- 16.0	4.57- 4.88	Ĭ	,			l		100	98	91	59	1
	SS-6	26.0- 27.0	7.92- 8.23	I I				I	100	95	90	80	38	11
	P-7	31.0- 31.7	9.45- 9.66								L			
		31.7- 32.3	9.66- 9.85											
	L	32.3- 32.6	9.85- 9.94								I	100	93	7 (
		32.6- 33.3	9.94-10.15					L			L			
	P-8	40.7- 40.8	12.41-12.44	1	- 1					<u> </u>		100	75_	6!
	P-9	<u>51.3- 51.8</u>	15.64-15.79	L				1	L	L	100	90 _	55	3,4
L	P-10		18.50-18.56					1	.	1	1	100	89	7 :
L	P-11	70.7- 71.3	21.55-21.73					L	Ĺ	l	L	ļ		L
<u> </u>			21.73-21.79					ļ .				100	95	8(
	P-12		24.78-24.90	1							↓	100	92	7(
	P-13		<u>27.7</u> 7-27.83		L			ļ		L		100	99	8-
	P-14		30.51-30.69					ļ		 	<u> </u>	<u> </u>		1
·	ļ	101.4-101.9						ļ., , , ,		.	100	99	68	39
		126.3-126.8						ļ	ļ	ļ	1	100	94	_84
	P-16		45.72-45.93							.	ļ. —	ļ	ļ .	
ļ			45.93-46.12							L	L	ļ		
	 _	151.3-151.8						ļ		ļ	100	97	_77	45
	T		53.77-53.89					ļ			ļ	100	92	7€
	P-18		60.99-61.17	.				-	ļ	ļ			,	L
		201.3-201.5	61.36-61.42					ļ		ļ	100	90	50	41
	P-19	225.8-226.0	68.82-68.88	ļ						ļ	ļ	100	96	43
			76.63-76.69					.				100	99_	91
L	P-21	269.7-269.9	82.20-82.27						ļ 	Ļ		100		. 7 <u>9</u>
			82.54-82.66	├ ──┤				-				100	99	9:
	P-23	274.3-274.5	83.61-83.67	├ ──				ļ		 	100	96	68	5.2
	P-24		84.12-84.34	-				 						
	D 05		84.52-84.58									100		81
}	1		85.44-85.50	}					-	100	99	98		72
	P-26		86.35-86.50						<u> </u>	<u> </u>	100	100	98	85
 	P-27		87.26-87.42					├ ──		 	100	99	88	77
	P-28		88.18-88.27					<u>-</u>				100	96	86
			89.09-89.18	 -			<u> </u>	 	<u> </u>	<u> </u>	 -	100	92	77
	P-30		89.61-89.82	╂			ļ	├	<u> </u>	ļ	 -	 	ļ —	
			89.82-90.01								 	100	25	
	P-31		90.01-90.10 90.92-91.01	├				 -	 -			100	96 100	85 83
	- J	<u> </u>	1/∪・/た ジエ・∪よ			ı	I	i						. 6.1

NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System; Table A-1

SS - Standard split spoon

P - Pitcher

D - Fugro Brive

(d) *Indicates that test has been performed and results are included in this report.

B - Bulk

(b) NP - Not Plastic

								UT12-NI				COMPACTED				(Đ)	0 ×		8	
IEVE N	10	PARTICLE SIZE (mm)		ATTERBERG Limits (b)		USCS		DRY UNIT		CONTENT (°) SATURATION (°)		MAXIMUM ORY DENSITY (pcf) (kg m³)		SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	L	CONSOLIDATION		
	311	T OR C	OR CLAY				(c)	WEIGHT		MOISTURE Content (°)	TURA	22	DRY DENSITY			S ¥ S	=	100 M	DIRECT Shear	301
100	200	.005	.001	LL	PL	PI] ``'	(pcf)	(kg m ³)) N	SA	RA.	(pcf)	(kg m³)	음을	9289	<u>~</u>	50	급종	8
							ML			10										
		İ	<u> </u>		†	NP	ML		1				-	Ī	1	1 1	-	1		1
75	66	37	8				ML	78.5	1257	16	38	1.15		I		T 1		1	1	1
		I	I .		I]	ML	83.1	1331	14.1	37	1.03	-	I	Ι.	l 1	į	I	1 - 1	. 1
11	10		. ↓		ļ		GP-GÇ.		↓	1.				ļ <u>-</u>	ļ					I
19	10		ļ .		1	NΡ	SW-SM		ļ	4.					ļ	1 . 1				
. 12	5		ļ .		ļ		SW.		ļ] 3				ļ <u></u>						
			↓		↓ .	↓ .	ML	69.8	1118	16	<u>-</u>	1.41			ļ			ļ		
			<u> </u>	.		<u> </u>	ML	72.8	1166	_ 21.1	l .	1.36		 -	ļ		*	ļ		
76	69	20	5		-	NP.	ML.	.76.8	1230	19 ,	42	1.20				ļ		L		
		<u> </u>	<u> </u>		ļ	↓ .	ML -	84.2	1349	13.8	_37	1.00		 	 	<u> </u>		Ļi		
65	60	23_	8		 	 	ML		+			-		٠.	 		·	ł		. +
34. 79	2 <u>4</u> 71	20	,		ł	NP	SC .	82.8	1326	18	48	1.04			 	} ⊣				·· 🗼
/9	, / 1 ,	20	8		 	ΙÑΒ.	ML ML	76.7	1229	21	46 42	1.20		ł	 	 		 	· · 🛉	+
80	67	25	9				ML ML	75.6	1211	18.9	42	1.23			 -	1		*	· 	+
76	59	31	10	·	ł	NP	ML	75 0	1201	21	47	1.25		}	 	·		 		🕂
84	72	19	6		† - · ·	 ``	ML	75.0. 99.5	1201 1594		. 54	69		t	† -	† · · · · · · · · · · · · · · · · · · ·	-	† †	· - †	- +
04	, , , ,	1 1	† ~		İ	†	SC	81.3	1302	14.7	37	1.07			† · · · - - - · ·					·
39	29	ţ	<u></u>		1	1	şc	78.6	1259	20	48	1.14			†				· · †	- †-
_84	74	10	3		Ť · · · · · · · ·	NP	ML	78.3	1254	12		1.15.		T	†			1		
			1		İ		SC	89.2	1429	16.6	-5Ω	89		T	1	1 1		1 1	1	1
		<u> </u>	i		1	1	sc	93.2	1493	23.7	79	.81			†	†		* 1		†
45	38	1	Ţ .		Ť "	1	sc	80.9	1296	25	62_	1.08		<u></u>	1	1			†	
76	67	15	4				ML	73.1	1171		44	1.30				1				
							SM	87.7	1405	16.2	48	92							I	
41	38		<u> </u>		L	NP	SM	88.5	1418	25	_ 75	90								
43	26	6	2	· · · · · · · · ·			SM	87.5	1402	12	35	93			<u> </u>					
91	69]	14_	6		L	ļ	ML		İ										I	
79	50		-		ļ	NP	SM	82.7_	1325	35	91	1.04			L	L				
95_	90		ļ	42	26	16	CL	87.9	1408	29	86	.92			ļ	L			∔	
52	46				 		SM			!				ļ	 	├	·	├ ──┤		 -∔
					<u> </u>		MH	81.2	1301	24.9	_62	1.08		ļ						 -
81	70	31	8	61	45	16	MH		}							├ ─┤				
72		17		21	46	5	MH		 							 	·	├		
85 77	74 72	17_	4			 	MH	84.2	1349			1.00				├				∔
86	64			36	31	4	ML	73.7	1181			1.29			 	├		-		-+
77	65			- 50	├. <u>;</u> -	├── ┤	ML ML	82.2	1317			1.05			├					+
	- 55	-			 	-	ML	80.9	1296			1.08		ļ	 				 †	+
		<u> </u>	 -		 	 	ML	87.8 76.6	1406	18.2 36.8	54 83	.92			\vdash			*	 	+
85	72	38	10		t		ML	_/Q_Q	1-1-2-2-1	30.8	0.5	1.20			 			\vdash	·	
83		14	5				ML	82.7	1325	22	57	1.04			1					
																-				

SUMMARY OF LABORATORY T BORING DL-B-1 DRY LAKE VALLEY, NEVADA, G

MX SITING INVESTIGATION CEPARTMENT OF THE AIR FORCE

TUBRO NATION

	-SITU				OMBAGE								
-		Z			OMPACTE		S	p)	3 N		. S		
	MOISTURE Content (')	SATURATION	_	MAXI		OPTIMUM Moisture (†)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	. .	CONSOLIDATION	CHEMICAL	RELATIVE Density
	DIST DNTE	URA (°)	VOID RATIO	DRY DE	YTIZM	OPTIMUM Moistur (?)	NA I	1 A X	CON R	DIRECT	SOL		RELATIV Density
- ,	0.0	SAI	A A	(pcf)	(kg m³)	90 X	S 22 P	7.8	3 5	급종	NO.	3	2E 0E
	10												
	16	38	1.15				"					*	
57 31	14.1	3".	1.03				}				,		
						-	1	•			·		
	. 1												
	. 3	,											
LTΩ	16 21.1	3 <u>1</u>	1.41				L		L	l			
Լան	21.1		36					*	L				
:30. (2 £4	19 13.5	$\frac{42}{37}$	1.20 1.00						ļ		·		
الالان	 ;	_J	<u> </u>				h						
6.26	lo .	48	1.04				l — —		,				
29	21	46	1.20			· · · · · · · · · · · · · · · · · · ·		-					
11	18.9		1.23						*				
	,												
0.1	21	. 47	1.25										
594,	14 .	54	.69	l	 	ļ			ļ		L		
3 02	14.7		1.07		}	}							
259	20		1.14			 							
.5 4 :29:	12 16.6	27 50	.89		<u> </u>		· ·			-			
493	23.7	79	.81				f		f				
296.	25.		1.08		İ .	1							
:71		1	1.30										
105	16.2	48	.92										
418		75	-90		<u> </u>			-	.				
402	12	35	-93			-							
325	_35	_9 <u>1</u>	1.04			}			├ ──┤				
408		_ 86	92										
,	,	ab	-92		ļ	l							
301	24.9	62	1.08										
									L				
						ļ			ļ				
	20		1.00			ļ		<u> </u>					
	29		1.29			ļ ——							
	_20		1.05						├				
296.			1.08			 			├				
406 227		54 83	.92 1.20		 				*			*	
l		 _	4.20		 								
325	22	57	1.04										

SUMMARY OF LABORATORY TEST RESULTS

BORING DL-B-12

DRY LAKE VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION CEPARTMENT OF THE AIR FORCE. SAMSO

B-1

		_	_		_		_	_	_	_	_	_	-	т-	,	_	 -	,	_	,	,	,	_	_	,	_	,	 _
HEIGHT	DIAMETER	2.0	2.4	2.4	2.4	2.4	2.4	2.2	2.2	2.4	2.4	2.4	2.4															
DEGREE OF	(%)	78.7	68.1	36.6	68.6	84.4	41.6	79.3	82.9	36.0	57.0	64.7	78.3															
MOISTURE	(%)	40.5	33.0	14.1	16.9	30.7	18.9	23.7	36.8	10.3	20.9	22.4	36.4															
DRY DENSITY	kg/m3	1129	1169	1281	1621	1320	1171	1493	1221	1251	1357	1395	1197															
DRY DI	pcf	70.5	73.0	82.5	101.2	85.0	75.6	93.2	76.6	95.3	84.7	87.1	74.7															
IF I NED TRENGTH	kN m2	517	345	115	201	101	221	723	453	155	321	393	326															
UNCONFINED	kst	10.8	7.2	2.4	4.2	2.1	4.6	15.1	9.5	3.2	6.7	8.2	8.8															
1108	TYPE	HW	NS.	Mľ	ML	HL	ĦĹ	MS	ML	NS	ML	MH	J#I															
INTERVAL	METERS	4.66-4.85	8.14-8.32	2.32-3.54	35, 97-36, 18	55.05-55.23	21.55-21.73	45.93-46.12	89.82-90.01	1.52-8.69	15.24-15.45	3.05-3.26	21.88-22.07															
SAMPLE	FEET	15.3-15.9	26.7-27.3	10.9-11.6	118.0-118.7	180.6-181.2	70.7-71.3	150.7-151.3	294.7-295.3	5.0-5.7	50.0-50.7	10.0-10.7	71.8-72.4															
SAMPLE		P3	P-5	P-2	P-16	P-19	P-11	P-16	P-30	P-1	P-8	P2	P-10															
9	NO.	01-8-5		01-8-8			01-8-12			01-8-18		01-8-19																

SUMMARY OF UNCONFINED COMPRESSION TEST RESULTS DRY LAKE VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE B-2

							_									•
BACK PRESSURE	kN/m^2	0	0	0	0	0	0	0	0	0						
PRES	ksf	0	0	0	0	0	0	0	0	0						
STRAIN	Ü	11.	11.	01.	Ξ.	0.	9.	01.	.09	. 09						
MAXIMUM DEVIATOR TRESS ($\mathcal{O}_1 - \mathcal{O}_2$)	kN/m ²	1680	819	1235	2571	1412	900	541	704	1925						
1		35.1	17.1	25.8	53.7	29.5	18.8	11.3	14.7	40.2						
NING RE(O ₃)	kN/m^2	469	235	670	1331	359	171	96	168	316						
CONFINING PRESSURE (03)	ksf	9.8	4.9	14.0	27.8	7.5	3.7	2.0	3.5	6.6						
MOISTURE CONTENT	(%)	5.3	0 " L	34.1	27.8	13.8	17.4	10.3	6.2	22.5						
DENSITY	kg/m^3	1533	1643	1291	1323	1349	1193	1211	1571	1251						
DRY DI	pc f	95.7	102,6	90°8	82.6	84.2	74.5	98.1	98.1	78.1				}	}	
TYPE OF	TEST	CO	C)	O)	00	gg	9	8	00	C)						
1108	TYPE	SP	SP	H	ML	ML	H	SP	SP	SM						
INTERVAL	METERS	15.54-15.73	15.24-15.45	42.67-42.89	54.86-55.05	9.94-10.15	9.66-9.85	6.10-6.28	6.28-6.46	9.54-9.72						
SAMPLE	FEET	51.0-51.6	50.0-50.7	140.0-140.7	180.0-180.6	32.6-33.3	31.7-32.3	20.0-20.6	20.6-21.2	31.3-31.9						
SAMPLE	M.U.	P-8	P-8	L1-4	P-19	P-7	P-7	P-4	þ-4	9-d						
9	NO	8-8-10				01-8-12		81-8-10		01-8-18						

SUMMARY OF TRIAXIAL SHEAR TEST RESULTS DRY LAKE VALLEY, NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

B-3

BORING	SAMPLE	SAMPLE 1		SOIL	NORMAL	STRESS	MAX! SHEAR S	TRENGTH
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m²	ksf	kN/m ²
0L-B-8	P-14	90.0-90.6	27.43-27.61	MZ	9.0	431	6.4	306
DL-8-13	P-10	80.0-80.7	24.38-24.60	SW-SM	8.5	407	5.7	273
	P-17	225.0-225.7	68.58-68.79	SP-SC	12.0	575	8.2	393
DL-B-18	P-6	30.0-30.7	9.14-9.36	SM	3.0	144	3.7	177
						[
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		-						
							<u> </u>	
					<u>_</u> .			
				1				
			-	 -	•		<u> </u>	

SUMMARY OF DIRECT SHEAR TEST RESULTS DRY LAKE VALLEY, NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

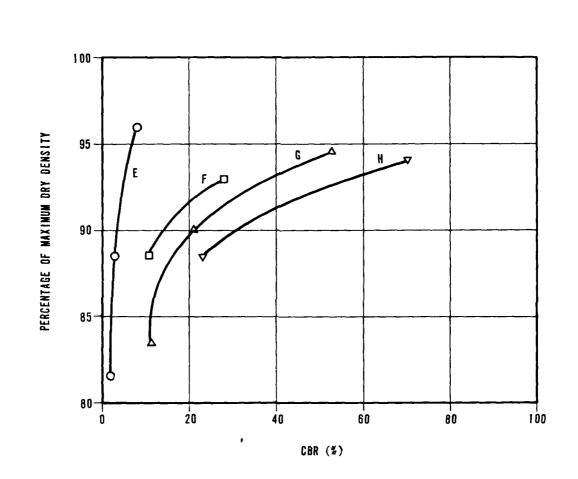
TABLE B-4

COMPOSITE	SOIL	PERCENT PASS ING	ATTERBERG LIMITS	TTERBERG Limits	SPECIFIC	L	MAXIMUM ORY DENSITY	OPT INUM MOISTURE	COMPACTED DRY DENSITY	CTED	COMPACTED	PERCENT OF MAXIMUM	CBR
NUMBER	ITPE	#200	11	Ы	GKAVIIT	pc f	kg/m3	(%)	pcf	kg/m3	(%)	DRY DENSITY	(%)
									106.2	1701	14.2	95.8	8
									98.2	1573	15.0	9.88	က
ш	⊒	89	24	2	2.59	110.8	1775	16.5	90.3	1446	14.7	91.5	2
				3									
									119.4	1913	9.8	92.9	28
					-				113.9	1825	8.8	88.6	11
L	S	91			2.57	128.5	2058	8.5					
					·								
									102.7	1645	18.1	94.7	53
									97.7	1565	18.4	0.08	21
6	ES.	4			2.55	108.5	1738	18.0	90.06	1451	18.4	83.5	11
								•					
									116.7	1869	9.3	94.1	70
									109.8	1759	9.5	98.6	23
=	S	91	•		2.60	124.0	1986	10.0			_		
			-										

CALIFORNIA BEARING RATIO
(CBR) TEST RESULTS
DRY LAKE VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

B-5



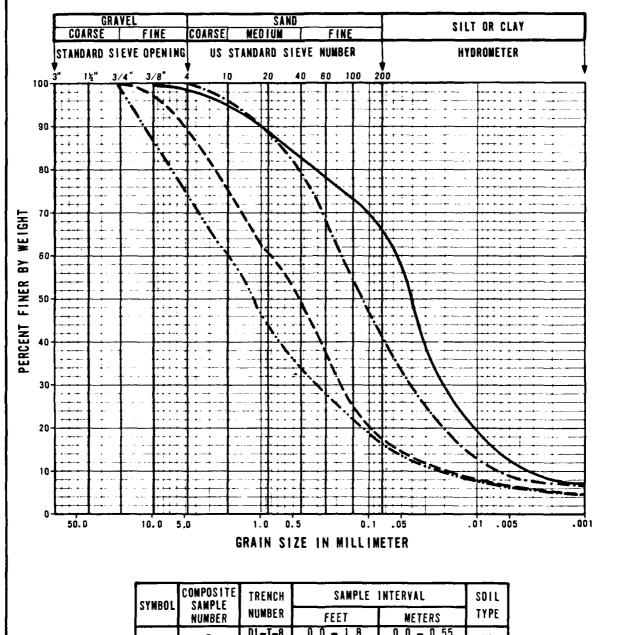
SYMBOL	COMPOSITE Sample Number	SOIL TYPE
0	E	ML
	F	SM
Δ	G	MZ
▽	H	SM

CALIFORNIA BEARING RATIO
(CBR) CURVES

DRY LAKE VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

B-7



SYMBOL	COMPOSITE SAMPLE	TRENCH	SAMPLE	INTERVAL	SOIL
SIMBUL	NUMBER	NUMBER	FEET	METERS	TYPE
	E	DL-T-8 DL-T-8	0.0 - 1.8 3.0 - 5.0	0.0 - 0.55 0.91 - 1.52	ML
	F	DL-T-17 DL-T-15	0.0 - 1.0 $8.0 - 10.0$	0.0 <u>- 0.30</u> 2.44 <u>- 3.05</u>	SM
	G	DL-T-12 DL-T-12	17.0 - 18.0 BLEND	5.18 - 5.49	MZ
	Н	01-1-11	7.0 - 9.0 14.5 - 15.5	2.13 - 2.74	SM

GRAIN SIZE CURVES. CBR TESTS
DRY LAKE VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAWSO

B-8

<u>ugro national, inc.</u>

APPENDIX C
GEOTECHNICAL DATA - RALSTON VALLEY

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LOG OF TRENCH RV-T-8	Figure C-4
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CALIFORNIA BEARING RATIO (CBR) CURVES	Figure C-7
GRAIN SIZE CURVES, CBR TESTS	Figure C-8

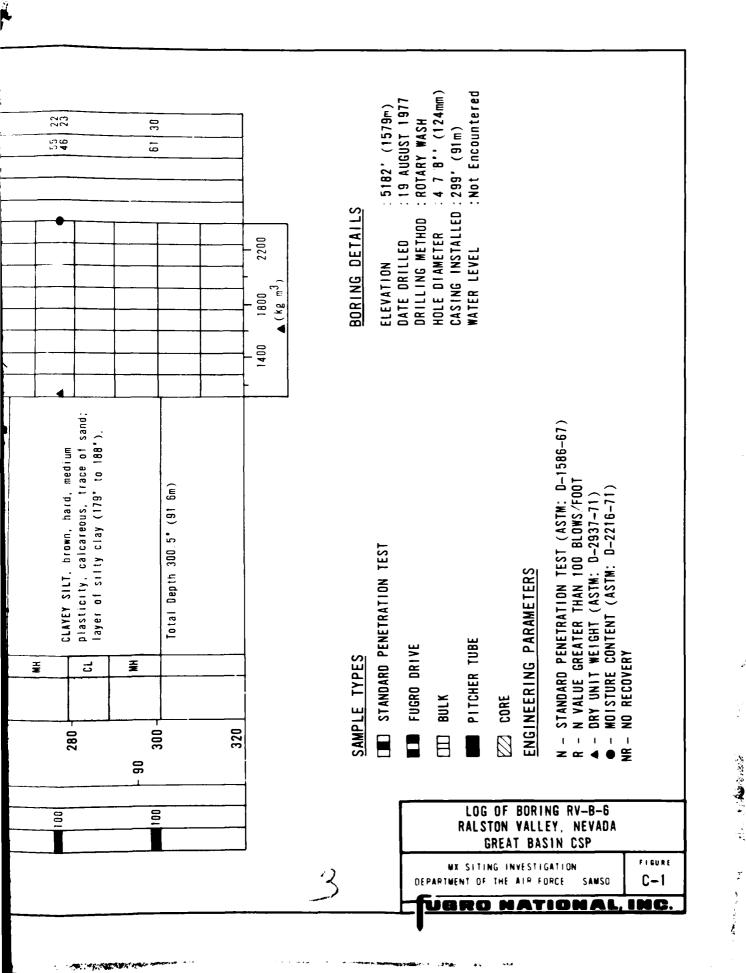
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	=	<u> </u>	-		36						<u>,</u>					
[<u>~</u>	+	63	37	30		38	18	,	89	ري دي	43	13	43	4	91	
SIEVE	SA	37	63	7.0		09	82		52	44	5.6	95	57	83	69	
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pcf 10 1		L						-								
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	<u> </u>											y, f suba	:rac (0° elly			
	SOIL DESCRIPTION											SILTY SAND, light gray, fine to medium, dense to very dense, subangular to	angular, calcareous, trace of gravel; layers of sandy silt (0° to 2° and 60° to 62°), layer of gravelly sand (19°	10 22').		
202			200		SP			3 8		量		SILTY SAND, light giay, f dense to very dense, subar	angular, calcareous, traclayers of sandy silt (0° to 62°), layer of gravelly	to 22').	S	
	sn	JM V	200	,	SP			* S		IW A		SILTY SAND, light giay, f dense to very dense, subar	angular, calcareous, traclayers of sandy silt (0° to 62°), layer of gravelly	10 22').	X	
есг Ногоел	sn	JM Z Z O	2		20 - SP			40 - 34		N		80 - SILTY SAND, light giay, f dense to very dense, subar	angular, calcateous, trac layers of sandy silt (0° to 62°), layer of gravelly	100	120 - SM	
SOS HOFOCA	n2 F111						-10			09	n 7 - 2 n			- 1		
S02 H0100k	N W WETE LITE	0							001	09	100			- 001		

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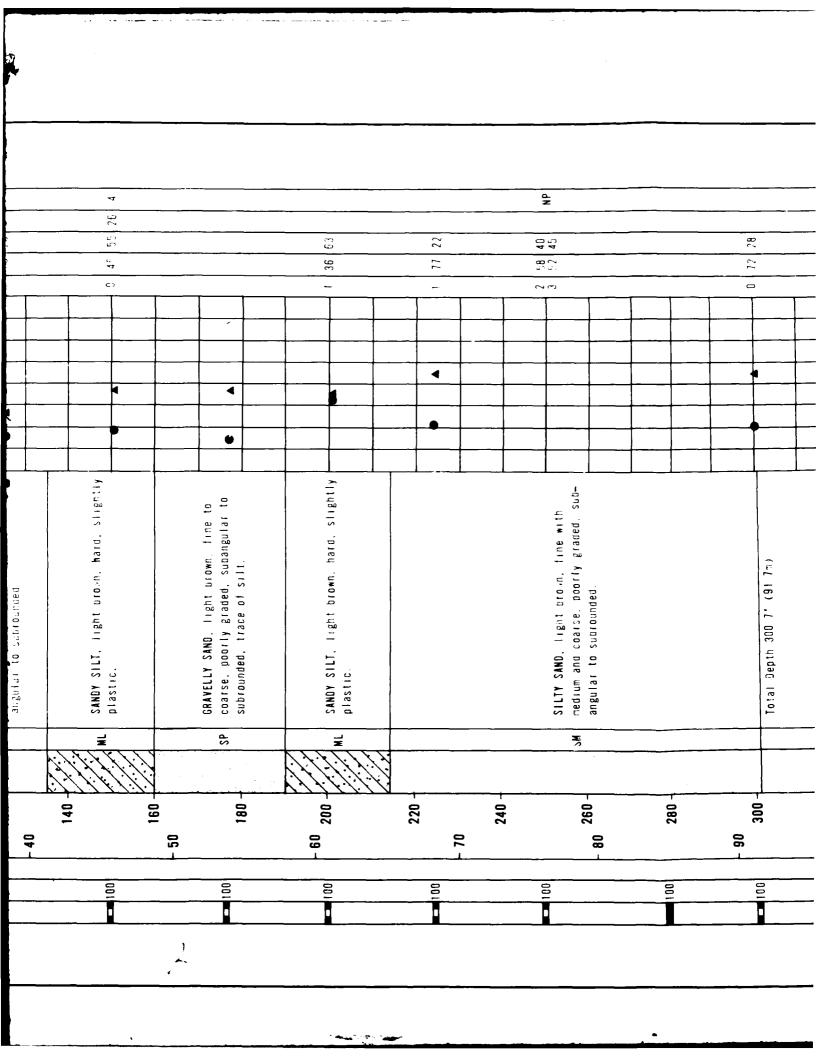
SILTY CLAY, brown, hard, medium plasticity, calcareous, with a little sand. CLAYEY SILT, brown, hard, medium plasticity, calcareous, with a little sand. SAND, brown, fine to coarse, poorly graded, very dense, subangular to submounded, trace of silt, trace of gravel. CLAYEY SAND, brown, fine with medium, poorly graded, very dense, subangular to submounded, calcareous. CLAYEY SAND, brown, fine with medium plasticity, calcareous, trace of sand; to subrounded, calcareous, trace of sand; layer of silty clay (179° to 188°).	SILTY CLAY, brown, hard, medium plasticity, calcareous, with a little sand. CLAYEY SILT, brown, hard, medium plasticity, calcareous, with a little sand. SAND, brown, tine to coarse, poorly graded, very dense, subangular to sub-graded, trace of silt, trace of graded, very dense, subangular to sub-graded, very dense, subangular to subrounded, calcareous, trace of sand; to subrounded, calcareous, trace of sand; layer of silty clay (179' to 188').	SILTY CLAY, brown, hard, medium sand. CLAYEV SILT. brown, hard, medium plasticity, calcareous, with a little sand. SAND, brown, fine to coarse, poorly sand. SAND, brown, fine to coarse, poorly tounded, trace of silt, trace of gravel. CLAYEV SAND, brown, fine with medium. CLAYEV SAND, brown, fine with medium. CLAYEV SAND, brown, fine with medium. CLAYEV SILT, brown, hard, medium to subrounded, calcareous. CLAYEV SILT, brown, hard, medium to subrounded, calcareous, trace of sand; layer of silty clay (179° to 188°).	160 -	- 180	- 60 200 -	220 -	240-	280	- 000 - 001
SILTY CLAY, brown, hard, medium plasticity, calcareous, with a little sand. CLAYEY SILT, brown, hard, medium plasticity, calcareous, with a little sand. SAND, brown, fine to coarse, poorly graded, very dense, subangular to subfrounded, trace of silt, trace of gravel. CLAYEY SAND, brown, fine with medium, poorly graded, very dense, subangular to subrounded, calcareous. CLAYEY SAND, brown, fine with medium, poorly graded, very dense, subangular to subrounded, calcareous, trace of sand; layer of silty clay (179° to 188°).	SILTY CLAY, brown, hard, medium plasticity, calcareous, with a little sand. CLAMEY SILT, brown, hard, medium plasticity, calcareous, with a little sand. SAND, brown, fine to coarse, poorly graded, very dense, subangular to sub-rounded, trace of silt, trace of gravel. CLAMEY SAND, brown, fine with medium. CLAMEY SAND, brown, fine with medium. Doorly graded, very dense, subangular to subrounded, calcareous. CLAMEY SILT, brown, haid, medium plasticity, calcareous, trace of sand: layer of silty clay (179° to 188°).	SILTY CLAY, brown, hard, medium plasticity, calcareous, with a little sand. CLAYEY SILT, brown, hard, medium plasticity, calcareous, with a little sand. SANO, brown, fine to coarse, poorly graded, very dense, subangular to sub-rounded, trace of silt, trace of gravel. CLAYEY SANO, brown, fine with medium. CLAYEY SANO, brown, fine with medium. CLAYEY SANO, brown, fine with medium. Districtly, calcareous, trace of sand: layer of silty clay (179° to 188°).		10	臺			불 13	표
				SILTY CLAY, brown, hard, medium plasticity, calcareous, with a little sand.	CLAYEY SILT, brown, hard, medium plasticity, calcareous, with a little sand.		CLAYEY SAND, brown, fine with medium, poorly graded, very dense, subangular to subrounded, calcareous.		Total Depth 300

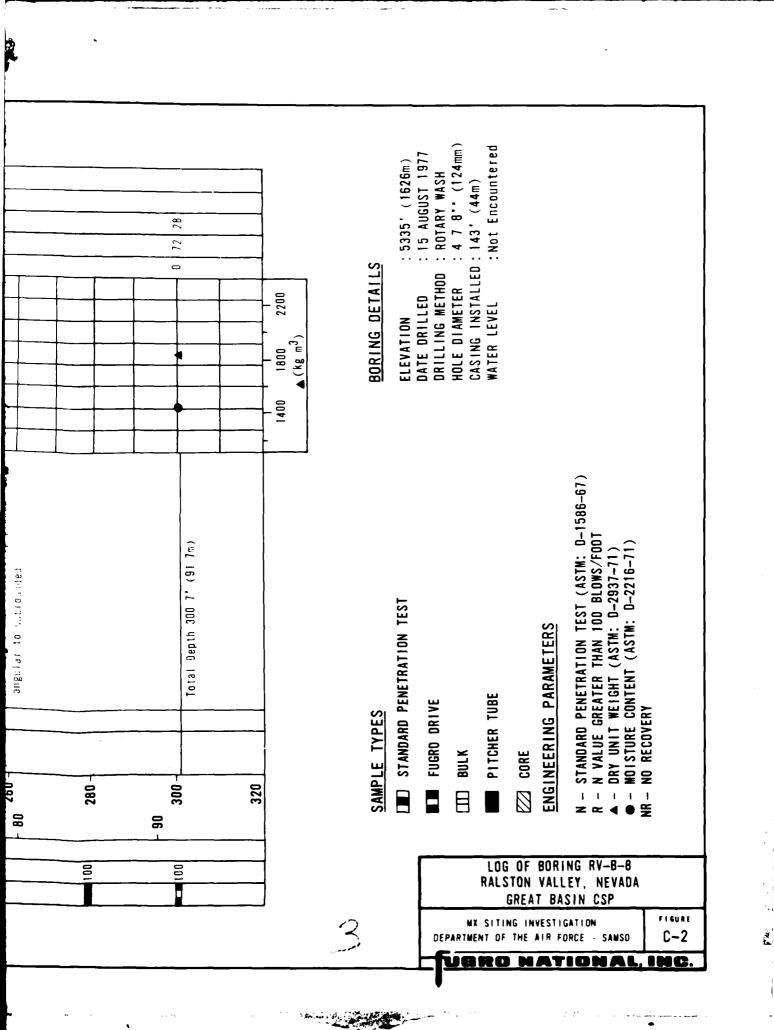
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	SOIL DESCRIPTION		GRAVELLY SAND, brown, tine to coarse,	poorly to well graded, loose to dense, subangular to subrounded, trace of silt,	with a little clay (20° to 45°).		CANOY GRAVEL, fight gray brown, fine with medium, well graded, very dense subangular to subrounded, trace of srit.			GRAVELLY SAND, light brown, fine to coarse, well graded, very dense, sub-	_			angular to subrounded.
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_	11			35	34									
] =			20	13									

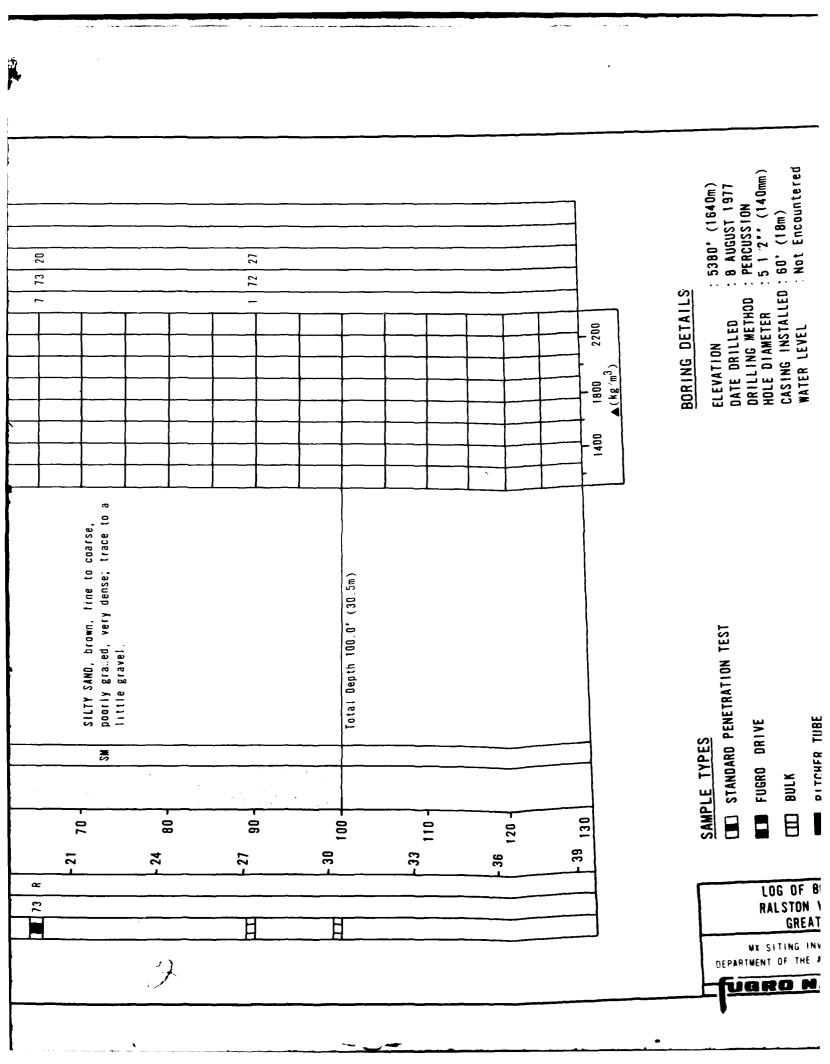


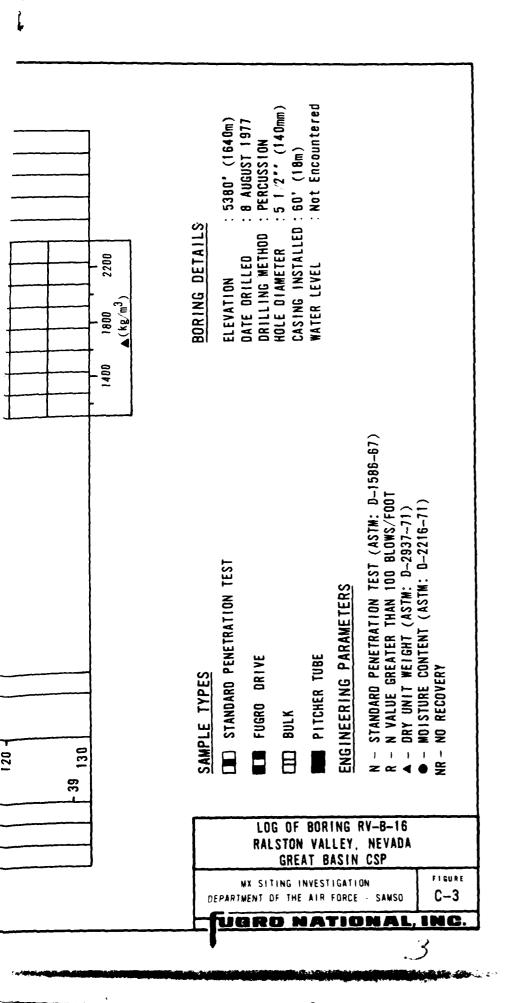


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	PT			ne							
	SOIL DESCRIPTION			SANDY GRAVEL, brown, fine to medium, loose to medium dense, subrounded,	trace of silt.						
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	NOS			SANDY	t race						
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FT	LITHOL USCS	0	10	20 -000 SANDY	300000000000000000000000000000000000000	40					~
3U. 를 30.	METERS FEET LITHOL USCS	0	10	20 -000 SANDY	300000000000000000000000000000000000000	40					13 R

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BULK SAMPLE	METERS TO FEET TO	L 1 THOLOGY	nscs	CONSISTENCY	2011	DESCRIPTION		SIEV			
<u>m</u>		1 5		CON	3016		GR	SA	FI	LL P	21
Щ	0 0			Loose							
	2 · · · · · · · · · · · · · · · · · · ·		SP	Medium dense			34	63	3		
	-3 ₁₀ .				maist to very mais	wn, fine to coerse, slightly t, subangular to subrounded, low 9° (3m), trace of silt; ize to 1.5°° (38mm).					
	12 - - 4 14 ·		SW-	Bense							
П	16 - -5				Total Depth 18° (5.	5m)	41	53	8		
	-8 20 -					ty of vertical walls: e O to 9° (O to 2.7m) g to 18° (2.7 to 5.5m)					
	22	<u> </u>	Ш	<u>}</u>						上	ل
	SURF DATE SURF	CH DETAILS ACE ELEVATION EXCAVATED ACE GEOLOGIC CH LENGTH		: 20 Au	gust 1977	LOG OF TRENCH RALSTON VALLEY GREAT BASI	', N	EVA			
		CH ORIENTATIO	IN	: N70E	· · · · · · · ·	MX SITING INVESTIGAT	I ON			FI	GU

BULK SAMPLE	WETERS	tH E	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION		IEV ALY:	E SIS	
BG.		FEET	[1]		CO	SOIL DESCRIPTION	GR	SA	FI	LL PI
	0	0			L00 56					
	- 1 - 2	6		SP- SM		· CONSTITUTE DAMP. house discussed days	38	55	7	
	-3 -4	10 12 14		SW-	Dense	GRAVELLY SAND, brown, fine to coarse, dry, subangular, weakly cemented, trace of silt, trace of cobbles at 12° (4m); maximum particle size 8° (200mm).	30	61	9	
	-6	18 - 20 -				Total Depth 18" (5.5m) Stability of vertical walls: Stable O to 18" (O to 5.5m)				
<u></u>	<u>L</u> .	22	L	<u> </u>						<u> </u>
	_		CH DETAILS CE ELEVATION			(1703m) LOG OF TRENC	H RV	. T -	10	

SURFACE GEOLOGIC UNIT : A5y
TRENCH LENGTH : 65' / 20m)
TRENCH ORIENTATION : N70W

GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAMSO FIGURE

BULK SAMPLE	METERS JABO	9070	uscs	CONSISTENCY	2011	DESCRIPTION	- 1	SIEV ALY:	i	
<u>ā</u>				CON			GR	SA	FI	LL P
			ML	Soft	SANDY SILT, brown, calcareous, trace o	moist, slightly plastic, f cobbles, trace of boulders.				19
	2	(<u>////</u>		Medium dense						
	3 1	2	SW-	Dense	slightly moist, su	ht brown, fine to coarse, bangular to subrounded, cal- silt; maximum particle size	29	63	8	
	1 <i>(</i> 5	; - 1	SM	Medium dense			28	59	13	
	6 24 21) -			Unstab!	5m) ty of vertical walls: e				
			<u> </u>	L	<u> </u>				1	
	SUR Dat Sur	NCH DETAILS FACE ELEVATION E EXCAVATED FACE GEOLOGIC NCH LENGTH	UN I 1	: 19 Au : A5i	(1811m) gust 1977 21m)	LOG OF TRENCH RALSTON VALLEY GREAT BASIN	, NE	VA		
		NCH ORIENTATI			& CH /	MX SITING INVESTIGATI				FI

									PERCEN	IT FINE	ER BY W	EIGHT		
G ~	R (a)	SAMPLE 1	NTERVAL			TANDARD	SIEV						DARD S	IEVE NO
BORING	SAMPLE NUMBER	ł		BLDRS.	COBB	LES		GRA	VEL			SAN	10	
8 3	S. ∃	FEET	METERS	24"	12"	6"	3"	11.11	3 4"	3 8"	4	10	40	100
RV-B-6	P-1	5.0-5.7	1.52-1.74							'		100	91	61
	P-2	10.0-10.7	3.05-3.26							l	Ţ	- 1		
	P-3	15.7-16.3	4.79-4.97						[i	[]		100	97	68
	P-4	20.0-22.7	6.10-6.92			{	[]		100	91	82	69	29	7
	P-5	25.0-25.7	7.62-7.83	[]	ì	1		ļ .	<u> </u>	100	98	94	76	54
	P-6	30.0-30.8	9.14-9.39	(<u> </u>	. 1	()	L	<u>L</u> i		1	100	99	89	47
	P-7	40.0-40.8	12.19-12.44	<u> </u>	أ	نــــا	نــــا	L	<u></u> i	<u> </u>	L1]		<u></u>
	P-8	50.1-50.9	15.27-15.51			تــــا				نـــا	<u></u>	100	97	85
	P-9	60.1-60.9	18.32-18.56	\Box			ــــا		ــــا	Ĺ <u></u>		100	99	89
	P-10	70.1-70.8	21,37-21.58	\Box		L1	[]		L	100	99	98	90	75
	P-12	80.1-80.8	24.41-24.63				نـــا	<u></u>	<u></u>	100	98	94	66	30
<u> </u>	P-13	90.1-90.8	27.46-27.68	ļ l		1	ļ .			<u> </u>	100	97	82	70
	P-14	100.1-100.8	30.51-30.72	L		1 - 4	L - 4	L	L	100	98	91	67	33
<u> </u>	P-15			L	1	<u> 1</u>	L	ļ	100	97	85	72	56	41
<u> </u>	P-16	149.1-149.8	45.45-45.66	L		L1	L	L	L	L1	L		<u></u>	LI
<u> </u>	P-17		53.68-53.92	 	1	ļ <u>.</u>	1. 1	ļ	ļ 1	L]	t = 1	t = 1	1 1	ļ l
		176.1-176.9	53.68-53.92	! l		<u> </u>	د	L		LÌ	L1	<u> </u>		L
		176.9-178.6	53.92-54.44	ļl		ļ. j	4	L		<u> </u>	L	L		L . .
	P-18	200.2-201.0_		ţl		 	 _			L	L	L	L1	ļ
L		200.2-201.0		ļ l	ļ	1 4			—	L	L4		<u> </u>	Ļ ļ .
	P-19	227.5-228.2	69.34-69.56	, 1				ļ,		100	95	81	40	15
	P-20	250.1-250.9	76.23-76.47	 		<u> </u>					<u> </u>	100	92	70
		250.1-250.9		L _l		L	<u> </u>	ļ	L			L1	<u>'</u>	<u> </u>
]		276.1-276.8	84.16-84.37	L- 1		L1	نـــــــــــــــــــــــــــــــــــــ				نسا	ĹÌ	L	
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NOTES:

- (a) Sample types (c) USCS Unified Soil Classification System; Table A-1
 - SS Standard split spoon
 - P Pitcher
 - D Fugro Drive
 - B Bulk
- (d) *Indicates that test has been performed and results are included in this report
- (b) NP Not Plastic

							<u> </u>	$\overline{}$			N-SITU		\neg		COMPACTE	<u></u>	—т	<u> </u>			
NDARD S	IEVE N	0	PARTI SIZE	ICLE (mm)		TERBE Mits (uscs	DRY U	UNIT		SATURATION (%)		MAXI		OPTINUM MOISTURE (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	<u> </u>	NOTTECT
AND			T OR C	LAY	Ļ,			(C)	WEIG		MOISTURE Content (2)	(%)	VOID RATIO	DRY DE	ENSITY	PTIM DIST	SAY I	¥	MCON	DIRECT SHEAR	100
40	100	200	. 005	.001	LL	PL	PI	 l	(pcf)	(kg. m ³)		-	++	(pcf)	(kg m³)	0 🗷	222	<u> </u>	53		ا م
91	61	37	9	4				SM	87.0	1394	8.4	24	,93				1			*	$\lfloor - \rfloor$
1	!]	1	' I		[]	L _		SM	103.0		6.5	28	.64	·	L	1	<u></u>		<u>'</u>	*	_
97	68	30	' 1	ļ j			1	SM	97.4	1560_	5.7	21	. 73	'	Ļ	1	ı l	'. <u>]</u>	']	* 1	
29	7	4	2	1	36	25	11_	SP	75.6	1211	30.0	66	1.23	1	ļ	1	<u>. </u>	'. I	*]	! . ₄	ļ
76	54	38			ļ	-	ļ ļ	SM_	90.5	1450	20.9	65	.86	<u></u>	 		1- En	<u></u>	L	L	-
89	47	18	'- 4	├ -	-	f - 4	+ 1	SM	93.5	1498	11.5	39	.72	<u>'</u>		1	2.58	<u>'</u>	└ ── ∤	L1	-
+	<u>├</u> ┤		١	 	-			SM	110.1		13.8	70	.74	L	 	+	├ ──┪	*	├		+
97	85	48	11	1 -		-		SM	97.0	1554	$\begin{array}{c} 8.6 \\ 15.4 \end{array}$	32 47		'	+	+	2.59	<u>└</u> ~~		F 1	t
99	89 75	56 43	11	7	 	$\vdash \neg$		ML SM	89.2 92.3	1429	11.9	39	.81	L		+	12.33	*		 -	 -
90	30	13	·		├ ¬	1-1		SM SM	102.7		16.7	70	.64	L	 	 	 			+	†-
82	70	43	<u></u>	1		†	+1	SM SM	107.0		18.7	88	.57		 	+	+ 1	*	 	 -	†
67	33	14		1			1-1	SM	107.0		14.4	65	.59	·	†		1	-	!	T	1
56	41	16	5	1	† 7	t	† -1	SM	97.€	1563		70	.73		1	1	1	t '	1		
T ~ 1						1		SM	96.6	1547	17.1	62	.74	1	T		T	Ţ			
1	ŗ †		1	[]	46	23	24	CL	94.4	15.	24.9	86	.78	<u></u>	L	L	<i>1</i>	[1
1	1	†]					CL	89.3	1430	30.6	93	.89	T	[1	*		1
<u>'</u>		82	·					CL	84.0	1346		96	1.01	1				L	*	L	ļ
↓ l		. 1	'. <u> </u>		66	37	29	МН	74.4	1192	44.3		1.15	1		<u></u>	2.56	L	*	L	1
↓			·	<u> </u>	L	<u></u>	<u>[]</u>	мн	75.7	1213	41.5	91	1.23	!	ļ		L	L	-	-	1
40	15	7	'	1 1	1	1	1 1	SP-SM	110.2		16.3	.84	.53	<u>.</u>	1	+	1		*	-	+
92	70	40	13	7	38	22	16	SC	3.88	1422	28.8	87	.90	L			_	L	ļ	-	+
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+	L		<u>'</u>	 	55	34	22	МН	80.4	1288	36.9	91	1.10	<u> </u>	 	+	}		*	 	+
+	<u></u>	 ↓	·——	\vdash	61	31	30	МН	-	Ļ		<u> </u>	1	<u> </u>		+			-	 	+
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SUMMARY OF LABORA BORING RALSTON VALLEY, NEVA

WX SITING INVEST. CEPARTMENT OF THE AIR F

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		MAX	MUM	35	2 × C	AL (INEI		JATE	11	ے ج
	YOID RATIO	DRY DE	NSITY	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT Shear	CONSOLIDATION	CHEMICAL	RELATIVE DENSITY
	Y S	(pcf)	(kg m³)	P OM	2 22 P	T.R	300	SH	SOS	3	풀삠
П	.93							*			
	.64							*			
	. 73						*	*		*	
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	.72				2.58						
	.53			·	2.30		 			·	1
	.74			ļ		*					
				İ	2.59						
• 1	. <u>81</u> .83					*					
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SUMMARY OF LABORATORY TEST RESULTS
BORING RV-B-6

RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

UBRO NATIONAL, INC.

TABLE

C-1

			_			,								 ,	 ,		 	 · · · · ·	 	 ,	_	
HEIGHT	DIAMETER	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4									
DEGREE OF	(%)	92.6	58.5	93.0	96.7	94.5	94 3	91.0	92.3	73.4	72.0	64.5	68.1									
	(%)	40.8	23.3	30.6	37.3	44.3	32.3	36.9	1.94	20.1	13.8	24.2	12.0									
NSITY	kg m3	1233	1301	1430	1322	1192	1403	1288	1149	1521	1762	1339	1829									
DRY DENSITY	pcf	77.0	81.2	89.3	82.5	74.4	87.6	80.4	71.7	96.8	110.0	83.6	114.2									
IF I NED Frength	kn m²	134	101	259	311	263	378	407	230	335	689	134	282									
UNCONFINED COMP. STRENGTH	kst	2.8	2.1	5.4	6.5	5.5	7.9	8.5	4.8	7.0	14.4	7.8	6.1									
7108	TYPE	SM	SP	CL	70	¥	SC	至	¥	Mí	Ä	J.	NS.									
NTERVAL	METERS	75.29-75.53	6.10-6.31	53.68-53.92	54.25- 54.44	61.02-61.26	76.78~76.39	84.16-84.37	91 26-91 41	6.10-6.34	9.14-9.39	24.69-24.90	76. 26-76. 47									
SAMPLE INTERVAL	FEET	247.0-247.8	20.0-20.7	176.1-176.9	178.0-178.6	200 2-201 0	251.9-252.6	276.1-276.8	299, 4-299, 9	20.0-20.8	30.0-30.8	81.0-81.7	250.2-250.9									
SAMPLE	. NO.	P-20	P-4	P-17	P-17	P-18	P-20	P-21	P-22	P-4	P-6	P-11	0-19									
9	NO.	RV-B-1	RV-B-6							RV-8-7			RV-8-8									

SUMMARY OF UNCONFINED COMPRESSION TEST RESULTS

RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

C-2

ugro national, inc.

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BACK	kN/m	0	0	8	_	-	0	-	0	0	0	0	-	0	-	0	0	0	0	0	0	-
PRE	ksf	0	0	0	0	0	0	-	0	0	0	-	-	0	0	0	-	0	0	0	0	-
STRAIN	(°, m	.07	.07	70.	.07	60 .	.07	.07	.07	.07	70.	70.	.07	.07	70.	70.	90.	.07	70.	70.	£0 ·	.07
MAXIMUM DEVIATOR TRESS(O:-O3)	kN/m ²	694	1230	1747	1297	3083	5295	2159	1125	7995	627	694	1436	1532	2628	5803	369	867	2178	417	1029	1288
MAXI DEVI STRESS	ksf	14.5	25.7	36.5	27.1	64.4	110.6	45.1	23.5	167.0	13.1	14.5	30.0	32.0	54.9	121.2	1.1	18.1	45.4	8.7	21.5	26.9
€ 6 (σ₃)	kN/m²	8.1	192	426	263	594	1288	474	967	2135	1.8	182	412	263	809	1484	57	158	421	57	139	278
CONFINI PRESSURE	ksf	1.1	4.0	8.9	5.5	12.4	26.9	9.9	20.2	44.6	1.1	3.8	8.6	5.5	12.7	31.0	1.2	3.3	8.8	1.2	2.9	5.8
MOISTURE	(%)	8.2	5.4	8.8	8.5	8.8	14.6	13.3	10.3	12.7	13.1	9.1	1.7	12.1	8.3	15.8	12.6	7.8	7.4	11.6	5.4	9.7
NSITY	kg/m ³	17 25	1901	1752	1892	1884	1643	1744	1945	1767	1772	1615	1619	1495	1525	1701	1608	1855	1873	1796	1865	1786
DRY DE	pc f	107.7	118.7	109.4	118.1	117.6	102.6	108.9	121.4	110.3	110.6	100.8	101.1	93.3	95.2	106.2	100.4	115.8	116.9	112.1	116.4	111.5
TYPE 0F	TEST	CD	CO	CO	CO	8	63	CD	8	CO	00	8	3	23	CO	00	00	00	co	co	CD	93
11	IV PE	SP-SM	GP-GM	SC	SC	SC	NS-WS	NIS	SIM	SH	SIE	SP-SH	SM	SIK	SM	SM	SP-SM	MS-MS	sc	GP-GM	SW-SM	WS
INTERVAL	METERS	4.72-4.88	6. 25-6. 40	7.62-7.92	15.39-15.54	18.65-18.81	21.43-21.58	27.49-28.01	30.54-30.69	39.08-39.23	4.57-4.82	6.10-6.34	7.62-7.86	15.27-15.51	21.37-21.58	27.46-27.68	3.26-3.41	4.66-4.82	6.22-6.37	3.11-3.32	4.69-4.85	6.19-6.34
SAMPLE	FEET	15.5-16.0	20.5-21.0	25.0-26.0	50.5-51.0	61.2-61.7	70.3-70.8	90.2-91.9	100.2-100.7	128.2-128.7	15.0-15.8	20.0-20.8	25.0-25.8	50.1-50.9	70.1-70.8	90.1-90.8	10.7-11.2	15.3-15.8	20.4-20.9	10.2-10.9	15.4-15.9	20.3-20.8
SAMPLE	2	0-3	0-4	0-5	0-8	6-0	D-10	D-13	D-14	0-15	P-3	P-4	P-5	P-8	P-10	P-13	2-0	0-3	4-0	D-2	D-3	0-4
g Q	. 0	RV-8-1									RV-8-5			RV-B-6			RV-B-8			RV-8-12		

SUMMARY OF TRIAXIAL SHEAR TEST RESULTS
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION CEPARTMENT OF THE AIR FORCE. SAMSO

C-3

BORING	SAMPLE	SAMPLE I	NTERVAL	SOIL	NORMAL	STRESS		MUM Strength
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m ²	ksf	kN/m ²
RV-B-5	P-4	20.8-21.1	6.34-6.43	SP-SM	4.0	192	3.2	153
	P-5	25.8-26.1	7.86-7.96	SM	8.0	383	6.8	326
RV-B-6	P-1	5.0-5.7	1.52-1.74	SM	1.0	48	1.2	57
	P-1	5.0-5.7	1.52-1.74	SH	2.0	96	1.9	91
	P-2	10.0-10.7	3.05-3.26	SM	1.0	48	1.1	53
	P-2	10.0-10.7	3.05-3.26	SM	2.0	96	1.9	91
	P-2	10.0-10.7	3.05-3.26	SM	4.0	192	5.1	244
	P-3	15.7-16.3	4.79-4.97	M2	1.5	72	1.6	77
	P-3	15.7-16.3	4.79-4.97	SM	3.0	144	3.0	144
	P-3	15.7-16.3	4.79-4.97	SM	6.0	287	5.2	249
RV-B-7	P-1	5.0-5.7	1.52-1.74	SW-SM	0.5	24	0.7	34
	P-1	5.0-5.7	1.52-1.74	M2-W2	1.0	48	1.3	62
	P-1	5.0-5.7	1.52-1.74	M2-W2	2.0	96	2.0	96
RV-B-12	P-6	30.0-30.7	9.14-9.36	SM	3.0	144	2.7	129
	P-8	48.0-48.7	14.63-14.84	SM	10.0	479	10.8	517
RV-B-13	P-8	50.0-50.8	15.24-15.48	ML	6.0	287	4.2	201

SUMMARY OF DIRECT SHEAR TEST RESULTS RALSTON VALLEY, NEVADA GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

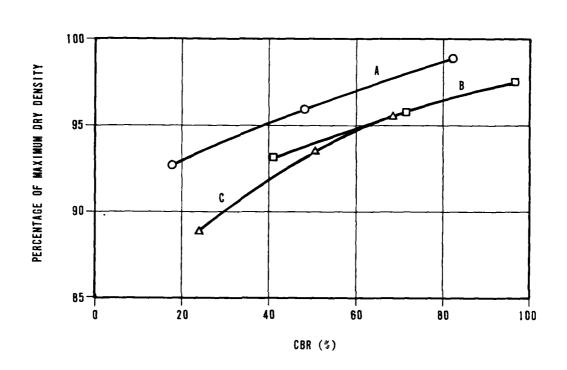
C-4

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MALSTON TALLET, NEVADA, GREAT BASIN CST

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

C-5



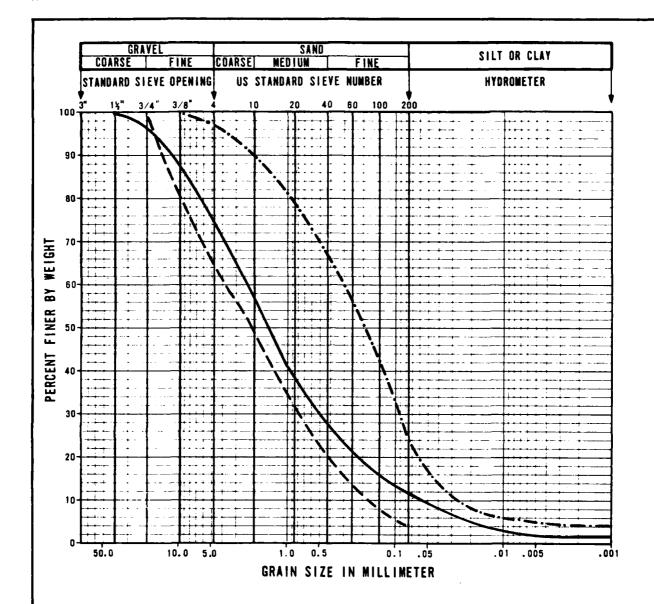
SYMBOL	COMPOSITE Sample Number	SOIL TYPE
0	A	SW-SM
0	В	SP
Δ	C	SM

CALIFORNIA BEARING RATIO (CBR) CURVES

RALSTON VALLEY, NEVADA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

FIGURE



SYMBOL	COMPOSITE Sample	TRENCH	SAMPLE	INTERVAL	SOIL
SIMOOF	NUMBER	NUMBER .	FEET	METERS	TYPE
	A	RV-T-10 RV-T-14	14.5 - 15.5 10.0 - 11.5	4.42 - 4.72 $3.05 - 3.51$	SW-SM
	В	RV-T-8 RV-T-9	2.5 - 4.5 2.5 - 5.0	0.76 - 1.37 $0.76 - 1.52$	SP
	С	RV-T-7 RV-T-7	2.0 - 3.0 16.5 - 18.0	0.61 - 0.91 5.03 - 5.49	SM

GRAIN SIZE CURVES. CBR TESTS
RALSTON VALLEY, NEVADA
GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE S

FIGURE C-8

APPENDIX D

GEOTECHNICAL DATA - SACRAMENTO VALLEY

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BORING AND TRENCH LOGS	
LOG OF BORING SV-B-3	Figure D-l
LOG OF BORING SV-B-8	Figure D-2
LOG OF BORING SV-B-12	Figure D-3
LOG OF TRENCH SV-T-2	Figure D-4
LOG OF TRENCH SV-T-6	Figure D-5
LOG OF TRENCH SV-T-10	Figure D-6
SUMMARY OF LABORATORY TEST RESULTS	
BORING SV-B-12	Table D-1
SUMMARY OF SHEAR STRENGTH	
TRIAXIAL SHEAR TEST RESULTS	Table D-2
DIRECT SHEAR TEST RESULTS	Table D-3
SUMMARY OF CALIFORNIA BEARING RATIO (CBR) T	ESTS
CALIFORNIA BEARING RATIO (CBR) TEST RESULTS	Table D-4
CALIFORNIA BEARING RATIO (CBR) CURVES	Figure D-7
GRAIN SIZE CURVES, CBR TESTS	Figure D-8

TYPE	RECOVERY	VALUE		HT	רספא	ي			80 90 100 110 120 130 140 ANALYSIS									l		
SAMPLE 80		Y N	METERS	FEET	L I THOLOGY	USCS	SOIL DESCRIPTION			5 10 15 20 25 30 35					\vdash	SA	$\overline{}$	LL	PI	
			0	ū	00° 10°° 10°°		SANDY GRAVEL, brown, fine to		•		T	• (*) • (*)				59	32	9		
	20		- 3	10 -	000°	GW- SM	coarse, well graded, medium dense, subangular to subroun calcareous, trace of silt.	ded;		1	+		-						5	
	28				000															
	60		- 6	20 -		*			┪	+	-			-		40	34	26		
	50				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0						+		\uparrow							
			- 9	30 -	SANDY GRAVEL, light bro		SANDY GRAVEL, light brown, f to coarse, poorly graded, de subangular, calcareous, weak	nse,												
			- 12	40 -	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	comented, some silt.														
50		- 15	50 -	50 -						-										
					00000		Total Depth 50.4° (15.4m)									1				
			- 18	60																
										401) 	180 kg/r	3)	220	00					
	S F B	TAN UGR ULK	DARO O DR	I VE	ETRATION	TES	Ţ	٠.	BOR ELEV DATE ORIL HOLE CASI WATE	ATI DR LIN DI NG	ON ILLE G ME AME I INSI	D THOS ER	: 2 : 3 : 4 : 0 : N	24 J tali 3 5/ tone	anu ow 8 **	ary Ster	197 n Au Bmm (iger)		
N	- ! - !	STAN N V	IDARD ALUE Uni1	PEN GREA	TER THAN GHT (AST	1 1 01 M: (ST (ASTM: 0-1588-67) D BLOWS,FOOT 0-2937-71)		SA		AME	OF NTO REA	٧A	LLI	EΥ,	AF	RIZ		A	
			RECOV		IENI (AS	FM:	D-2216-711				TING	INV	ESTI	GAT	1 ON			Ī	_	6U

TUGRO MATIONAL, INC.

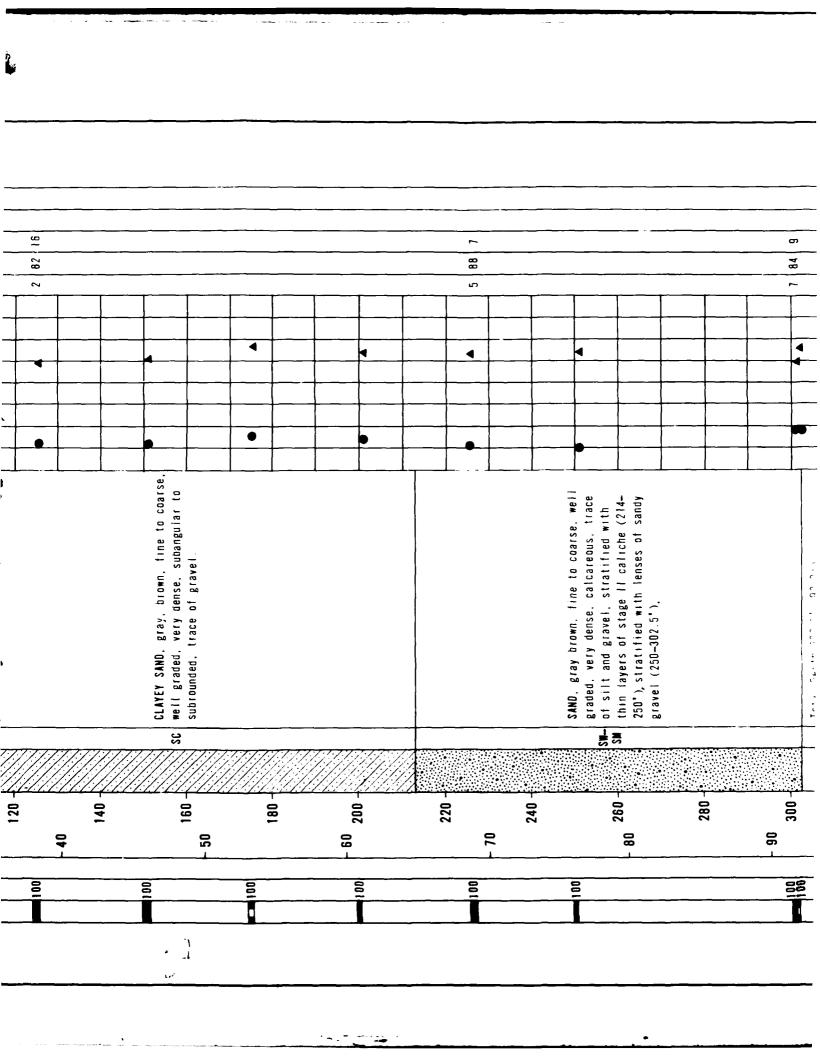
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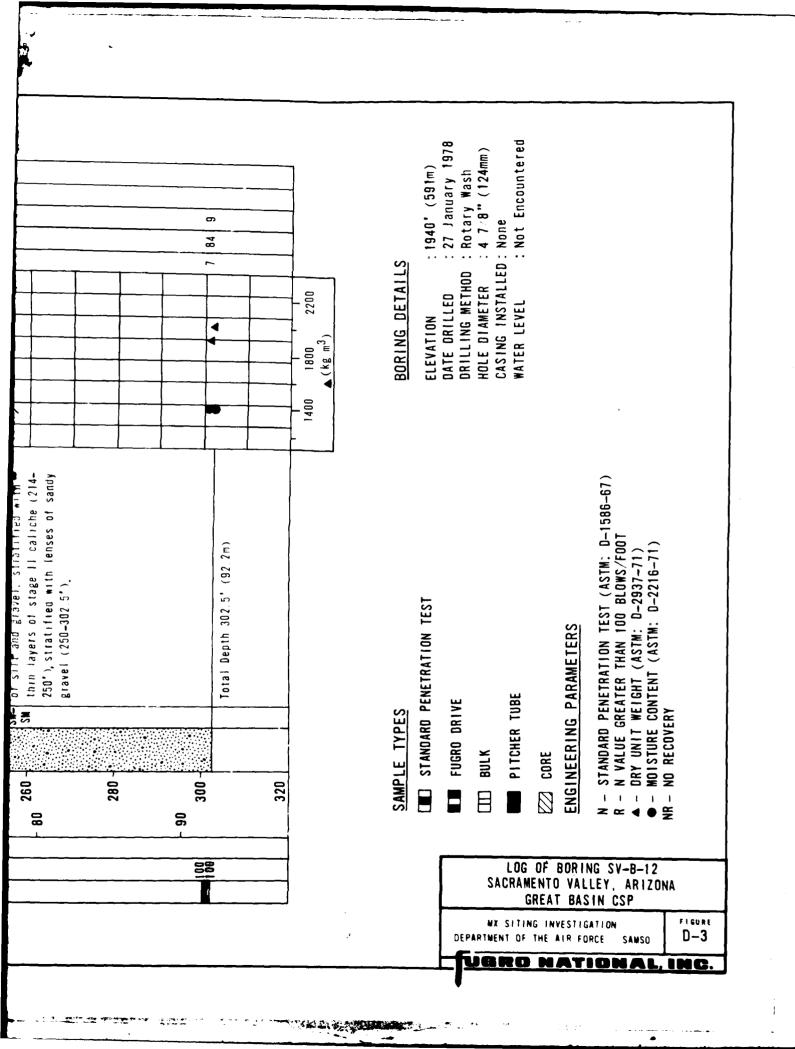
SAMPLE TYPE % RECOVERY	쁘	PTH	LITHOLOGY	nscs		64	60 90 100 (10 120 130 10 ANALYSIS									\overline{a}		
SAMPLE TYP % RECOVER N VALUE		FEET	_		SOIL DESCRIPTION	5		0	15 2	Q 2	5 30	3	15		S#	_	LL	ΡI
30 30	0	O SM				•											40	8
20	- 3	10		SW-		H		_						13	76	11		
1 00										_			_					
00	- 6	20			SILTY SAND, brown, fine to coarse poorly to well graded, medium dense to very dense, calcareous,													
71	9	30		SM	layer of silty gravel (0-1°), little gravel (7.5°-12°), stage l caliche (2°-7°), stage lll caliche (7°-7.5°), trace of clay.													
30								_					-					i
60	- 12	40				-	-	_		_			-					
	- 15	50 ·		СН	CLAY, brown, hard, highly plastic, calcareous, little sand.	lastic, calcareous, little			E.	22								
60		50			Total Depth 50.5° (15.4m)												31	22
	- 18	80					140					220						
						L			<u> </u>	g.⁄m'	3)			}				
SAMPLE S S F S F P	ī	BORING DETAILS ELEVATION : 2320° (707m) DATE DRILLED : 24 January 1978 DRILLING METHOD : Hollow Stem Auger HOLE DIAMETER : 8 5/8° (168mm) CASING INSTALLED : None WATER LEVEL : Not Encountered											:					
R N	TANDAR VALUE RY UNI	D PEN GREA T WE!	ETRATION TER THAN GHT (AST	1 1 0 0 M : 0	T (ASTM: 0-1588-67) D BLOWS: FOOT 1-2937-71)	\$		RAI	OI MEN GRE	TO	VA	LLI	EΥ,	Al	RIZ		Α	
NR N			ITENT (AS	IM:	D-2216-71)	MX	(S)	TI	NG I	NVE	STI	GAT	1 ON			T		6u R

UGRO NATIONAL INC.

A LOCAL SECTION

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40	35							_	_					_			 	 	_
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0.6	- 12	• •	•			1							_						
SOIL DESCRIPTION			CLATET SANU, gray brown, fine to coarse, poorly graded, very dense,			SILIY SANU, brown, fine to coarse, poorly graded, very dense, subangular	to subrounded, calcareous, grave!			CLAYEY SAND, brown, fine to coarse, poorly graded, very dense, calcareous,	interbedded with lenses of sandy gravel (58.8-70.5").				VIIIV SEXT brown fine to coarse von				
202	n	38		SP- SC		25	300	S	25 25			ა 2		7:7-7 7		E S		77.7.7	_
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문 283 도 구	MET	0				2				ç	07.				30	•	•	_	
ANTAN	N																		-
ECOVERY	N %	100	001	100	100	100	1 8	3	00.	9-	100	- 5	3	100	1 9	3		001	





SM Loose SILTY SAND, red brown, fine to coarse, poorly graded, subangular to subrounded, calcareous, trace of gravel. Dense SANDY GRAYEL, red brown, fine to coarse, poorly graded, subrounded, calcareous weakly cemented, trace of silt. Very dense 12 Total Depth 12' (3.7m) Stability of Vertical Walls: Stable 0-12' (0-3.7m)	BULK SAMPLE METERS S	EPTH	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	SIEVI	318
SM Loose SILTY SAND, red brown, fine to coarse, poorly graded, subangular to subrounded, calcareous, trace of gravel. Dense SANDY GRAVEL, red brown, fine to coarse, poorly graded, subrounded, calcareous, weakly cemented, trace of silt. Very dense Total Depth 12' (3.7m) Stability of Vertical Walls: Stable 0-12' (0-3.7m)					03		GR SA	FI LL
Dense SANDY GRAYEL, red brown, fine to coarse, poorly graded, subrounded, calcareous, weakly cemented, trace of silt. Yery dense Total Depth 12' (3.7m) Stability of Vertical Walls: Stable 0-12' (0-3.7m)	∭°	,		SM	Loose	coarse, poorly graded, subangular to subrounded, calcareous, trace		
Total Depth 12' (3.7m) Stability of Vertical Walls: Stable 0-12' (0-3.7m)		_			Dense	SANDY GRAVEL, red brown, fine to	48 40	12
Total Depth 12° (3.7m) Stability of Vertical Walls: Stable 0-12° (0-3.7m)		8 -		GP- GM	Very dense	calcareous, weakly cemented, trace		
16-	-4					Stability of Vertical Walls:		1
	- 5	16 -						
18-		18-						
6 20 -	-6	20 -						

TRENCH DETAILS

SURFACE ELEVATION : 2520° (768m)
DATE EXCAVATED : 30 January 1978

SURFACE GEOLOGIC UNIT: A51
TRENCH LENGTH: 29.5*
TRENCH ORIENTATION: N82E

LOG OF TRENCH SV-T-2 SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

0-4

The state of the s

BULK SAMPLE	METERS	FEET KI	L 1 THOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION		ALYS		
30.1	₩ 0	<u>8</u>			8		GR	SA	FI	LL PI
	۱	U			Loose					
	1	2		SP- SM	Dense	GRAVELLY SAND, red brown, fine to coarse, poorly graded (0-8°), well graded (8-10.5°), rounded, calcareous, stage I to stage II caliche (8-10.5°),				
	- 2	6 - 8 -				trace of silt.				
\prod	- 3	10 -		SM-	Very dense	Total Depth 10.5' (3.2m)	28	67	5	
	-4	12 -				Cementation exceeded capacity of John Deere 400 backhoe at 10.5° (3.2m). Stability of Vertical Walls: Unstable 0-8° (0-2.4m) Stable 8-10.5° (2.4-3.2m)				
	-5	16 -								
		18 -								
	-6	20 -								

TRENCH DETAILS

SURFACE ELEVATION : 2500' (762m)
DATE EXCAPATED : 31 January 1978

LOG OF TRENCH SV-T-6
SAJRAMENTO VALLEY, ARIZONA
GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

D-5

BULK SAUPLE	METERS 3		LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION		S I E \		
BOL		FEET	=		CON	SOIL DESCRIPTION	GR	SA	FI	LL P
	0	0			Loose					
	- 1	4 - 6 - 8 -		SC	Very dense	CLAYEY SAND, gray brown, fine to coarse, poorly graded, calcareous, stage I caliche (2.5°-10°) stage II caliche (10°-12°).				
	- 3	10 -				Total Depth 12° (3.7m)	6	51	43	
	-4	14-				Stability of Vertical Walls: Unstable 0-2.5° (0-0.8m) Stable 2.5-12° (0.8-3.7m)				
	-5	16 -								
	- 6	18 -								
	<u></u>	22	<u> </u>	<u> </u>				Ц_	نـــا	

SURFACE ELEVATION : 2200° (671m)

DATE EXCAVATED : 1 February 1978

SURFACE GEOLOGIC UNIT: A5y/A5i TRENCH LENGTH: 28.2° TRENCH ORIENTATION: N35W LOG OF TRENCH SV-T-10
SACRAMENTO VALLEY, ARIZONA
GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE. SAMSO

FIGURE D-6

	a)								PERCE	T FIN	ER BY	WEIGHT			
	_	SAMPLE II	NTERVAL		S	TANDAR	SIEV	E OPEN	ING		U :	S STAP	IDARD :	SIEVE	NO
BOR ING Number	SAMPLE	,		BLDRS.	COBE	LES		GRA	VEL			SA	ND		
8 3	SA	FEET	METERS	24"	12"	6"	3"	1½"	3 4"	3 8"	4	10	40	100	20
SV-B-12	D-1	2.7-3.4	7.82~1.04											}	
	1)-3	5.7-6.4	1.74-1.95									1			
	D-4	10.2-10.9	3.11-3.32							[1				T
	₽-5	15.0-16.5	4.57-5.03					I		100	92	1.9	33	16	1
	P-6	20.0-21.5	6.10-6.55												
	P-7	25.0-26.5	7.62-8.08						Ι	ŀ					
	P-8	30.0-32.3	9.14-9.84							100	97	[81]	38	22	1.
	P-9	40.4-41.8	12.31-12.74												Γ_{-}
	P-10	50.3-52.3	15.33-15.94							1		ſ			
	P-11	61.0-62.1	18.59-18.93						100	97	92	7.4	3.5	22	1
	P-12	71.0-72.5	21.64-22.10												
	P-13	81.0-81.7	24.69-24.90												
	P-14	90.0-91.4	27.43-27.86					<u> </u>	<u> </u>	L				<u> </u>	
	D-15	100.2-100.9	30.54-30.57												Ι
	P-16	125.0-126.3	38.10-38.50							100	98	78	37	2.3	1
	P-17	150.0-151.5	45.72-46.18							I		1		Ī	
	D-18	175.2-175.9	53.40-53.61						1			T	Ī	1	
	P-19	200.0-200.8	60.96-61.20												
	P-20	226.0-227.2	68.88-69.25					I	100	97	95	8.2	20	11	Π
	P-21	250.0-250.8	76.20-76.44									I			
	P-22	300.5-301.3	91.59-91.84					[Ì.	100	1 - 1 - 1	I 7%	3.5	15	
	D=23	391.7-302.4	91.96-92.17						1	[I -	I			1
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									1	<u> </u>		<u> </u>			Γ

NOTES:

(a) Sample types

- (c) USCS Unified Soil Classification System
- SS Standard split spoon
- P Pitcher
- Indicates that test has been performed and results are included in this report.
- D Fugro Drive
- B Bulk
- (b) NP Not Plastic

									11	I-SITU			C	OMPACTE		I		_ ₹		
EVE I	,	PART SIZE T OR C	(mm)		TERBE		USCS (c)	DRY (MOISTURE Content (%)	SATURATION (%)	V010 RAT10	MAXI DRY DE		OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL	UNCONFINED COMPRESSION	DIRECT	
100	200	.005	.001	LL	PL	PI	` '	(pcf)	(kg/m³)	물양	S.A.	25	(pcf)	(kg, m ³)	5 =	2 2 2	11	3 5	00	L
				 	 		sc	106.6	1703	4.0	18.8	0.58								
							SC	111.5	1786	4.3	22.7	0.51						I		L
				-	 		SC	113.3	1815	3.9	21.4	0.49				[<u> </u>	L	1
16	1				† · · · ·	-	SP-SC	110.0	1763	7.2		0.54					**	<u> </u>	.	1
	1				t "	t	Sr-SC	132.2	2118	6.0		0.28			1			↓	├	╀
	1			†	† —	1	SP-SC	128.3	2055	8.5	73.1	0.31		<u> </u>	<u> </u>			<u> </u>	 	╀
1	16			t	1	†	SM	114.7	1837	6.7	38.8	0.47		L				↓	***	╀
	1			†	 	t	SC	114.4	1833	5.7	3.1.5	0.47		Ι	L		L	↓	i	\perp
	 			 	\vdash	 	SP-SC	117.8	1387	8.8	55.3	0.43		Π		l		1	<u> </u>	L
(2)	17			1-		 	SC	105.6	1692	6.7	30.5	9.60			I	I		1	↓	\downarrow
	 - ' - '			†	<u> </u>	†	5C	116.5	1866	6.8	41.1	0.45				<u> </u>		1	↓	1
	 			t	 	1	SC	123.7	1982	5.0	41	U.36						1	↓	+
	† ~ ·			t		1	SC	123.3	1975	7.8	57.3	0.36		1		<u> </u>	L_	↓	↓	1
	 	 		†	 	<u>† </u>	SM	122.7	1966	6.2	44.7	0.37	1	Ι	<u> </u>	<u> </u>	<u> </u>	.	<u> </u>	1
.: 3	16	4	1	†		†	SC	119.2	1910	6.1	39.6	0.41			1	2.67	L	 _	*	1
. <u>-</u>	├	· · ·		 	1	t	SC	120.3	19.27	6.4	43.4	0.40		T		<u> </u>	<u> </u>	1	1	1
	+	†		†	 	 	SC	127.5	.043	7.1.	63.9	0.33	?	T	Ί	<u> </u>	L		_	1
	1			 	 	1	SC	124.5	1 + 1.1	7.2	55.3	0.35	,					1	<u> </u>	1
11	7	ł		t	 	1	SW-SM	122.7	1:30:00	5.3		0.37				<u> </u>	<u> </u>	1		4
	 	 		t	 	†	SW-SM	123.9	1985	5.3	40.3	0.36	5	T			<u> </u>		_	1
1 ,	1 5	 		 	+	1	SW-SM	117.4	1313	8.7	57.0	0.41				1	<u> </u>	1	1	1
	 	†	Ì	t	†	t	SW-SM	125.9	.2017	1 8.2						1	1	1		┙
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SUMMARY OF LABORATE BORING SV SACRAMENTO VALLEY, ARIZE

MX SITING INVESTIGA
DEPARTMENT OF THE AIR FOR

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-			C	OMPACTE)			a 8		8		
(%)	SATURATION (%)	VOID RATIO	MAX! DRY DE	NSITY	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL	UNCONFINED Compression	DIRECT SHEAR	CONSOLIDATION	CHEMICAL	RELATIVE Density
			(pcf)	(kg, m ³)	O X	80		20	00	3		
	19.5 27 .1.4 35.4	0.58 0.51 0.49 1.54										
	27	0.51		 				ļ				
-	: : : : : ; : : : :	0.49		 		·	**	ļ				
\vdash	(iii))	0.28			 							
	73.1	1.31		1	ļ							
	3,55 . 40	0.47							***			
	3	0.47	Ī					<u> </u>				
	155.3	0.43		ļ	ļ			 -	ļ			
7	30.5	1.60					<u> </u>	ļ	ļ			├
	41.1	36		}	 	}		 				
	57.3	0.36	<u>`</u>	 	 	†		†				
F —	44.7).37	1	 	1	<u> </u>						
. 1	314.0			1		2.67			*			
	43.4	7.40)									
	93.0	1 . 3.	?	1	I		L	ļ				
	55.3	0.3	Ď	 	.	}	-	 	ļ			
- :-	38.7		7	 	 	 -	 	 		<u> </u>		
- 3	40.3	0.3		}	 	 	 	 	}	 		
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SUMMARY OF LABORATORY TEST RESULTS BORING SV-B-12

SACRAMENTO VALLEY, ARIZONA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

TABLE D-1



_		_		_													_	
BACK	kN/m²	0	0	0	0	0	0	0	-	0								T
PRE	ksf	0	0	0	0	-	0	0	0	0		1	1					
STRAIN	(% min)		. I	=	01	=	2.	DI:	9.	0.								
MAXIMUM DEVIATOR	kN/m ²	1891	1245	1317	196	2226	171	1436	388	1355								
MAX DEVI	ks f	39.5	26.0	27.5	20.2	46.5	1.91	30.0	8-	28.3								
NING RE(O ₂)	kN/m ²	192	96	383	287	575	144	287	98	383						 -		
PRESSURE (0,)	ksf	4	2	80	8	12	9	9	2	80								
MOISTURE	(%)	10.4	7.8	5.7	7.5	5.9	9.1	5.7	5.2	7.1								
DENSITY	kg/m3	1927	1927	1772	1724	1778	1831	1887	1714	1743								
DRY D	pc f	120.3	120.3	110.6	107.6	11.0	114.3	118.4	107.0	108.8								
TYPE OF	TEST	8	8	93	8	2	8	CO	CO	9					<u> </u>			
7108	TYPE	SC	SC	NS	N.S.	NS.	SP-SC	SW-SM	SP-SC	SP-SC								
INTERVAL	METERS	4.57-4.79	4.79-5.00	6.10-6.31	15.24-15.42	15.42-15.61	7.68-7.89	15.00-15.21	4.57-4.72	4.88-5.03								
SAMPLE	FEET	15.0-15.7	15.7-16.4	20.0-20.7	50.0-50.8	50.6-51.2	25.2-25.9	49.2-49.9	15.0-15.5	16.0-16.5								
SAMPLE	30	P-5		P-6	P-1		1-1	0-10	<u>2</u>									
BORING	. ON	SY-B-1			SV-8-5		SV-8-10		SV-B-12									

SUMMARY OF TRIAXIAL SHEAR TEST RESULTS
SACRAMENTO VALLEY, ARIZONA
GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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BORING	SAMPLE	SAMPLE 1	HTERVAL	SOIL	NORMAL	STRESS	MAXI SHEAR S	MUM Trength
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m ²	ksf	kN/m²
SV-B-1	P-9	35.0-35.7	10.67-10.88	SP-SM	4	192	3.4	163
					6	287	6.0	287
					8	383	6.6	316
SV-8-5	D5	15.2-15.9	4 . 63-4 . 85	30	2	96	2.4	115
					4	192	3.6	172
					8	383	9.4	450
SY-B-7	D-5	15.4-16.1	4.69-4.91	SM	2	96	3.4	163
					4	192	5.6	268
					8	383	10.3	493
SV-8-10	D-4	13.7-14.4	4.18-4.39	SP-SM	2	96	2.0	96
					4	192	3.8	182
					8	383	6.6	316
SV-B-12	P-8	31.0-31.7	9.45-9.66	SM	3.5	168	3.6	172
					1	335	8.5	407
					10.5	503	9.9	474
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SUMMARY OF DIRECT SHEAR TEST RESULTS SACRAMENTO VALLEY, ARIZONA GREAT BASIN CSP

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAMSO

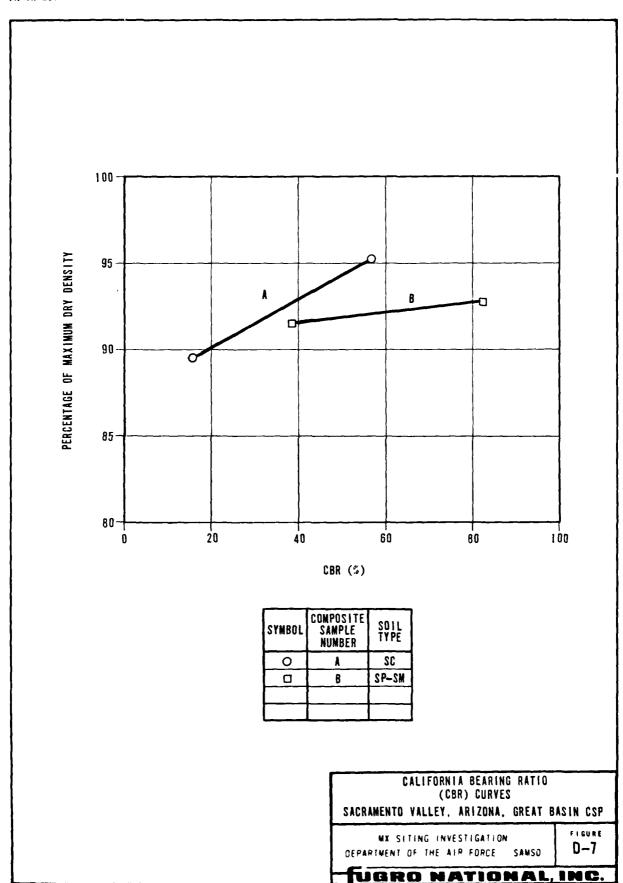
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	1108	PERCENT	ATTE	ATTERBERG LIMITS	SPECIFIC		MAXIMUM DRY DENSITY	OPTIMUM	COMP.	COMPACTED DRY DENSITY	COMPACTED	PERCENT OF MAXIMUM	CBR
	#20		=	<u>_</u>	GRAVITY		kg/m3	(%)	ac d	kg/m3		DRY DENSITY	<u>3</u>
									113 B	1820	11 7	1 20	1.5
25 25	•	<u></u>				119.5	1914	<u>.</u>	0 20	┵	1	- CO	5 2
	í								2.70		2	0.00	9
-													
									123.0	1970	8.1	93.8	82
SP-SM 1	_	=				131.1	2100	8.0	119.8	1913	8.3	91.4	39
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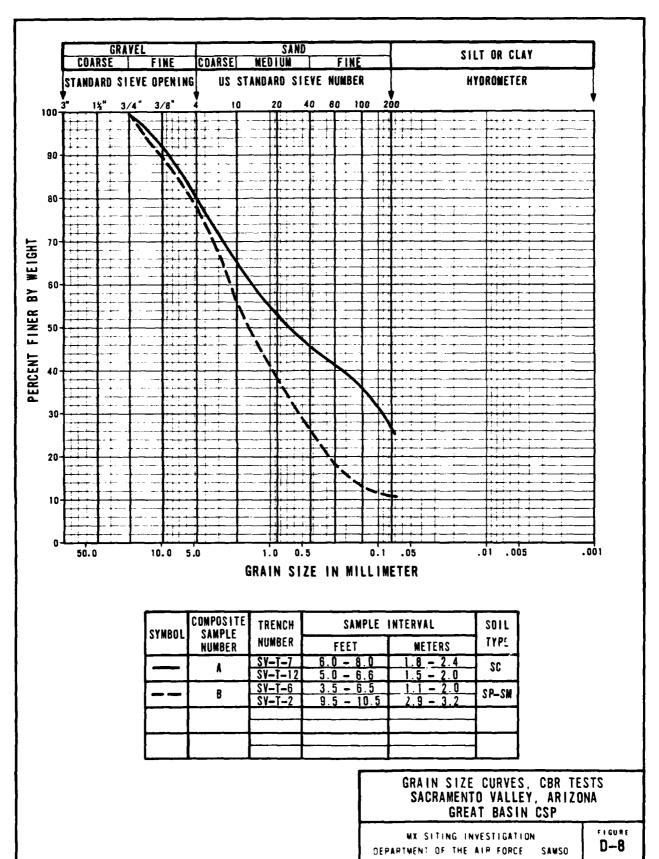
CALIFORNIA BEARING RATIO
(CBR) TEST RESULTS
SACRAMENTO VALLEY, ARIZONA, GREAT BASIN CSP

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

TABLE D-4



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